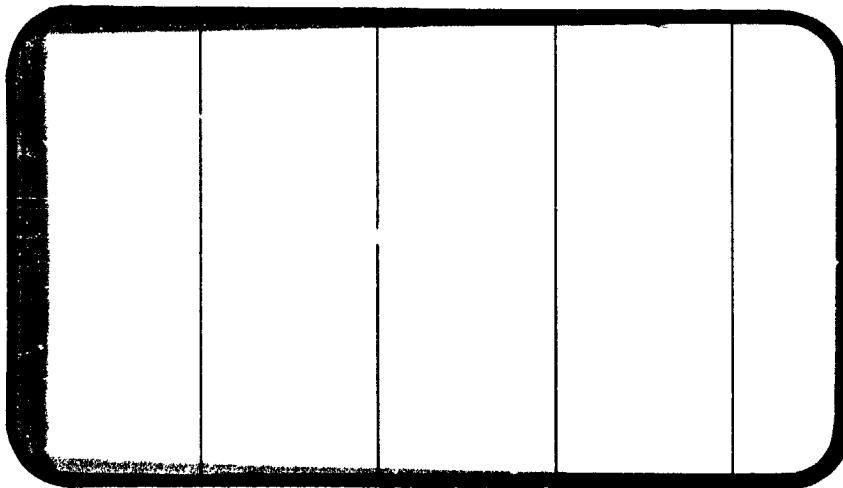


NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

NASA CR-

134425



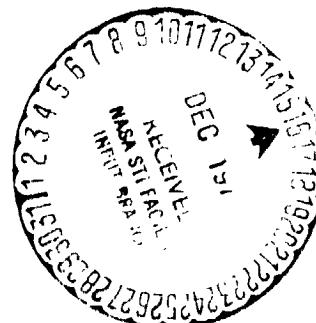
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SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT



JOHNSON SPACE CENTER

DATA MANAGEMENT SERVICES

HOUSTON, TEXAS

SPACE DIVISION

CH R
CORPORATION

November, 1974

S-DR-2181
NASA CR-134,425

A HYPERSONIC FORCE AND MOMENT TEST OF A
0.006 SCALE MODEL (466) OF THE 330.2 INCH DIAMETER
EXTERNAL TANK IN THE AMES RESEARCH CENTER
3.5 FOOT HYPERSONIC WIND TUNNEL (TA9F)

By

P. E. Ramsey, MSFC
T. C. Davis, NSI

Prepared under NASA Contract Number NAS9-13247

by

Data Management Services
Chrysler Corporation Space Division
New Orleans, La. 70169

for

Engineering Analysis Division

Johnson Space Center
National Aeronautics and Space Administration
Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Number: ARC 3.5 HWT 196
NASA Series Number: TA9F
Test Dates: 30 May through 12 June 74
Occupancy Hours: 120
Model Number: 466

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Chrysler Corporation Space Division assumes no responsibility for the data presented other than display characteristics.

A HYPERSONIC FORCE AND MOMENT TEST OF A 0.006 SCALE MODEL (466) OF
THE 330.2 INCH DIAMETER EXTERNAL TANK IN THE AMES RESEARCH
CENTER 3.5 FOOT HYPERSONIC WIND TUNNEL (TA9F)

By

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ABSTRACT

A wind tunnel force and moment test of the Space Shuttle External Tank (NASA series test number TA9F) was conducted at the Ames Research Center 3.5 Foot Hypersonic Wind Tunnel during June of 1974. The wind tunnel model was a 0.006 scale model of the 330.2 inch diameter External Tank with nose cap and lightning rod.

Data were obtained over an angle-of-attack range from 0 to 180 degrees at Mach numbers of 5.3 and 10.4. Body roll angles varied from 0 to 315 degrees for the Mach number 10.4 tests. A constant roll angle of 180 degrees was used for all Mach number 5.3 tests. The effects of protuberances and Reynolds number on the force and moment coefficients were investigated.

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PLOT SCHE. LES:

- A) CNM, CA, CL , CY , CBL, XCP/L VS. ALPHA
- B) CAF, CAB VS. ALPHA
- C) C , CA, C , CYNM, CBL, XCP/L VS. PHI
- D) CAF, VS. PHI
- E) DC , DC , DCYM, DCYNM, DCBL VS. ALPHA
- F) F, DC VS. ALPHA

INTRODUCTION

The Space Shuttle External Tank (ET) will be separated from the Orbiter before orbit is achieved. The ET will then reenter the atmosphere at hypersonic speeds. Since the ET is not designed structurally to withstand reentry, the combined force and heat loads are expected to break it up before impact in the Indian Ocean. The size of the "footprint" formed by falling pieces of the ET will depend on the altitude that breakup occurs. Therefore, to predict the altitude of breakup and thus the footprint, reliable estimates of aerodynamic heating rates and forces and moments must be obtained over the entire reentry trajectory. The purpose of this report is to present the results of a hypersonic force and moment test of the ET in the NASA Research Center 3.5' hypersonic tunnel.

The model tested was a 0.0 scale representation of the 330.2" diameter External Tank with nose cap. Photographs of the model, installed in the tunnel, are presented in Figures 3a through 3c. The configuration reference drawing is Rockwell International drawing VL78-00 62B. A reproduction of the basic ET fairing drawing is shown in Figure 2a. The model included scaled protuberances.

The test was conducted primarily at a Mach number of 10.4 but some data were taken at Mach 5.3. For Mach 10.4, data were recorded at thirty-six (36) angles-of-attack between 0° and 18° and at eight (8) roll angles between 0° and 360°. At Mach 5.3, data were obtained only at 18° roll angle and at angles-of-attack between 0° and 180°. The test covered a range of Reynolds numbers that correspond to an altitude range between

INTRODUCTION (Concluded)

35,000 and 80,000 feet as defined in the trajectory of Reference 1. Since portions of the test occurred near the transition flow regime, data at Mach 10.4 and roll angle of 0° were taken at the maximum and minimum Reynolds number capability of the facility to check for variation with Reynolds number.

The test required approximately 120 hours of test time. It began on 30, 1974. The test was assigned a test number of 196 and a SA series number of TA9F.

N ENCLATURE

GENE L

<u>SYM</u>	<u>PLOT</u>	<u>DEFINITI</u>	<u>UNITS</u>
<u>SYM</u>	<u>L</u>		
A_b		base area; cross-sectional area of the cylindrical ET	in. ²
A_c		cavity area, area of the opening required for the balance and sting	in. ²
		Balance nt Center	
b_{ref}	B F	reference span; diameter of the cylindrical section of the el	in.
c.g.		center of gravity	
ET		External Tank	
F_A		axial force (AF), positive in the negative direction of x	lb
F_N		no 1 force (NF), positive in the negative direction of z	lb
F_y		side force (SF), positive in the positive direction of y	lb
l_{ref}	LREF	reference length; dia ter of the cylindrical section of the el	in.
M	CH	ch number	
MRP	P	nt Reference Point (Located in the x, y, z axes by , YMRP, and RP)	
M_x		rolling nt (); a t about the x-axis (a positive rolling nt tends to rotate the positive y-axis t rd the positive z-axis)	in.-lb

N NCLATURE (Continued)

<u>SY OL</u>	<u>PLOT SY OL</u>	<u>INITI</u>	<u>UNITS</u>
M_y		pitching moment (); a moment about the y-axis (a positive pitching moment tends to rotate the positive z-axis toward the positive x-axis)	in.-lb
M_z		yawing moment (); a moment about the z-axis (a positive yawing moment tends to rotate the positive x-axis toward the positive y-axis)	in.-lb
q_∞	$Q(\text{PSI})$	free stream dynamic pressure	psi
$/L$	$/L$	unit Reynolds number	per ft
S_{ref}	S_{REF}	reference area; cross-sectional area of the cylindrical ET	in. ²
P		pressure	psi
SRB		Solid Rocket motor	
T		temperature, °F	

MISSILE SYSTEM COEFFICIENTS

C_{A_m}	CA	axial force; $F_A/q_\infty S_{\text{ref}}$
C_{Ab}		side axial force; $(P_a - P_b) A_b/q_\infty S_{\text{ref}}$
C_{Af_m}	CAF	fore axial force; $C_A - C_{Ab}$
C	CBL	rolling moment; $M_x/q_\infty S_{\text{ref}} L_{\text{ref}}$
C_{m_m}	C	pitching moment; $M_y/q_\infty S_{\text{ref}} L_{\text{ref}}$
C_{N_m}	C	lift force; $F_N/q_\infty S_{\text{ref}}$

N ENCLATURE (Continued)

<u>SY OL</u>	<u>PLOT SY L</u>	<u>DEFINITION</u>
C_{n_m}	CYNM	yawing moment; $M_z/q_\infty S_{ref} b_{ref}$
C_p	CP	pressure coefficient; $(P_1 - P_\infty)/q_\infty$
C_y_m	CYM	side force; $F_y/q_\infty S_{ref}$
ΔC	DCA	incremental axial force coefficient
ΔC_{Ab}	DC	incremental base axial force coefficient
ΔC_{Af_m}	AF	incremental fore-aft axial force coefficient
ΔC_{L_m}	DCBL	incremental rolling moment coefficient
ΔC		incremental no. 1 force coefficient
ΔC_{m_m}		incremental pitching moment coefficient
ΔC_{n_m}	DCY	incremental yawing moment coefficient
ΔC_{y_m}	DCYM	incremental side force coefficient
$X_{cp/l}$	XCP/L	center of pressure location, where XCP is the center of pressure location in terms of the decimal fraction of ET length (1846.9) aft of the ET nose (sta 328.92), $XCP/L = 0.5832 - 0.17(C_l/CNM)$
*	PHI	angle of roll, e.g. (for a pilot's viewpoint in an airplane, a positive roll angle is a clockwise rotation)
TC		test condition number, see Test Condition Section
ref		subscript, reference conditions
-		subscript, freestream conditions
b		subscript, base
c		subscript, cavity

NOMENCLATURE (Concluded)

<u>SY OL</u>	<u>PLOT SYMBOL</u>	<u>DEFINITION</u>
t		subscript, total conditions
m		subscript, missile axis
α		angle of attack in the body axis system, degrees
β	BETA	angle of sideslip in the body axis system, degrees.
α_T	ALPHA	angle of attack in the missile axis system, degrees.

CONFIGURATIONS INVESTIGATED

The model configuration for this test was defined by Rockwell International drawing VL78-000062B. A part of this drawing is reproduced in Figure 2a.

The model is a 0.006 scale representation of the Space Shuttle External Tank. Model length including the nose cap is 11.303 inches and model diameter is 1.98 inches. The model was machined in several parts to allow maximum utilization of all model parts while testing with different sting arrangements. The model could be mounted on the sting by the nose, tail or side. This allowed coverage of angles-of-attack from 0° to 180° with minimum sting interference. The basic model parts are the nose tip, the nose plug, the nose, the center body, the base and the base plug. These parts are shown in Figure 2b. Two center bodies were constructed. The first one, to be tested in the nose or tail mounted positions, could be rotated to cover the 0° to 315° roll angle range without removal of the protuberances. The second, to be tested in the side mount position, could not be rotated. All center body protuberances had to be moved each time a new roll angle was desired. The nose and tail sections were rotated to cover all of the roll angles without removing the protuberances. Drawings of these sections are shown in Figures 2c through 2i.

Only the largest protuberances were modeled (see Fig. 2a). They included the Orbiter-ET attach structure (forward and aft), the forward and aft SRB attach structure, LO₂ feed line, LO₂ recirculation line with electrical conduit and the LH₂ pressure line with electrical conduit.

CONFIGURATIONS INVESTIGATED (Concluded)

Drawings for the protuberances are shown in Figure 2h and in Figures 2j through 2q.

Because of the high temperatures encountered in this test, the balance was insulated with a sleeve especially built for the model. A drawing of the sleeve is shown in Figure 2r. The sleeve was built in 3 layers as shown. The inner layer, which was closest to the balance, was .125 inch thick stainless steel. The outer layer was also stainless steel and was .089 inch thick. The middle layer, or insulating material, was .25 inch thick and made from "G-10 Epoxy Glass" insulation material. The thermal conductivity of this material is 4×10^{-4} cal/sec/cm²/°C/cm. The insulation was machined for a press fit between the inner and outer layers. Eight (8) epoxy glass dowel pins were used to permanently bind all three layers together. A hole through the three layers in four places was used to attach the sleeve to the 3/4 inch diameter Task balance. The sleeve was then placed into the center body and pinned to the body in 2 places. The sleeve contained 8 holes, each equally spaced, to accept the 2 pins. These holes allowed the center body (for the 10° sting) to be rolled in 45° increments around the sleeve. There were no heat paths directly through the model to the balance. No heating problems were encountered during the test.

The model support hardware consisted of a 10° sting, a 90° sting and a sting adapter to connect the sting to the tunnel strut.

An assembly drawing of the model mounted in all three positions is shown in Figure 2s.

TEST FACILITY DESCRIPTION

The Ames 3.5 foot Hypersonic Wind Tunnel is a closed circuit blowdown tunnel capable of operating at nominal Mach numbers of 5.2, 7.4 and 10.4; at pressures to 1800 psia and temperatures to 3400°R for run times to four minutes. The major components of the facility include a gas storage system where the test gas is stored at 3000 psi, a storage heater filled with aluminum - oxide cored brick capable of heating the test gas to 3400°R, contoured nozzles with exit diameters of 42 inches for generating the desired Mach number, and a 900,000 ft³ vacuum storage system which operates to pressures of 0.3 psia. The test section itself is an open-jet type enclosed within a chamber approximately 12 feet in diameter and 40 feet in length, arranged transversely to the flow direction. The length of the jet is approximately 10 feet.

A model support system is provided that can pitch models through an angle-of-attack range of -20 to +18 degrees, in a vertical plane, about a fixed point 1 to 5 feet from the nozzle exit plane. The model is normally out of the test stream until the tunnel test conditions are established, after which it is inserted. Insertion time is adjustable to as little as 1/2 second and models may be inserted at any strut angle. A closed circuit video system with a recorder is available for visually monitoring the experiments within the test cabin.

A data acquisition system accepts analog signals at rates up to 2500 samples per second, converts them into digital form and records on magnetic tape for later reduction by a digital computer.

The tunnel operates two 8-hour shifts per 24-hour day.

INSTRUMENTATION

The balance used in this test was a .75 inch diameter Task balance. The balance is a six component internal strain gage balance. The reference balance drawing furnished by Ames is 6656. The description number given the balance is MK XXIX 6656 B. The load range of the balance is:

Normal Force	= 200 lb
Pitching Moment	= 200 in-lb
Side Force	= 100 lb
Yawing Moment	= 100 in-lb
Axial Force	= 30 lb
Rolling Moment	= 30 in-lb

Because of the small loads at Mach 10.4 as compared to Mach 5.3, a 1/2 load balance calibration was performed. This calibration was used in the data reduction for runs at Mach 10.4. The normal full scale calibration was used in the data reduction for runs at Mach 5.3.

TEST CONDITIONS

The test program consisted of approximately 120 hours of tunnel time. The angle-of-attack range was 0° to 180° in five degree increments. Two stings were used in an effort to minimize sting interference over the angle-of-attack range. The first one, the 10° sting, could be mounted in the nose or tail of the model and was used for angle-of-attack ranges -5° to 30° and 150° to 185° . The angle-of-attack range 30° to 150° was covered using a 90° sting mounted from the side of the model.

Because the sector of the tunnel is only capable of an angle range of -20° to 18° , the sting was mounted in one of three positions on the strut. These positions are assigned a number and are shown in Figure 2t. Number 1 position was 40° above the strut centerline. Number 2 position was on the strut centerline and number 3 was 40° below the strut centerline. In each case the center of rotation was the same. The following notation was used to denote the range to be covered on a run:

NOTATION	STRUT POSITION	STING	STING POSITION	MODEL α RANGE	SECTOR α RANGE
A'	2	10°	Tail	-5° to 30°	-20° to 15°
G	1	90°	Side	30° to 60°	-20° to 15°
F	2	90°	Side	70° to 105°	-20° to 15°
E	3	90°	Side	110° to 145°	-20° to 15°
C'	2	10°	Nose	150° to 185°	-20° to 15°

All increments are 5°

This schedule is illustrated pictorially in Figure 2t.

TEST CONDITIONS (Concluded)

The angle of roll was varied from 0° to 315° in 45° increments. When 10° sting was used the entire model could be rolled about the sting. This eliminated the necessity of removing all protuberances on every run. When the 90° sting was being used, the protuberances located on the center body were removed and relocated. Both the nose and tail could be rotated and protuberances located there were not removed. Runs were made with and without protuberances (clean body).

Test conditions at Mach 5.3 were chosen to restrict the dynamic pressure to a value that would not overload the balance. Test conditions for the runs at Mach 10.4 were chosen on the following bases: An intermediate stagnation pressure and temperature that allowed fast re-cycle time of the tunnel (determined by discussion with Ames personnel); a low and high stagnation pressure and temperature that allow data to be checked on a similarity parameter basis. The resulting test conditions are shown in the following table:

CONDITION NUMBER	M_{∞}	P_t (psia)	q_{∞} (psi)	T_t (°R)	TEST TIME (sec)	R_N/ft $\times 10^{-6}$
1	5.3	275	7.184	1200	140	3.81
2	10.4	400	.512	2000	100	.39
3	10.4	1200	1.720	2000	160	1.16
4	10.4	1800	2.303	2000	180	1.74

DATA REDUCTION

Parameters measured and recorded during this test were:

- o Wind tunnel conditions (P_∞ , P_t , T_t)
- o Six-component force and moment data
- o Sting attitude
- o Base pressure (on the runs where the angle-of-attack range was either -5° to 30° or 150° to 185°).

Tunnel conditions were used to calculate the Mach number, the dynamic pressure, and the Reynolds number; the six-component force and moment data were used to calculate static stability coefficients; the sting attitude and initial model attitude were used to calculate the model angle-of-attack, and the base pressures were used to calculate base pressure coefficients.

The following equations were used to reduce force and moment data to non-dimensional coefficients in the missile axis system.

$$C_{N_m} = \text{normal force coefficient}$$
$$= F_N/q_\infty S_{ref}$$

$$C_{m_m} = \text{pitching moment coefficient}$$
$$= M_y/q_\infty S_{ref} b_{ref}$$

$$C_{A_m} = \text{axial force coefficient}$$
$$= F_A/q_\infty S_{ref}$$

$$C_{Y_m} = \text{side force coefficient}$$
$$= F_y/q_\infty S_{ref}$$

$$C_{n_m} = \text{yawing moment coefficient}$$
$$= M_z/q_\infty S_{ref} b_{ref}$$

DATA REDUCTION (Concluded)

$$C_{\ell_m} = \text{rolling moment coefficient}$$
$$= M_x/q_\infty S_{ref} b_{ref}$$

$$C_{A_{b_m}} = \text{base axial force coefficient}$$
$$= (P_\infty - P_b) A_b/q_\infty S_{ref}$$

The positive directions of the forces and moments are shown in Figure 1.

The following reference data were used to reduce the force and moment data to aerodynamic coefficients:

$$S_{ref} = 3.08 \text{ in.}^2$$

$$l_{ref} = 1.98 \text{ in.}$$

$$b_{ref} = 1.98 \text{ in.}$$

$$A_b = 3.08 \text{ in.}^2$$

The moment reference point for this external tank configuration was at a tank X station of 1406 (see Fig. 2a). This placed the MRP 1.08 inches aft of the .

The center of pressure location was calculated as follows:

$$XCP/L = 0.5832 - 0.17 (CL /C)$$

where $0.5832 = (XT_{MRP} - XT_{NOSE})/L_{TANK}$

$$0.1788 = LREF/L_T K$$

$$XT_{MRP} = ET \text{ MRP station}$$

$$XT_{NOSE} = ET \text{ nose station}$$

$$L_T K = ET \text{ length}$$

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5. Davis, Tommy, "A Pre-Test Report for a Hypersonic Force and Moment Test of the .006 Scale 330.2 Inch Diameter External Tank in the Ames Research Center 3.5 Ft. Hypersonic Wind Tunnel", Northrop Services, Inc., M-9230-74-283, May 1974.

TABLE I.
TEST CONDITIONS
TEST 196

MACH NUMBER	REYNOLDS NUMBER per foot	DYNAMIC PRESSURE (pounds/sq. inch)	STAGNATION TEMPERATURE (degrees Fahrenheit)
5.3	3.81×10^6	7.184	740
10.4	3.90×10^5	.512	1540
10.4	1.16×10^6	1.720	1540
10.4	1.74×10^6	2.303	1540

CE UTILIZED: MK XXIX 6656B

C ACITY:

ACCURACY:

COEFFICIENT
TOLE CE:

NF	<u>200 lb</u>
SF	<u>100 lb</u>
AF	<u>30 lb</u>
PM	<u>200 in.-lb</u>
	<u>100 in.-lb</u>
	<u>30 in.-lb</u>

OO NTS:

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

TABLE II.

TEST : ARC 3.5 196 (TH49F) DATA SET RUN NUMBER COLLATION SUMMARY

DATA SET IDENTIFIER	CONFIGURATION	SCHED. NO.	CONTROL DEFLECTION α OR β (deg)	RUNS	PM I (°) FOR ALTERNATE INCIDENCE VARIABLES										
					A	B	MACH	RNL	0	45	90	135	180	225	270
REYMA1 TANK WITH PROTUBERANCES															
G1		G	T		8	22	27	28	33	34	39	40	45		
F1		F			8	23	26	57	32	35	38	41	44		
E1		E			8	24	25	30	31	36	37	42	43		
C1		C'	▼	▼	8	3	4	5	6	7	8	9	10		
REYMA2 BASIC TANK															
G2		G	T	T	1	1	1	1	1	1	1	1	1		
F2		F			1	1	1	1	1	1	1	1	1		
E2		E			1	1	1	1	1	1	1	1	1		
C2		C'	▼	▼	1	1	1	1	1	1	1	1	1		
REYMA3 TANK WITH PROTUBERANCES															
G3		G	T		1	1	1	1	1	1	1	1	1		
F3		F			1	1	1	1	1	1	1	1	1		
E3		E			1	1	1	1	1	1	1	1	1		
C3		C'	▼	▼	1	1	1	1	1	1	1	1	1		
CONCLUDING COMMENTS															
1	7	13	19	25	31	37	43	49	55	61	67	73	75	76	
COEFFICIENTS															
α OR β	$d(\alpha) = -5^\circ \rightarrow 30^\circ (\Delta\alpha = 5^\circ)$	$d(\beta) = 70^\circ \rightarrow 105^\circ (\Delta\beta = 5^\circ)$	α AND β	$d(\alpha) = 30^\circ \rightarrow 70^\circ (\Delta\alpha = 5^\circ)$	$d(\beta) = 110^\circ \rightarrow 150^\circ (\Delta\beta = 5^\circ)$	IOVAR (1)	IOVAR (2)	NOV							
SCHEDULES															
ACAB FOR DATA SETS REYMA1, C1, A2, C2, A3, C3, A4, AND A5 ONLY															

TEST: AR_C 35 196 (TA_F)

TABLE II.

DATA SET RUN NUMBER COLLATION SUMMARY

DATE: JUNE 1974

DATA SET IDENTIFIER	CONFIGURATION	SCMD.	CONTROL DEFLECTION: A OR B mm RAL	NO. OF RUNS	PAJ (%) FOR ALTERNATE INDEPENDENT VARIABLE	TEST RUN NUMBERS						
						45	90	135	180	225	270	315
<u>REYN4</u>	<u>TANK WITH</u>	A'	0	104	0.34							
	<u>G4 PROTRUSIONES</u>	G	T									
	F4	F	↓									
<u>REYM5</u>	<u>TANK WITH</u>	A'	0	104	1.74							
	<u>G5 PROTRUSIONES</u>	G	T									
	F5	F	↓									
<u>REYM6</u>	<u>TANK WITH PROTRUSIONES</u>	A'	0	104	0.31							
	F6	F	↓									
<u>REYM7</u>	<u>TANK WITH PROTRUSIONES</u>	A'	0	104	1.16							
<u>OR B SCHEDULES</u>												
<u>COEFFICIENTS</u>												
<u>IDVAR (1) IDVAR (2) NDV</u>												
7 13 25 31 37 43 49 55 61 67 75 76												

TABLE III.
DEL DIMENSI^O DATA

DEL CO ONENT: EXTERNAL TANK (ET)

GENERAL DESCRIPTION: EXTERNAL OXYGEN-HYDROGEN TANK (MACHINED IN SIX PARTS)

MODEL SCALE = .006

DRAWING NUMBER: V1.78-000062B

RE A

DIMENSIONS:

EL MODEL S E

Length, IN. (NOSE @ X_T=298) 1883.8 11.303 IN.

Max. Width IN. (DIA) 330.2 1.98 IN.

x. Depth

Fineness Ratio — 5.71 5.71

Area

x. Cross-Sectional — 3.08 IN.²

Planform

Wetted

Base — 3.08 IN.²

TABLE III. (Continued)

L COMPONENT: ATTACH STRUCTURE

RAL DESCRIPTION: FORWARD ORBITER/ET - ATTACH STRUCTURE

SCALE = .006

DRAWING NUMBER: VL78-000062B

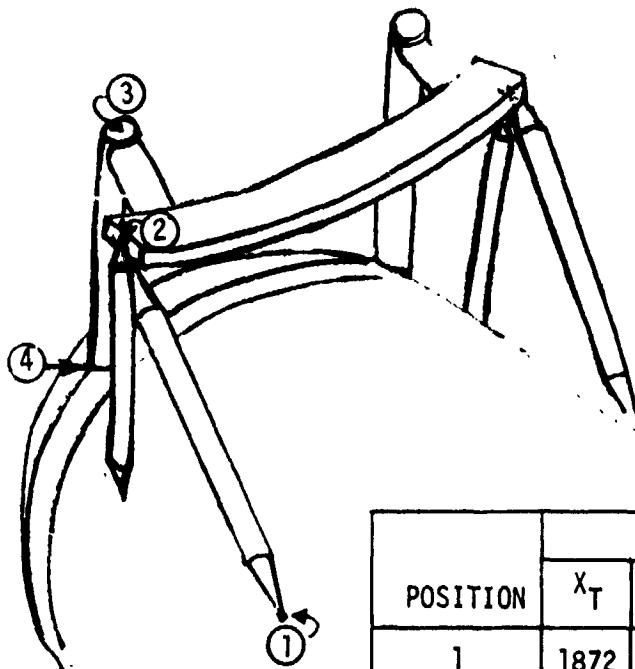
DIMENSIONS:	THEORETICAL		A	AL MEASURED
	FULL-SCALE	MODEL SCALE	MODEL SCALE	
LOCATION OF CENTER				
x_T	<u>1129.9</u>	<u>6.78</u>		
y_T	<u>0.0</u>	<u>0.0</u>		
z_T	<u>214.0</u>	1.284		
ANGLE MADE BY MEMBERS =	<u>92°40'</u>	<u>92°40'</u>		
DIAMETER OF MEMBERS =	<u>5.67</u>	<u>.034</u>		

TABLE III. (Continued)

MODEL COMPONENT: ATTACH STRUCTURE

GENERAL DESCRIPTION: REAR ORBITER ET ATTACH STRUCTURE. STRUCTURE IS MADE WITH BASE (PART NO. 80M42703).

DRAWING NUMBER: VL78-000062B and SK-RL 21974



POSITION	FULL SCALE			MODEL SCALE		
	X _T	Y _T	Z _T	X _T	Y _T	Z _T
1	1872	125.68	115.50	11.232	.754	.693
2	2058	96.50	203.56	12.348	.579	1.221
3	2088	70.0	203.56	12.528	.42	1.221
4	2088	70.0	100.00	12.528	.42	.6

*FOR DETAIL MODEL DIMENSIONS SEE FIGURE 2g.

TABLE III. (Continued)

MODEL COMPONENT: CENTER BODY AND BASE PROTUBERANCE NUMBER 1

GENERAL DESCRIPTION: LH₂ PRESSURE LINE AND ELECTRICAL CONDUIT

MODEL SCALE = .006

DRAWING NUMBER: VL78-000062B

<u>DIMENSIONS:</u> (INCHES)	<u>THEORETICAL</u>	<u>ACTUAL MEASURED</u>	
	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>	<u>MODEL SCALE</u>
HEIGHT	<u>5.0</u>	.03	_____
WIDTH	<u>10.0</u>	.06	_____
X _T (BEGINNING)	1040	6.24	_____
X _T (ENDING)	2052	12.312	_____
RADIAL POSITION	33°45'	<u>-35°9'</u>	_____

TABLE III. (Continued)

MODEL COMPONENT: NOSE AND NOSE PLUG PROTUBERANCE

GENERAL DESCRIPTION: LO₂ PRESSURE LINE AND ELECTRICAL CONDUIT ALONG NOSE

MODEL SCALE = .006

DRAWING NUMBER: VL78-000062B

DIMENSIONS: (INCHES)	THEORETICAL		A	AL	SURED
	FULL-SCALE	MODEL SCALE	MODEL SCALE	MODEL SCALE	
HEIGHT	6.67	.04			
WIDTH	10.00	.06			
X _T (BEGINNING)	<u>360.92</u>	2.165			
X _T (ENDING)	4.805	800.92			
RADIAL POSITION	<u>33.45°</u>	<u>32°42'</u>			

TABLE III. (Continued)

MODEL COMPONENT: CENTER BODY AND BASE PROTUBERANCE NUMBER 2

GENERAL DESCRIPTION: LO₂ FEED LINE

MODEL SCALE = .006

DRAWING NUMBER: VL78-000062B

DIMENSIONS: (INCHES)	<u>THEORETICAL</u>		ACTUAL MEASURED
	FULL-SCALE	MODEL SCALE	MODEL SCALE
HEIGHT	<u>16.67</u>	<u>.1</u>	
WIDTH	<u>16.67</u>	<u>.1</u>	
X _T (BEGINNING)	<u>1040</u>	<u>6.24</u>	
X _T (ENDING)	<u>2052</u>	<u>12.312</u>	
RADIAL POSITION	<u>23°24'</u>	<u>23°24'</u>	

TABLE III. (Continued)

MODEL COMPONENT: CENTER BODY AND BASE PROTUBE... CE NUMBER 3GENERAL DESCRIPTION: ELECTRICAL CONDUIT, LO₂ RECIRCULATION LINE AND LO₂
PRESSURE LINEMODEL SCALE = .006DRAWING NUMBER: VL78-000062B

DIMENSIONS: (INCHES)	FULL-SCALE	THEORETICAL	ACTUAL MEASURED
		MODEL SCALE	MODEL SCALE
HEIGHT	<u>6.67</u>	<u>.040</u>	
WIDTH	<u>19.0</u>	<u>.114</u>	
X _T (BEGINNING)	1040	6.24	
X _T (ENDING)	2052	12.312	
RADIAL POSITION	33°45'	34°16'	

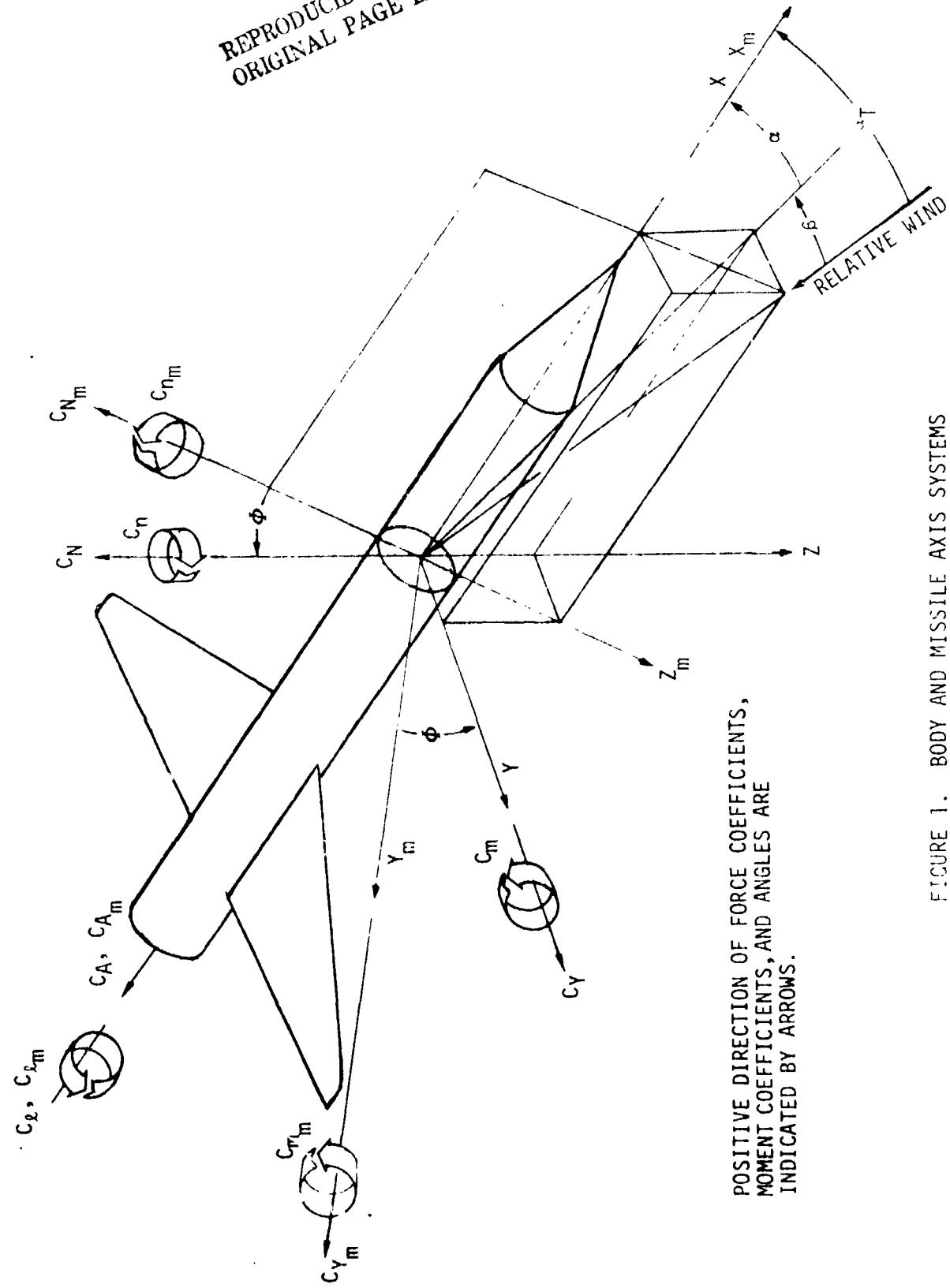
TABLE III. (Continued)

MODEL COMPONENT: ATTACH STRUCTUREGENERAL DESCRIPTION: AFT SRB/ET ATTACH STRUCTURE (3 MEMBERS, ET PORTION TESTED ONLY)MODEL SCALE = .006

DRAWING NUMBER: VL78-000062B

DIMENSIONS: (INCHES)	THEORETICAL		ACTUAL <u>MEASURED</u> MODEL SCALE
	FULL-SCALE	MODEL SCALE	
LOWER HORIZONTAL MEMBER			
X_T	<u>2052</u>	<u>12.312</u>	
Y_T	<u>+161.32</u>	<u>.968</u>	
Z_T	<u>-57</u>	<u>.342</u>	
DIAMETER	<u>5.5</u>	<u>.033</u>	
UPPER HORIZONTAL MEMBER			
X_T	2052	12.312	
Y_T	+161.32	.968	
Z_T	<u>57</u>	<u>.342</u>	
DIAMETER	<u>5.5</u>	<u>.033</u>	
UPPER VERTICAL MEMBER			
X_T	2052	12.312	
Y_T	<u>+161.32</u>	<u>.968</u>	
Z_T	57	.342	
DIAMETER	5.5	.033	

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POSITIVE DIRECTION OF FORCE COEFFICIENTS,
MOMENT COEFFICIENTS, AND ANGLES ARE
INDICATED BY ARROWS.

FIGURE 1. BODY AND MISSILE AXIS SYSTEMS

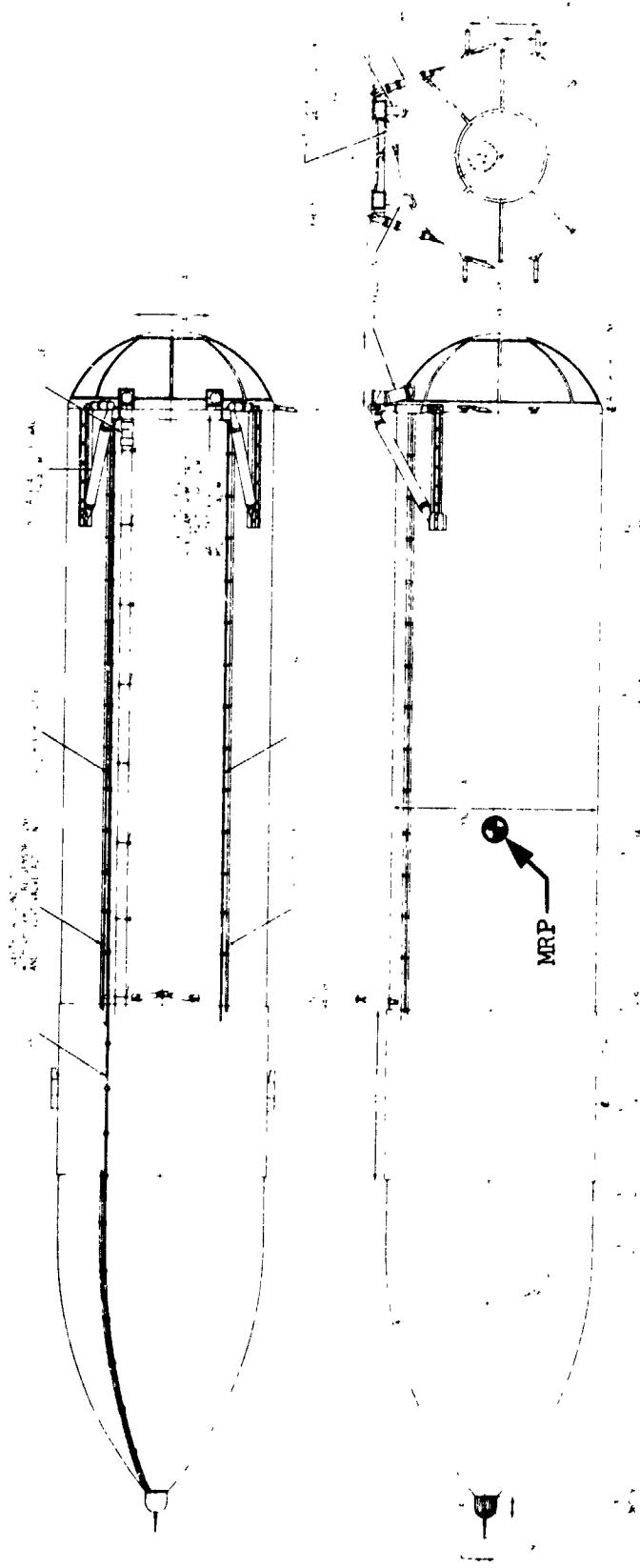


FIGURE 2a. CONFIGURATION DEFINITION FROM ROCKWELL DRAWING VL78-000062B

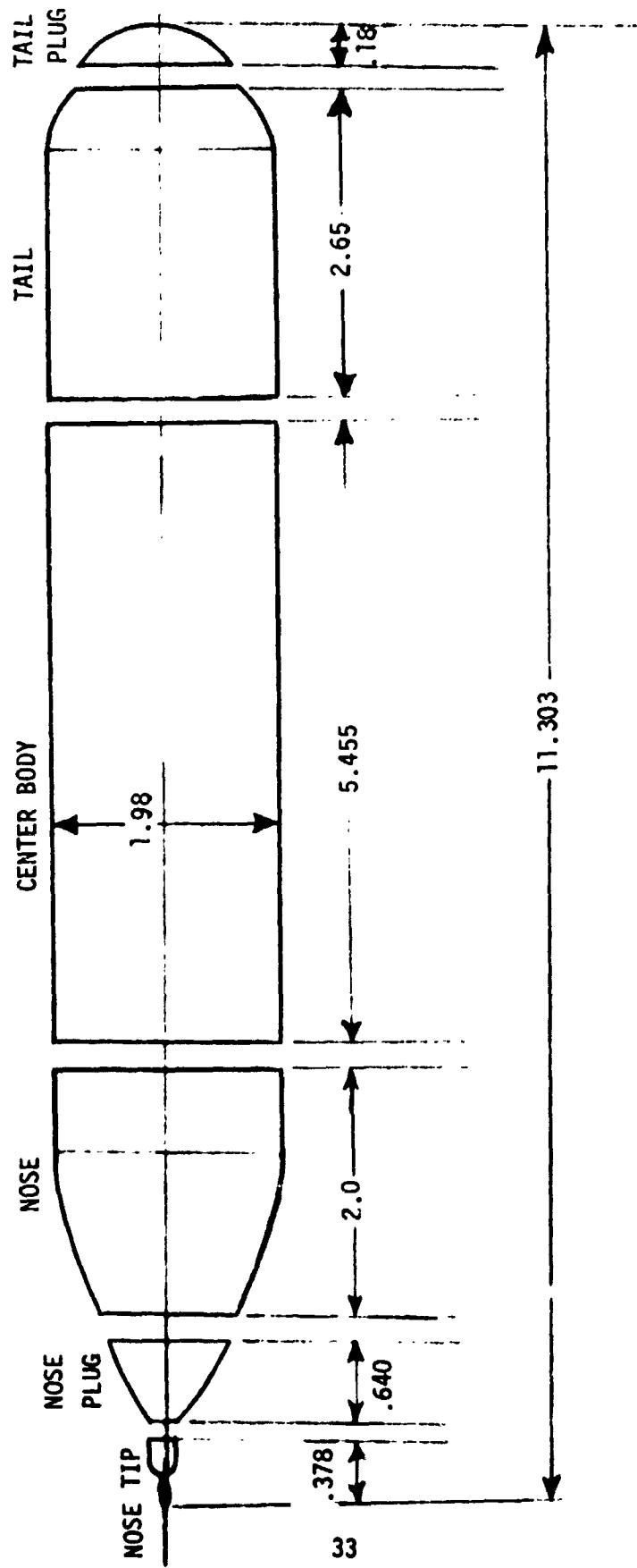
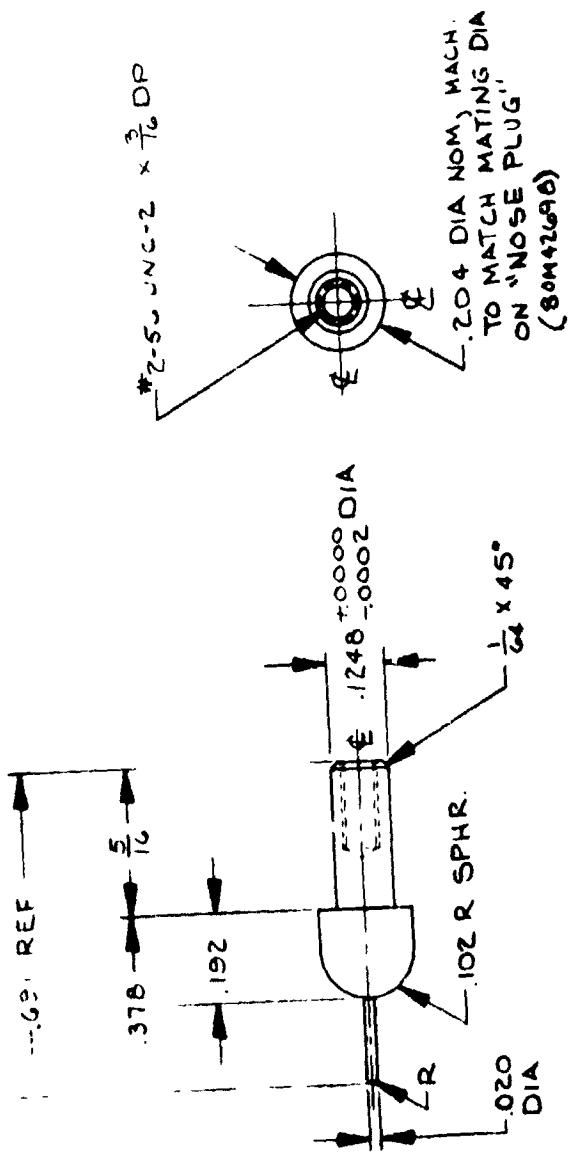


FIGURE 2b. SIC EL PARTS AND DI NSI S

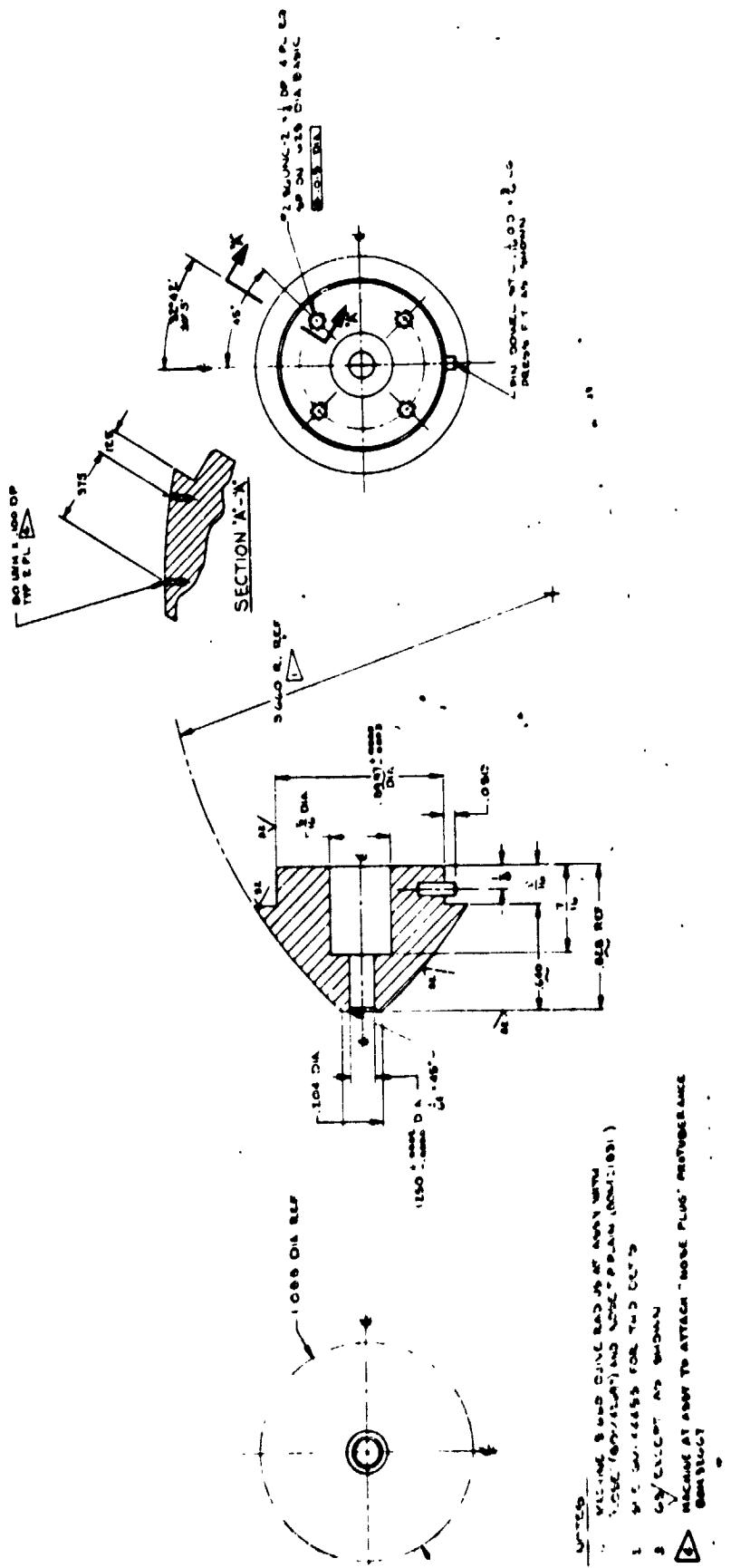


NOTES:

1. 32/
2. SEE GM444455 FOR THD DET'S.

F1 2c. L NOSE TIP

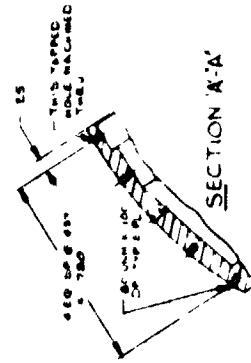
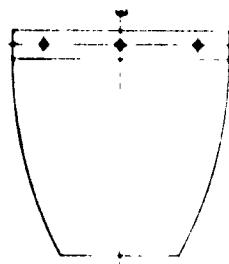
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ORIGINAL P



FR 2d. L SE PL

NOTES

1. SEE 3444485 FOR THE DET.
2. SEE 3444485 FOR THE DET.
3. THE 1950 MA. MUST BE DENTED IN HAVING A CENTER HOLE 3/4" IN DIAMETER WITH NO SLOTS.
4. HAVING 3 SLOTS ON THE 2 AT AN ANGLE OF 120° EACH.
5. HAVING 3 HOLES PLUGS 3/4" IN DIAMETER.
6. TIP FLANGE BOWEL IN.
7. WATCH ATT ASSEMBLY ATTACHMENT. SEE PRT. DIFFERENCE IN DIMENSIONS.



SECTION K-K'

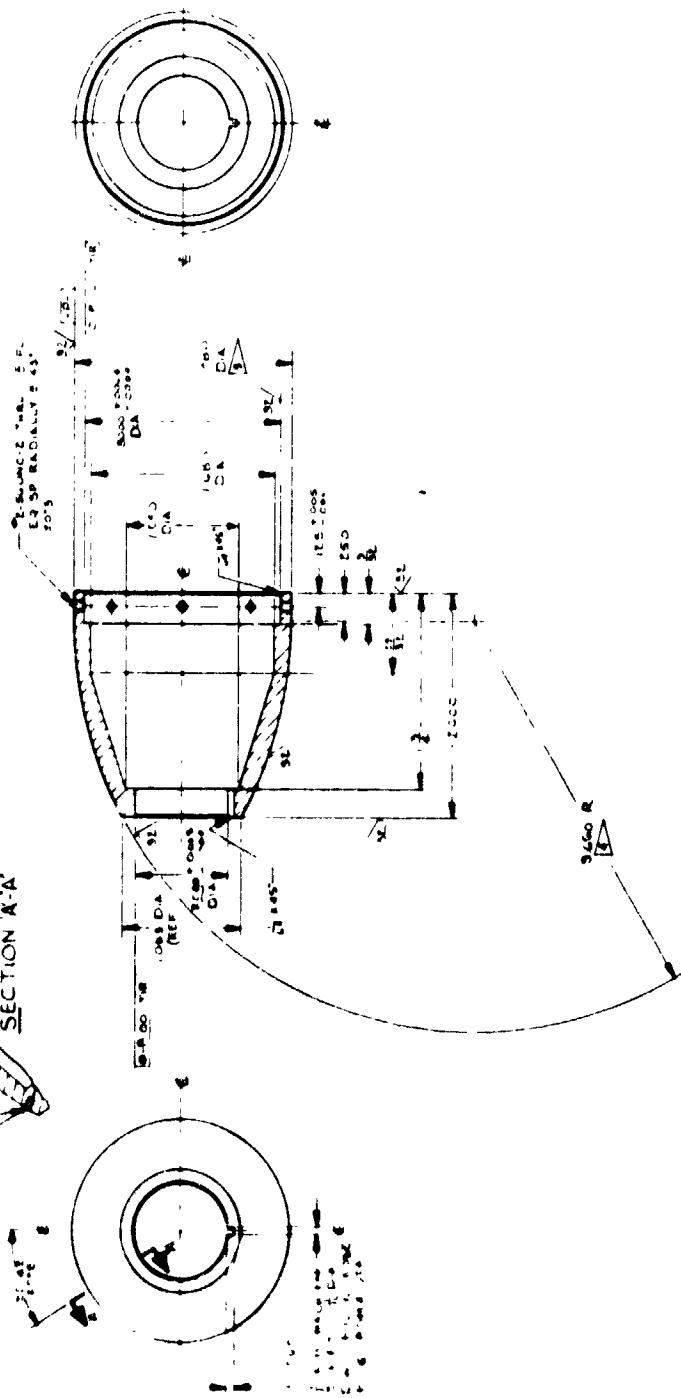
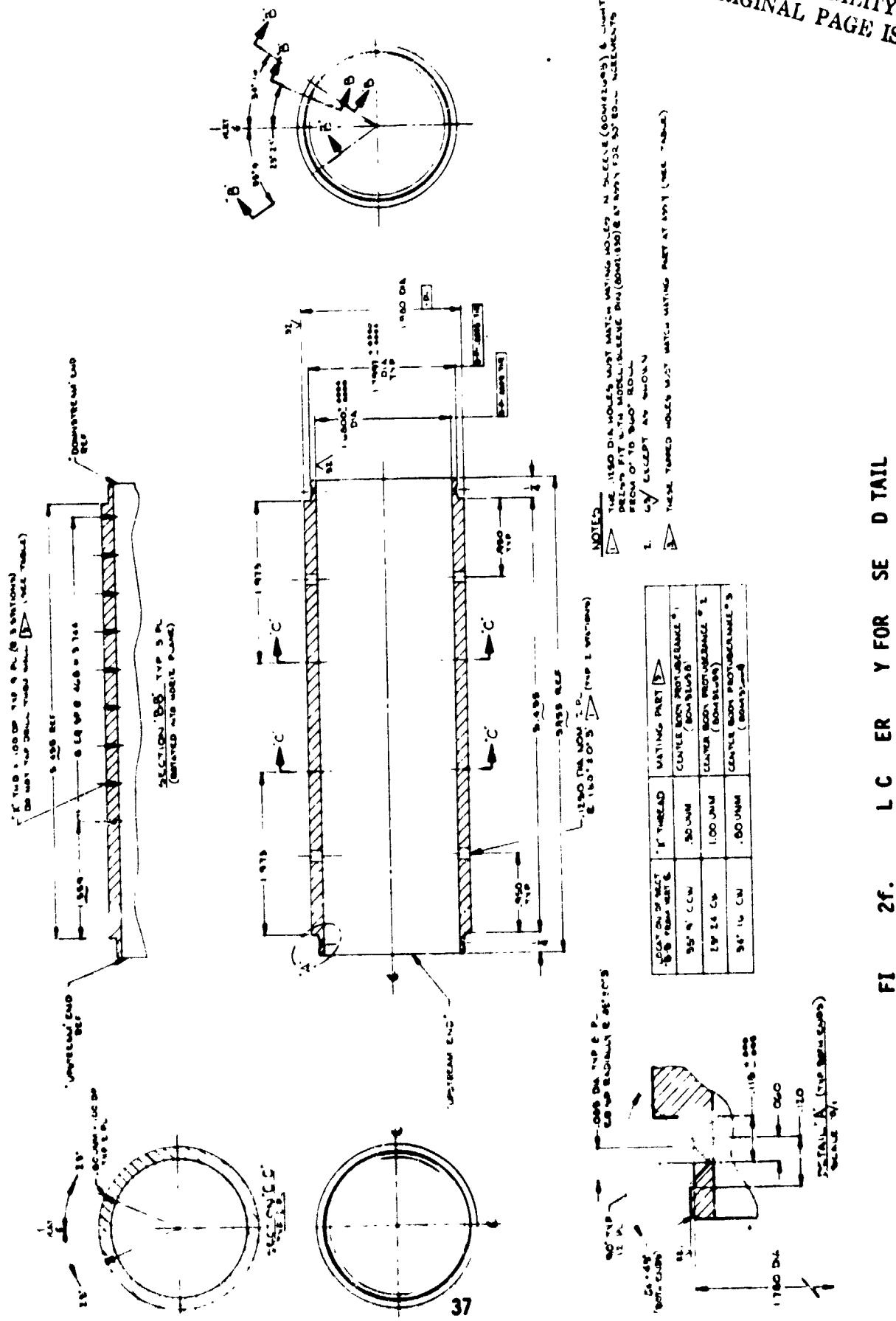


FIG. 2e. DEL NOSE

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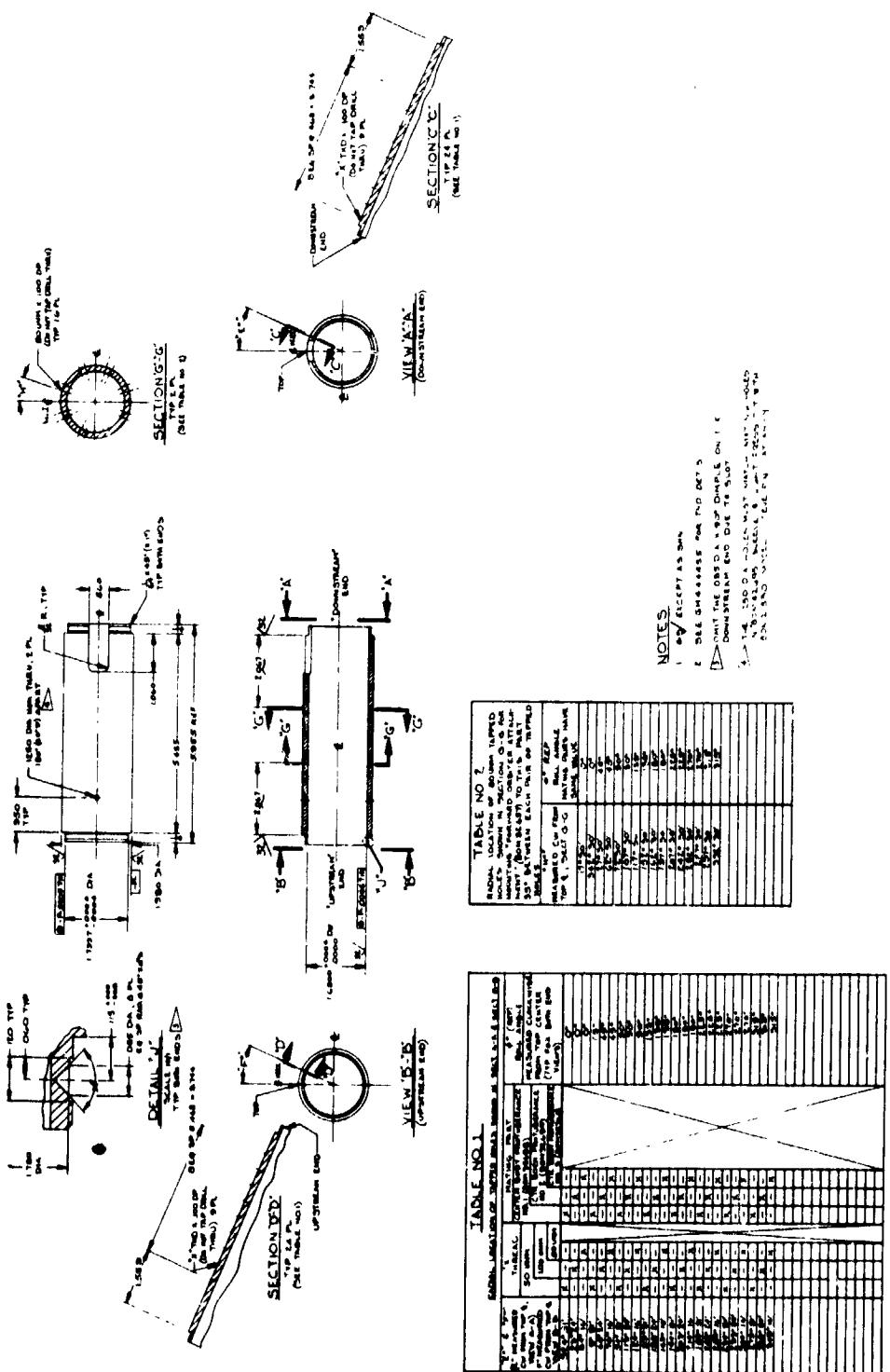


FIGURE 2g. MODEL CENTER BODY FOR SIDE MOUNT

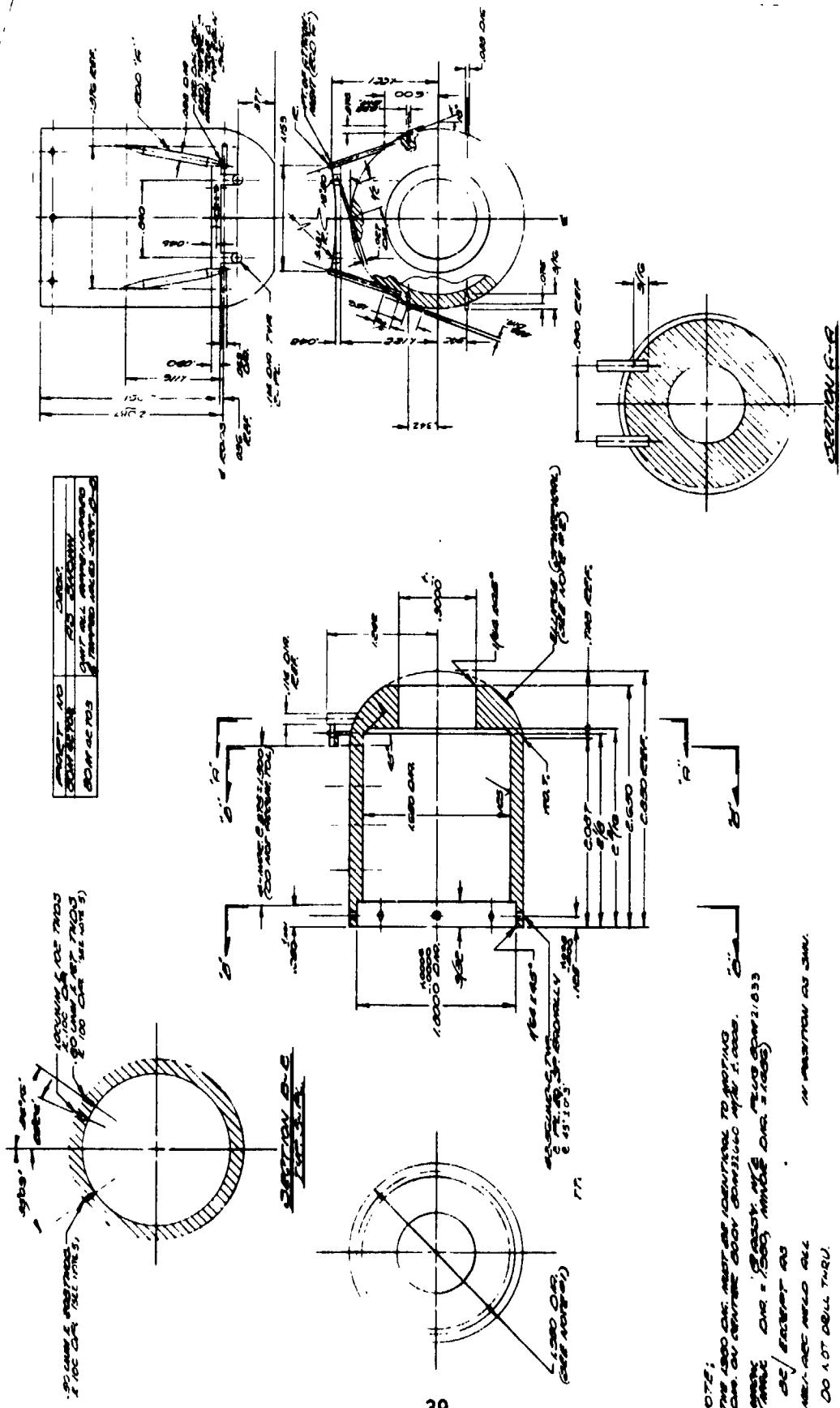


FIGURE 2h. DEL BASE

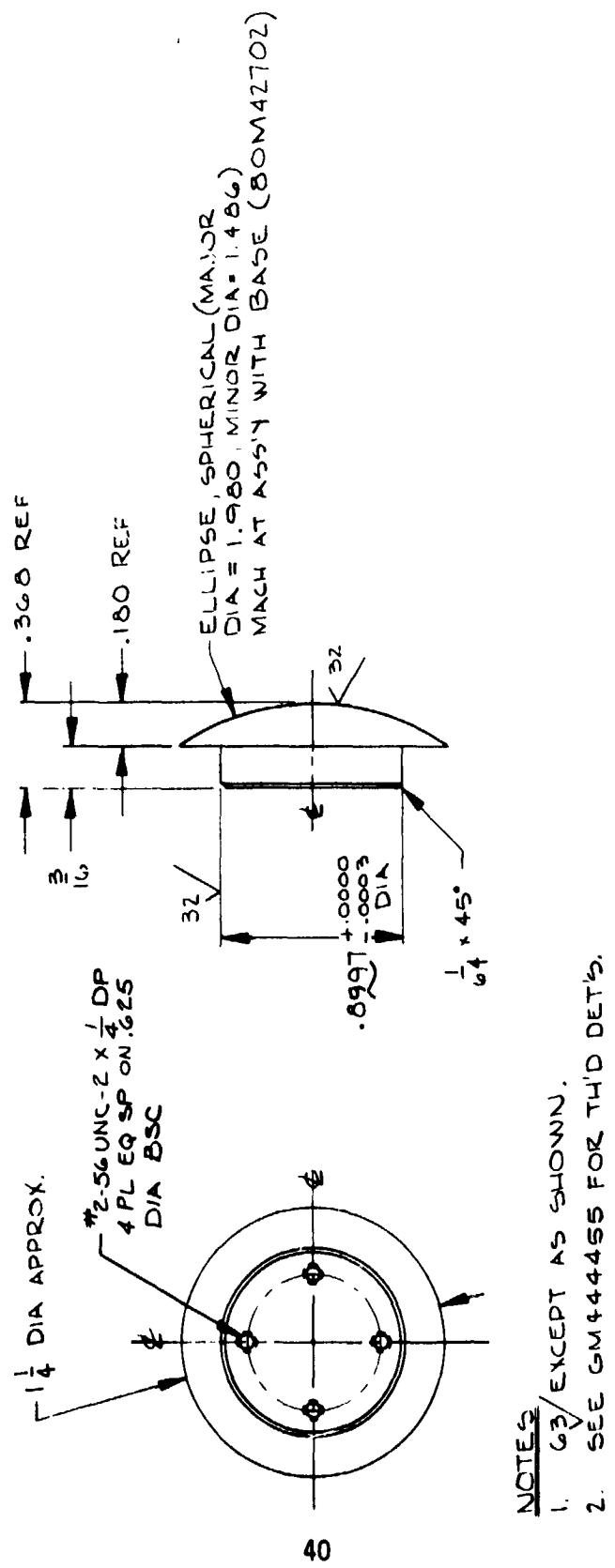
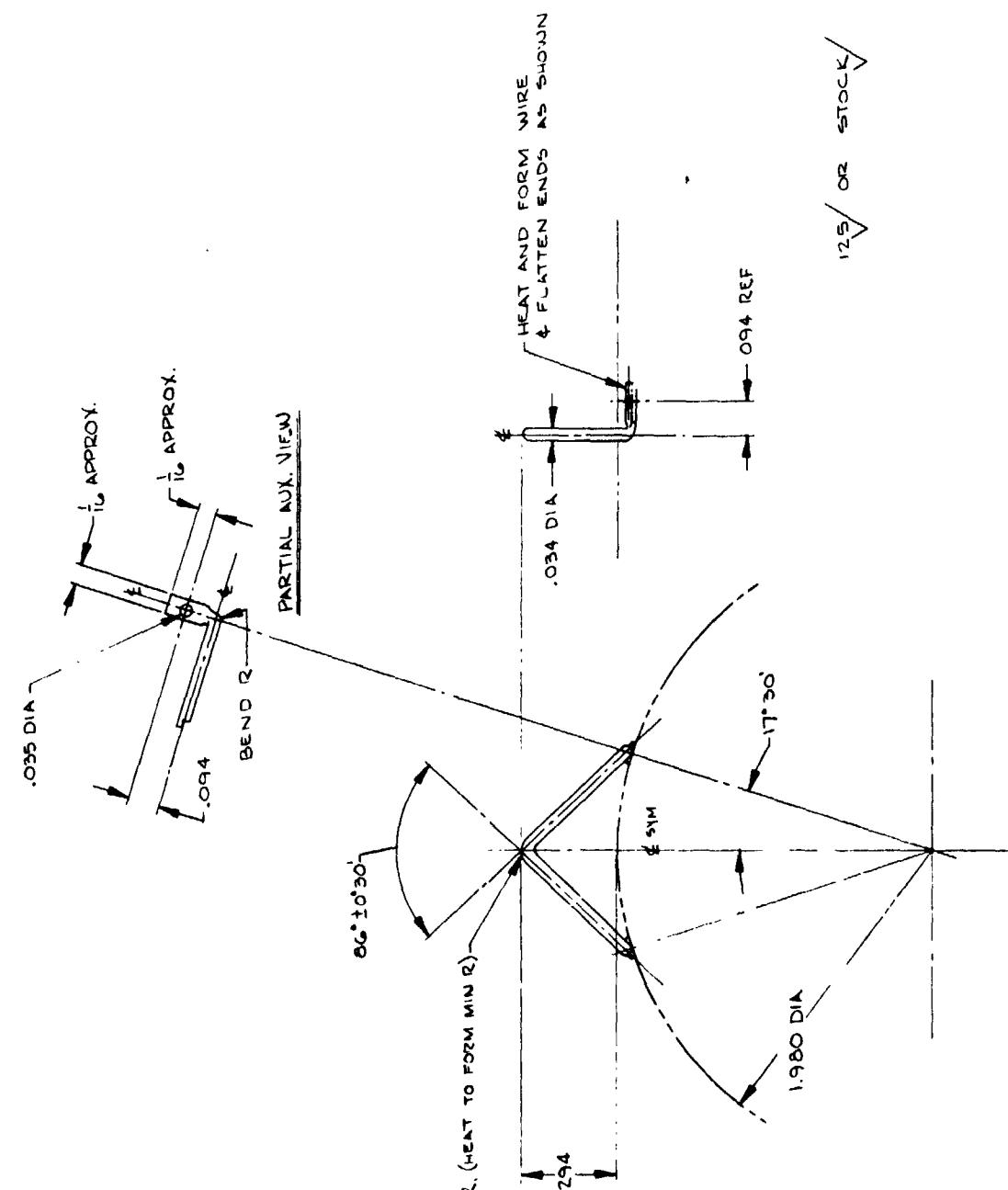


FIGURE 2i. MODEL BASE PLUG



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FIGURE 2j. FOR RD ORBITER ATTACH HARDWARE

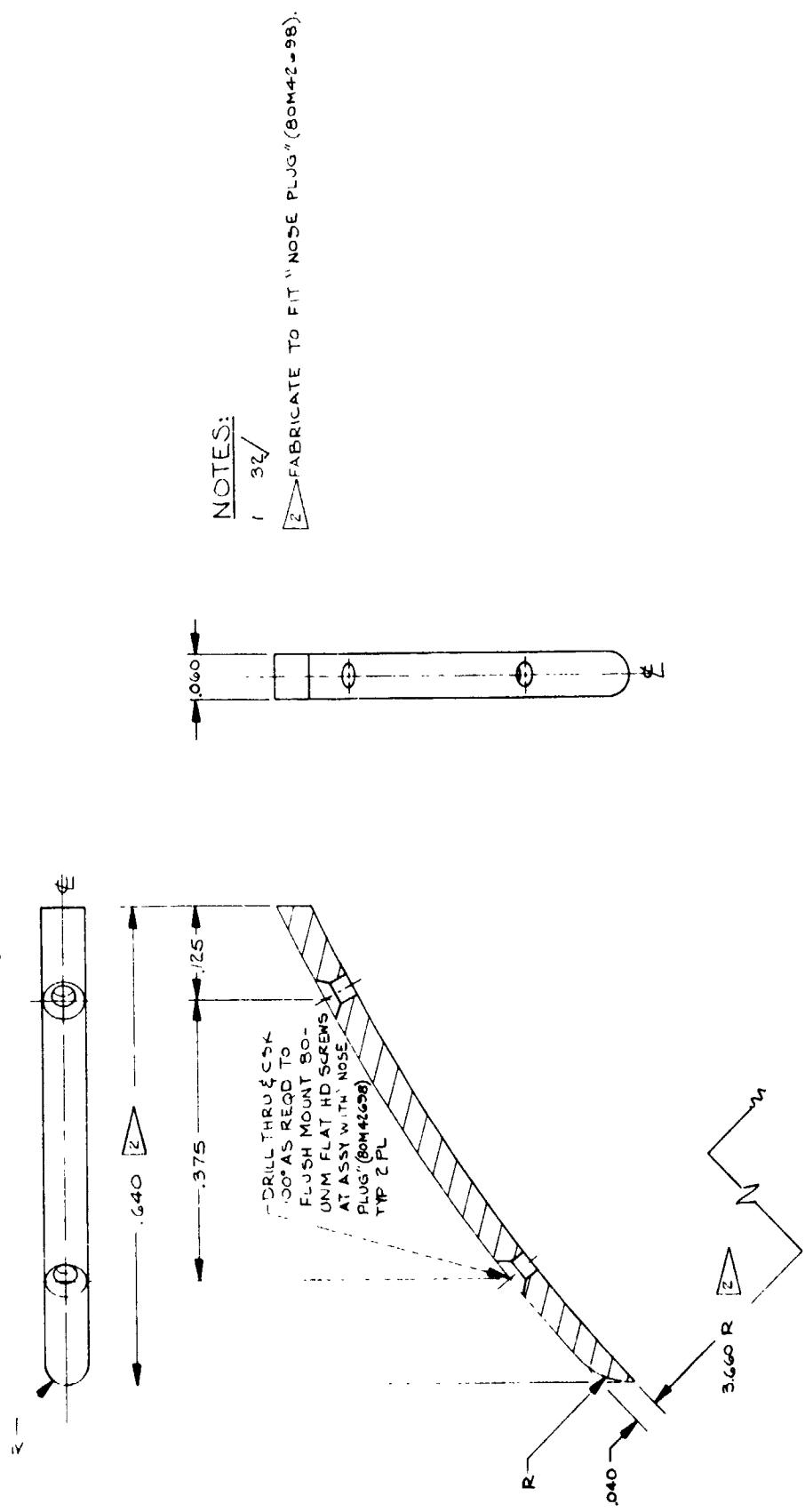


FIGURE 2k. ELECTRICAL CONDUIT NOSE PLUG PROTUBERANCE

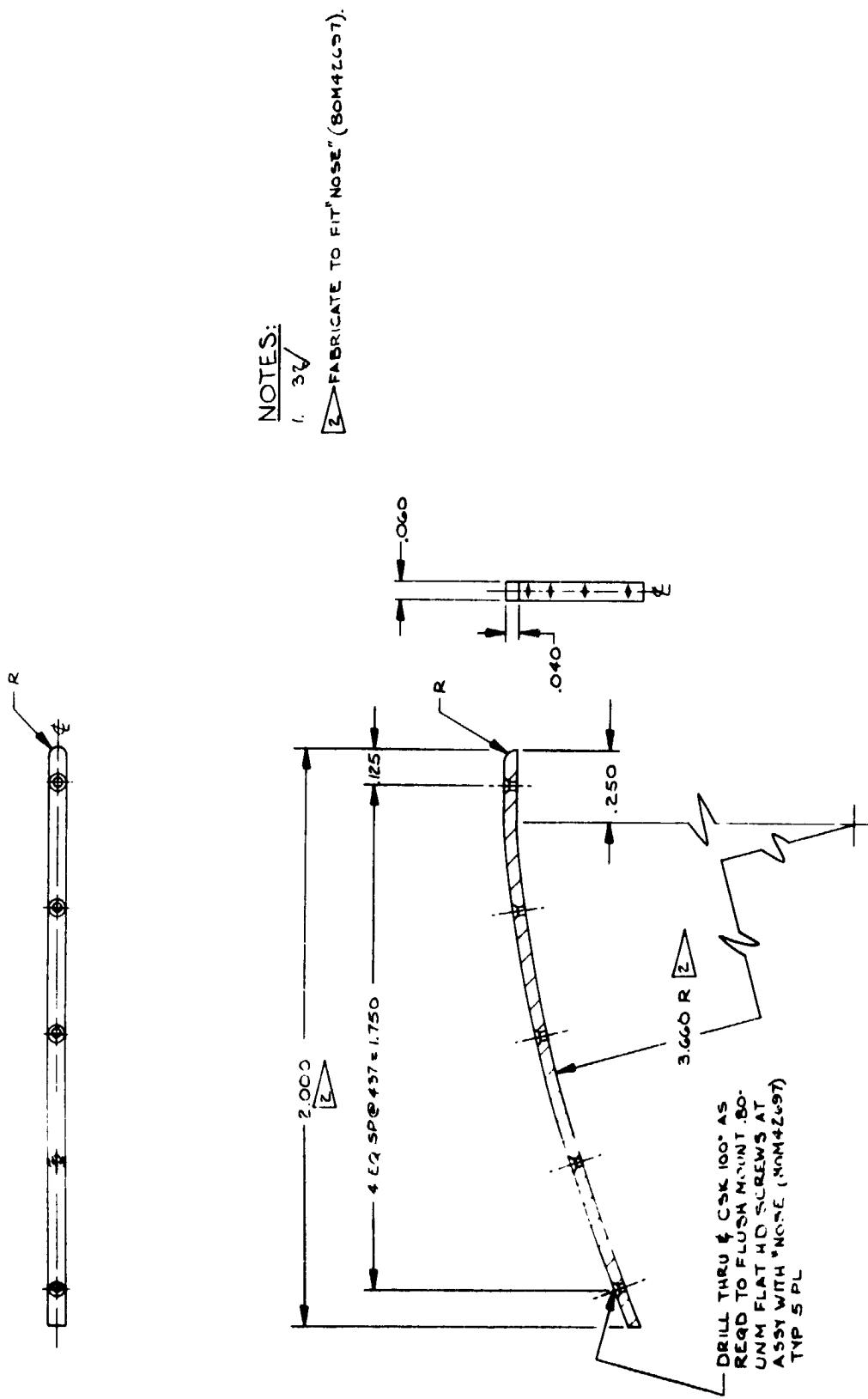


FIGURE 21. ELECTRICAL CONDUIT NOSE PROTOTYPE CE

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

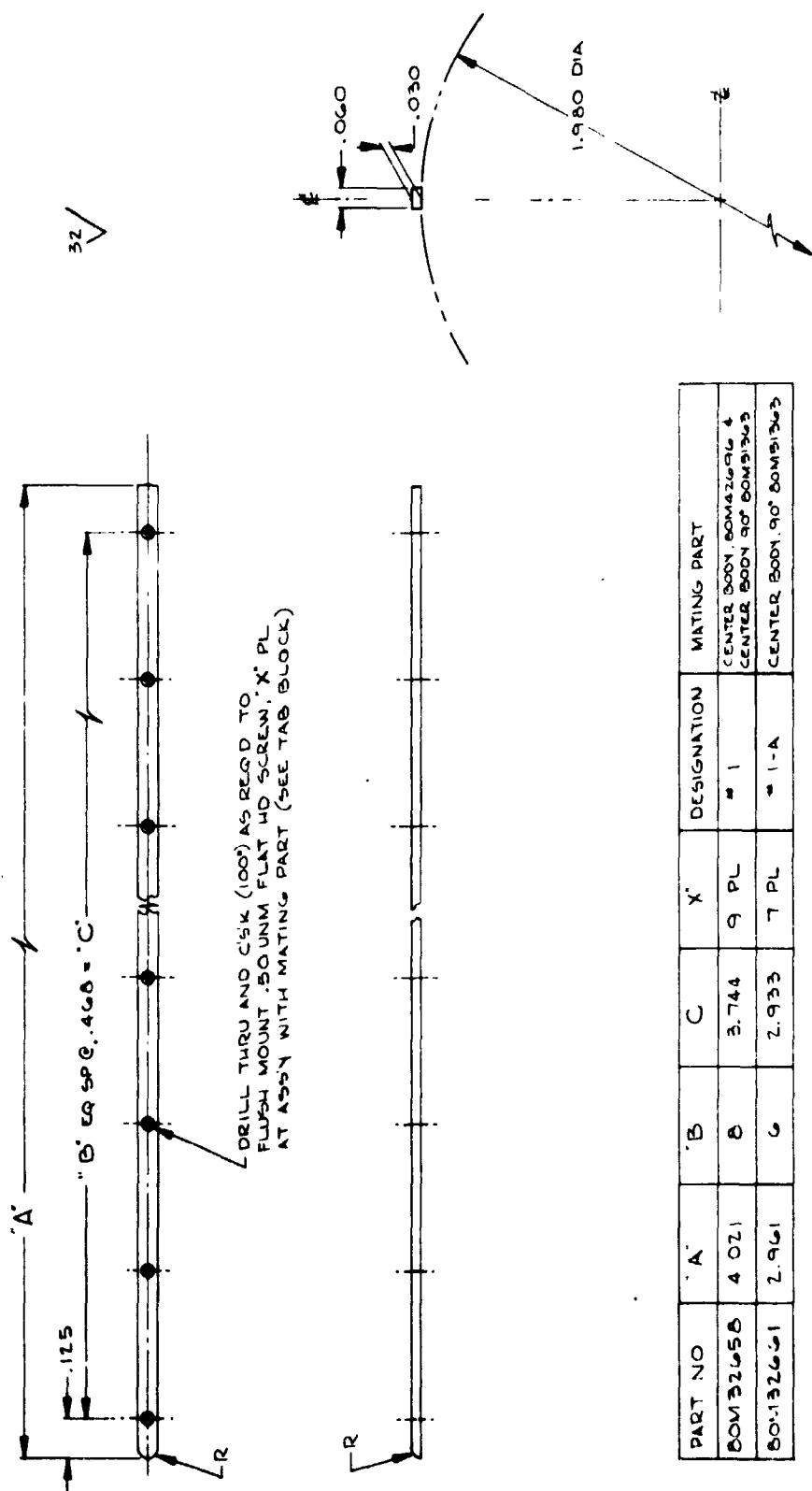


FIGURE 2m. LH₂ PRESSURE LINE PROTUBERANCE

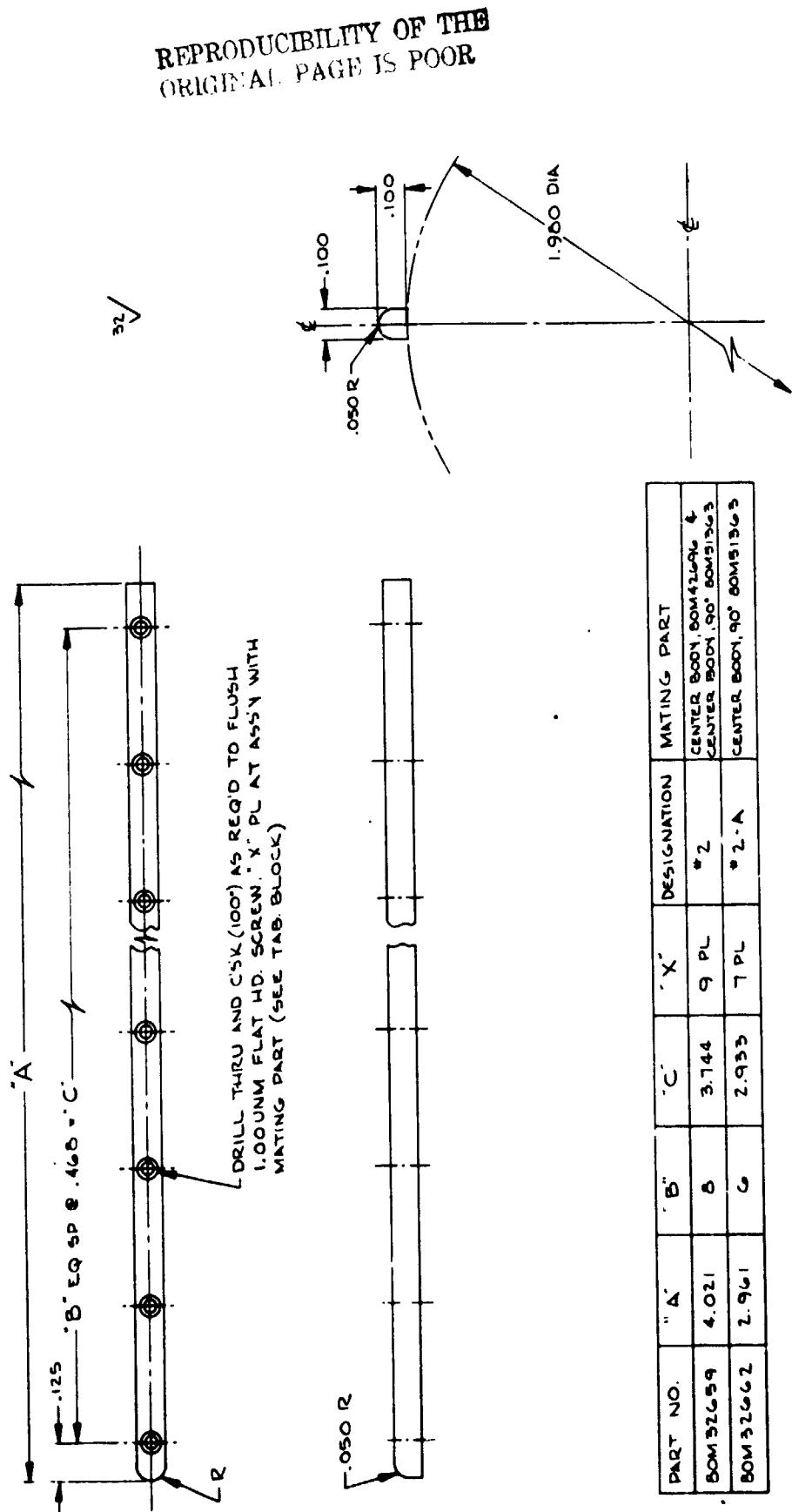
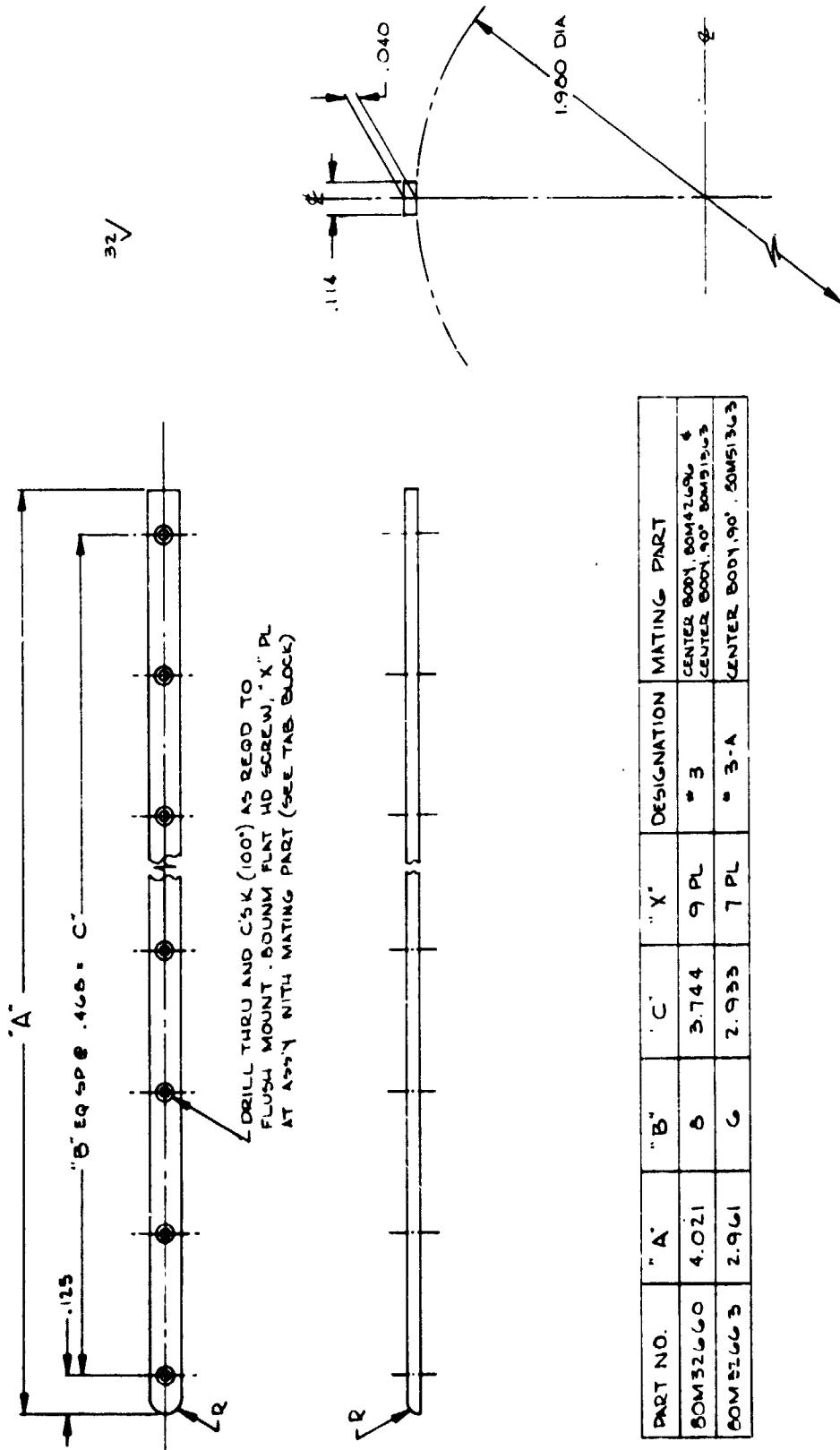
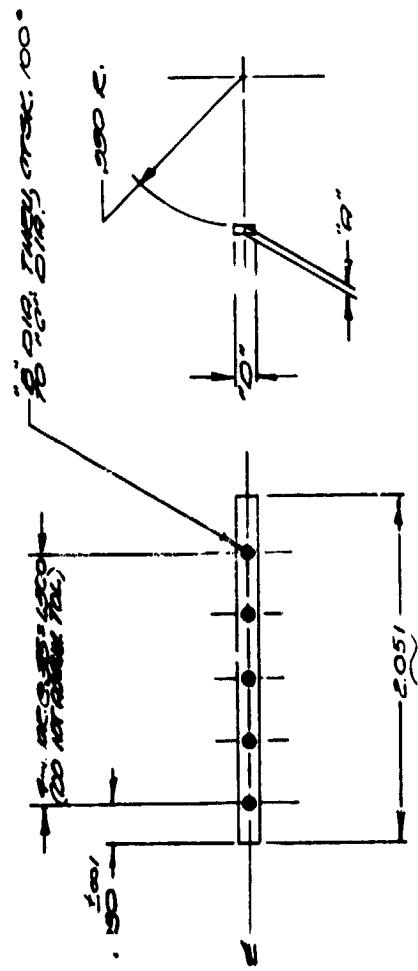


FIGURE 2n. LO₂ FEED LINE PROTURE CE



F1 20. LO₂ PRESSURE LINE, LO₂ RECIRCULATI LINE AND ELECTRICAL CONDUIT PROTUBE CE



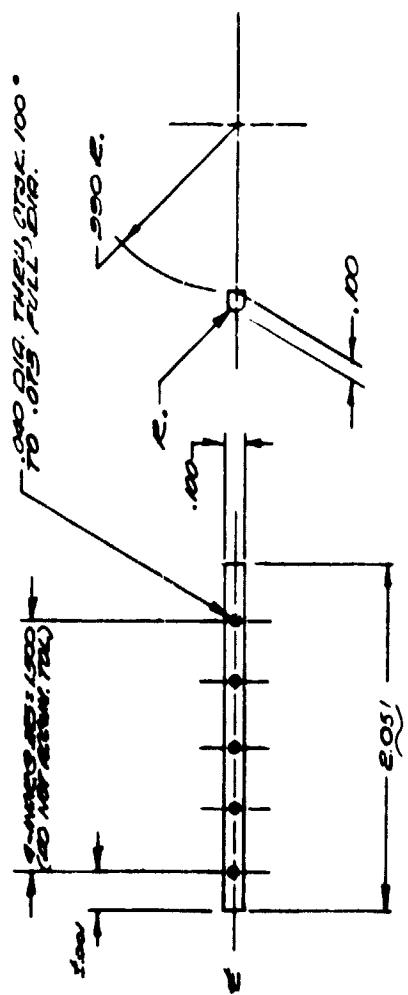
200	200	200	200	200	200	200
200	200	200	200	200	200	200
200	200	200	200	200	200	200
200	200	200	200	200	200	200

✓

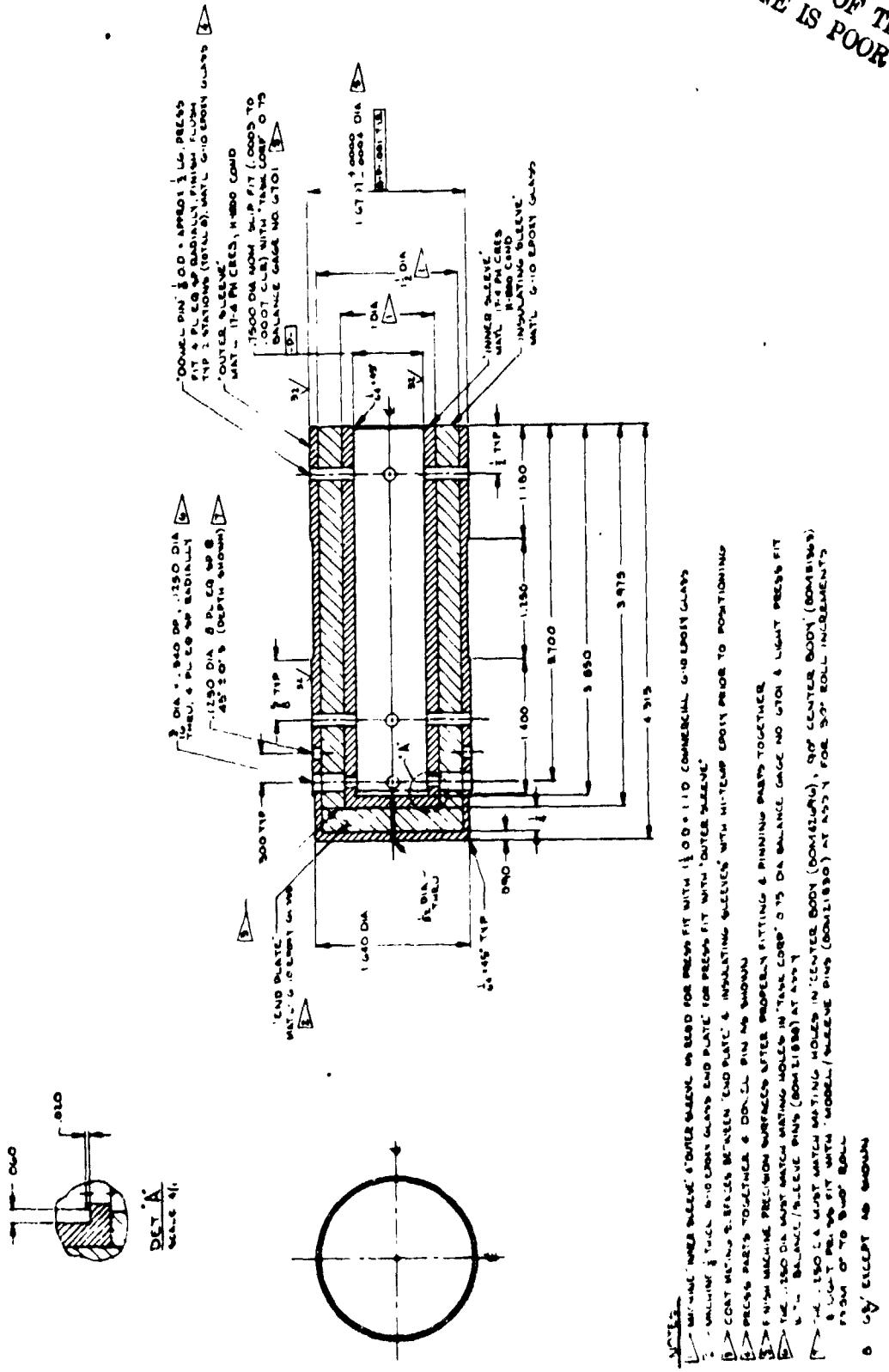
FI 2p. LH2 P S LINE P TUBE E D LO2 PRESSURE LINE,
LO2 CIRCULATING LINE D ELECTRICAL C IR PROTUBE CE

F1 2q. E P TION OF LO₂ FEED LINE PROTUBE CE

2c/

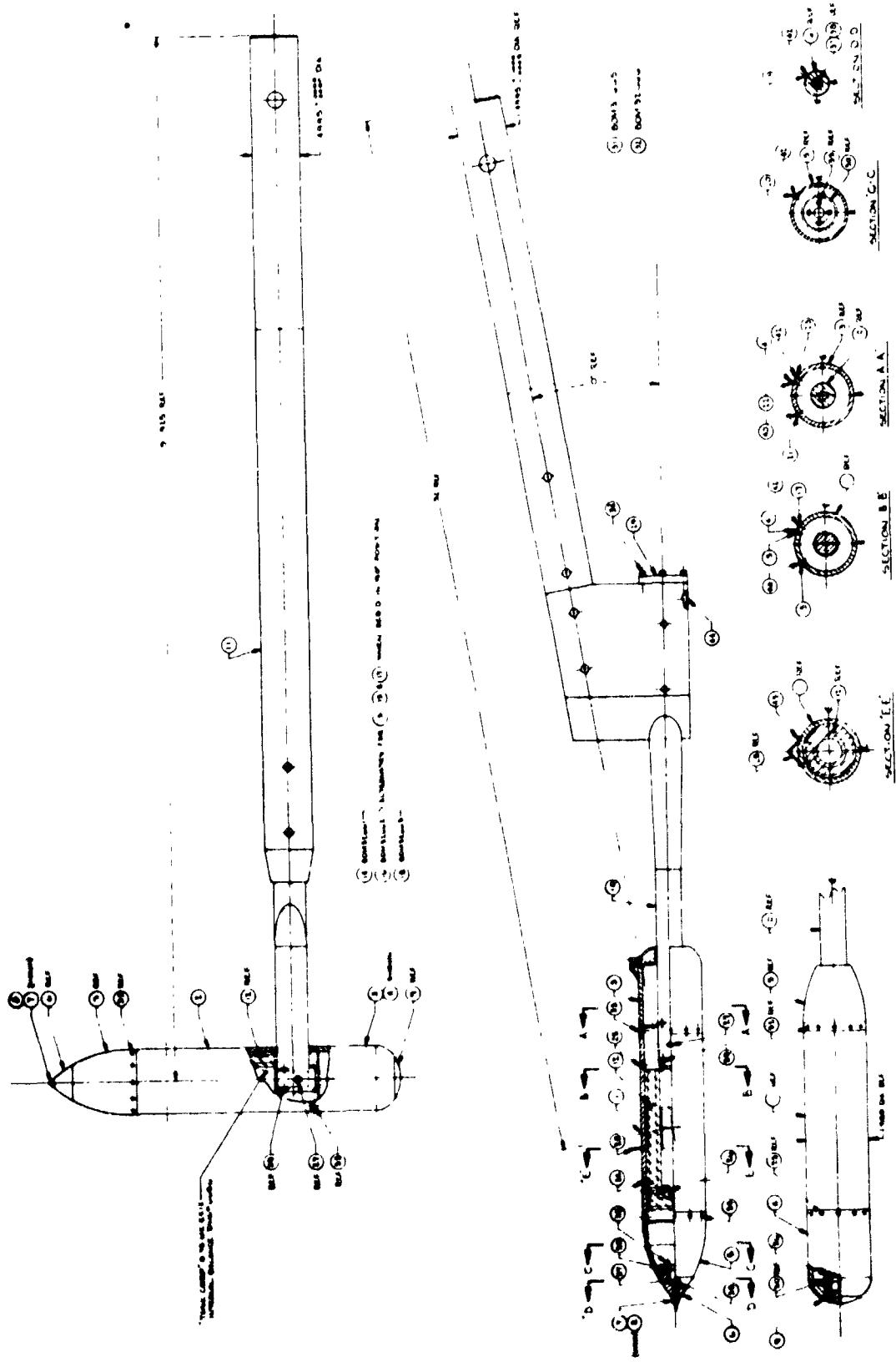


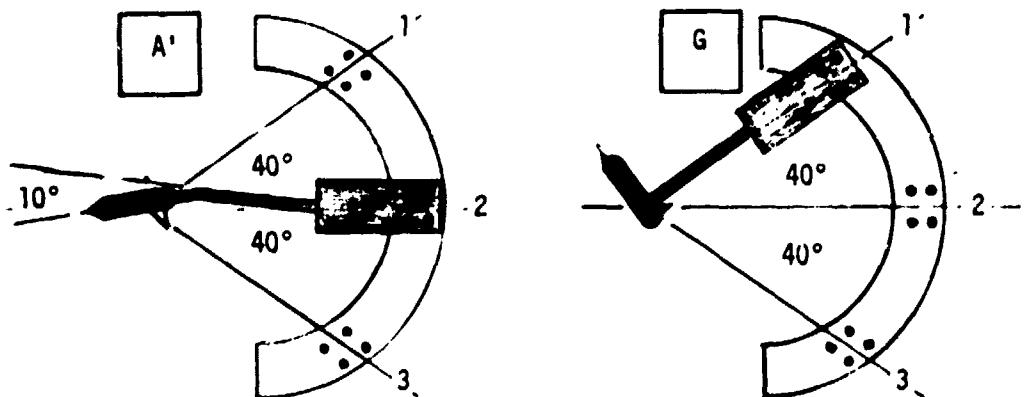
REPRODUCIBILITY OF THE
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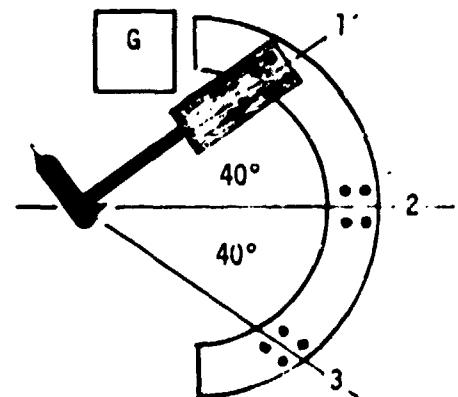
F1 2r. INSULATING SLEEVE

FIG. 25. DELASSELY ING

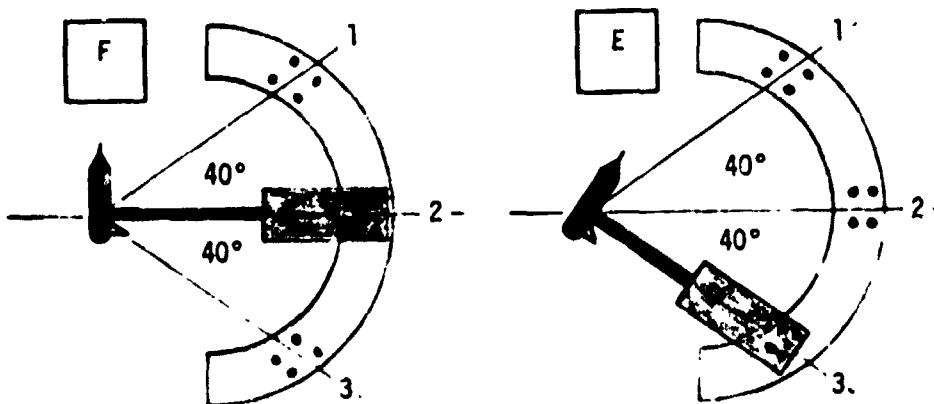




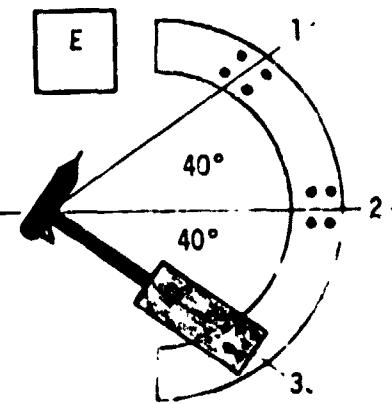
$\alpha = -5^\circ \text{ to } 30^\circ$



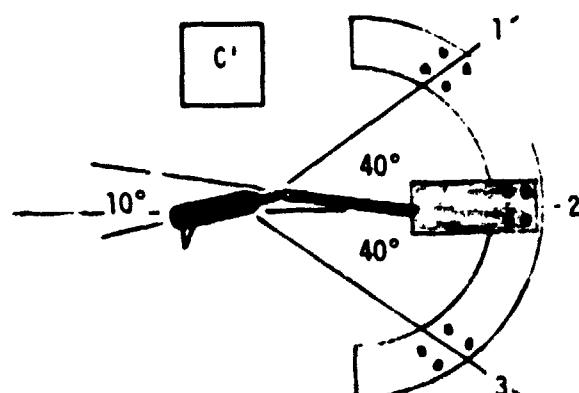
$\alpha = 30^\circ \text{ to } 65^\circ$



$\alpha = 70^\circ \text{ to } 105^\circ$



$\alpha = 110^\circ \text{ to } 145^\circ$



$\alpha = 150^\circ \text{ to } 185^\circ$

FIG. 2t. STRUT DROPPING POSITIONS FOR LE-OF-ATTACK S

FIGURE 3a. TYPICAL TUNNEL INSTALLATION WITH MODEL MOUNTED FROM THE NOSE



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U.S. AIR FORCE
AERONAUTICAL RESEARCH LABORATORY

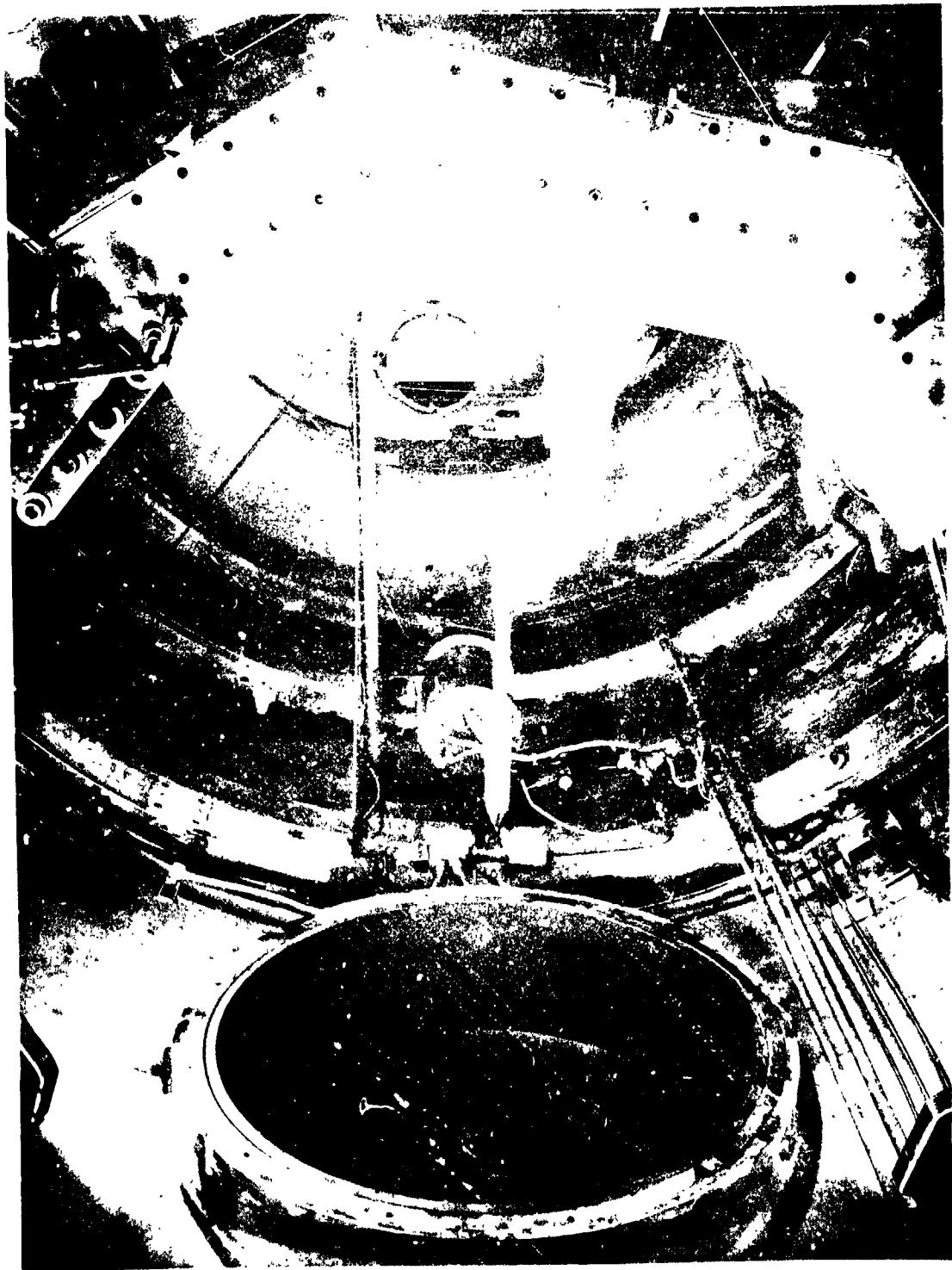


FIGURE 3b. TYPICAL TUNNEL INSTALLATION WITH MODEL MOUNTED FROM THE TAIL



FIGURE 3C. TYPICAL TUNNEL INSTALLATION WITH MODEL MOUNTED FROM THE SIDE

DATA FIGURES

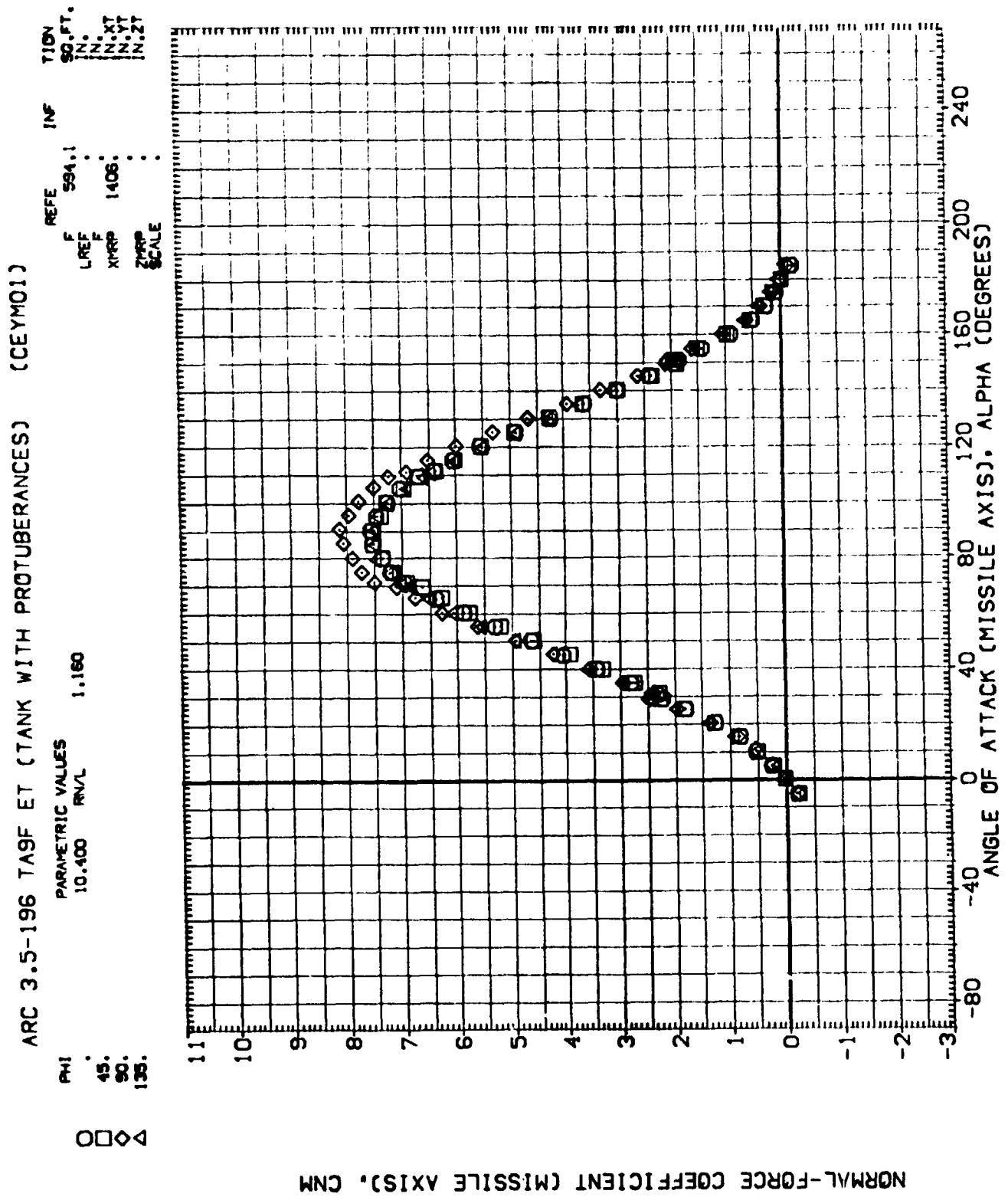


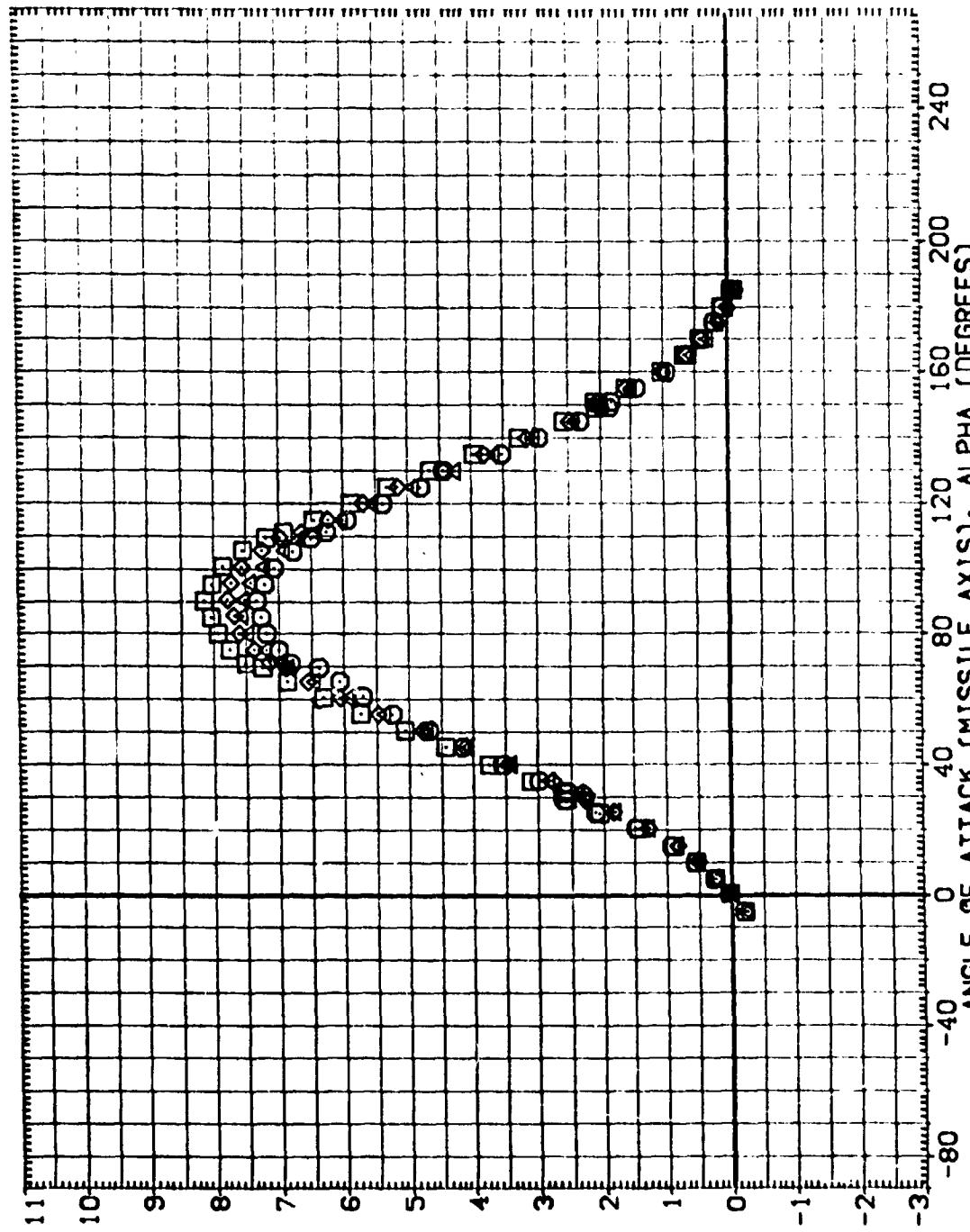
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

PHI
180.
270.
315.

P_{TRIC} V S 1.160
LREF
BREF
270.
227.
227.

SCALE



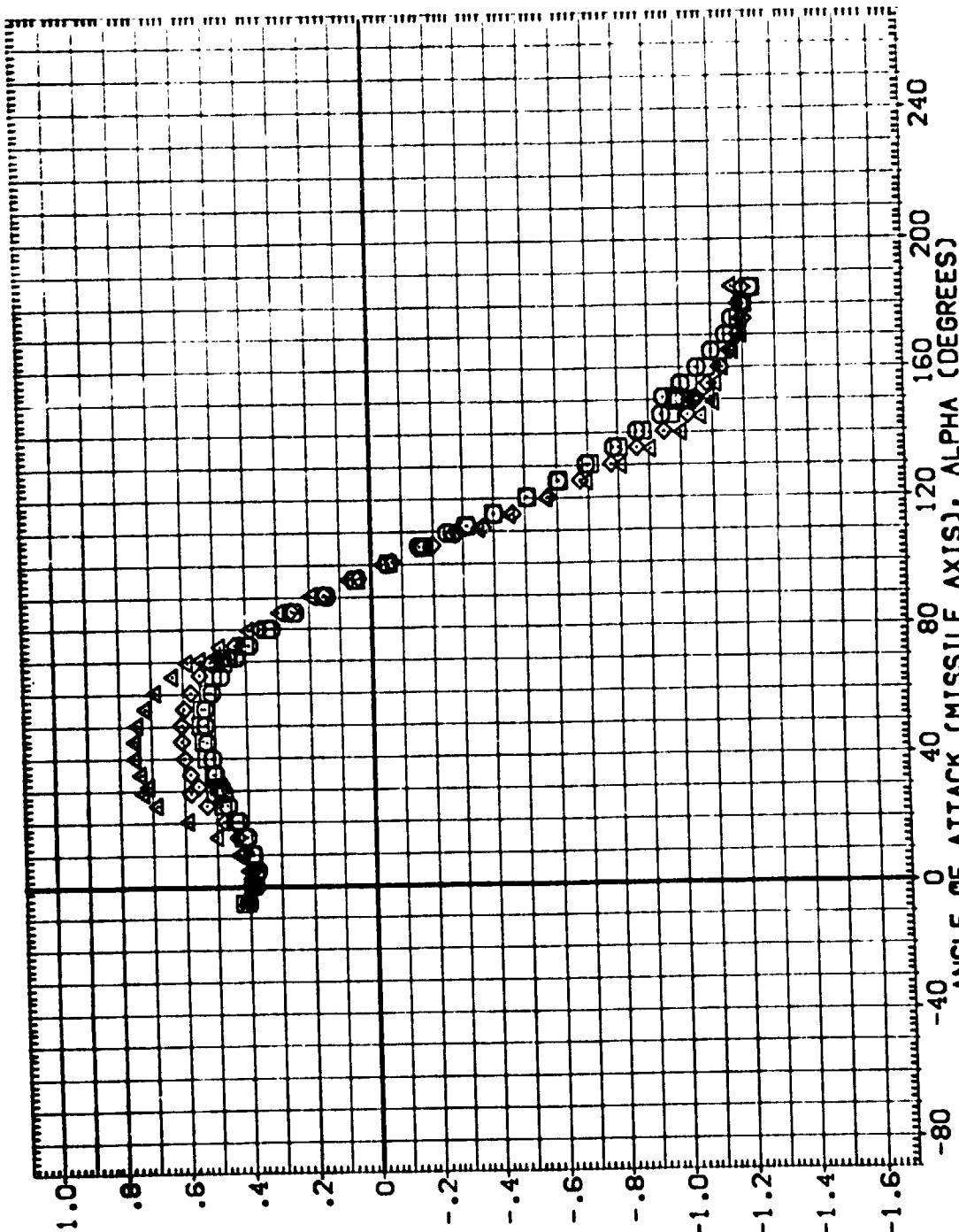
NORMAL-FORCE COEFFICIENT (MISSILE AXIS), C_N

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

PHI TRIC VALUES 1.160
 10.400
 45.
 90.
 135.
 O □ ◊ △

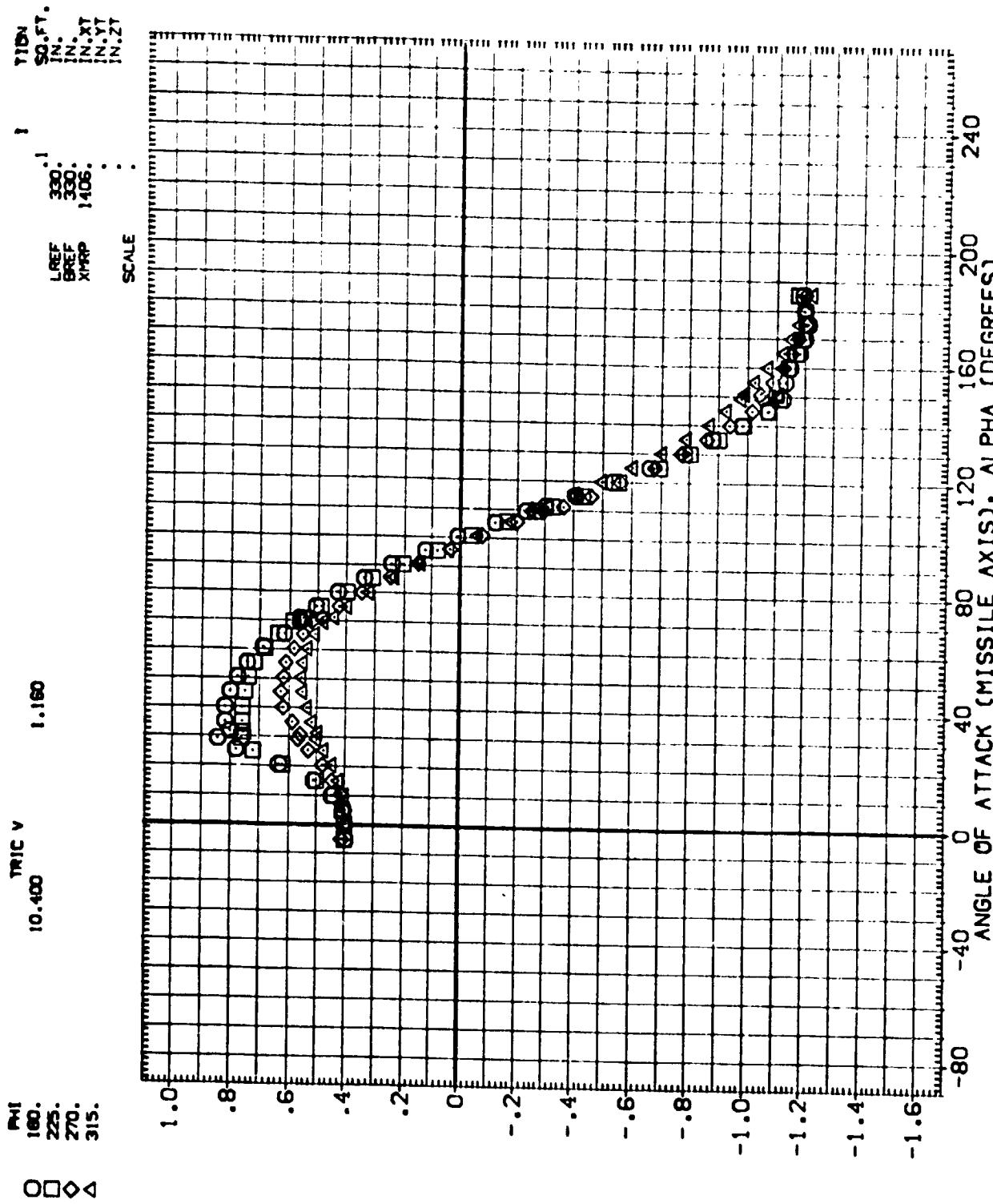
REFERENCE INFORMATION
 SREF 594.1
 LREF 330.
 BREF 330.
 XMRP 140.
 YMRP 140.
 ZMRP 140.
 SCALE



AXIAL FORCE COEFFICIENT (MISSILE AXIS).

FIG. 4 COEFFICIENTS VERS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTECTIONS) (CEYMO1)



AXIAL FORCE COEFFICIENT (MISSILE AXIS), CA

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

POLAR TRIC VALUES
10,400 RNDL 1.160
45.
90.
135.

○ □ ◇ △

PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLMM

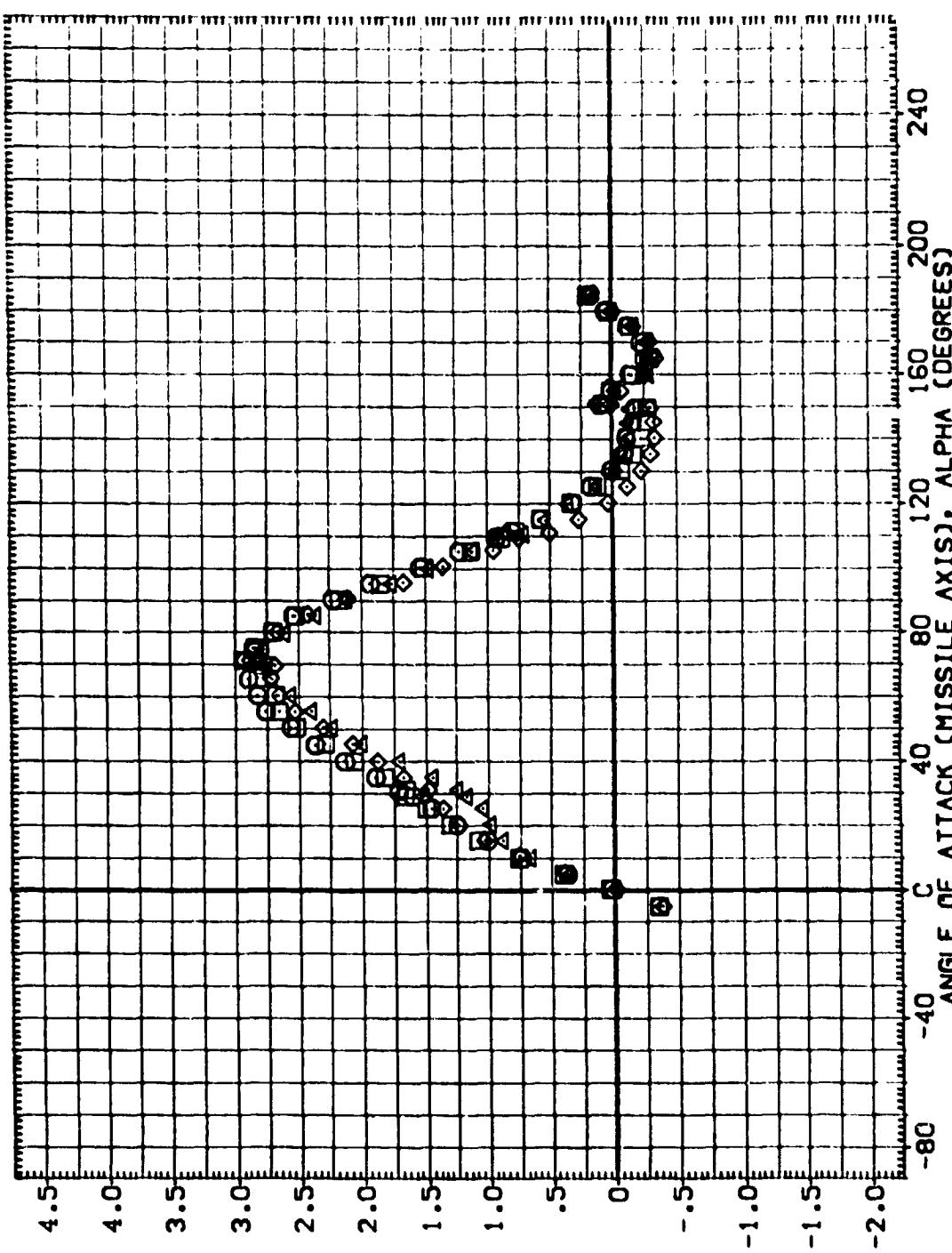


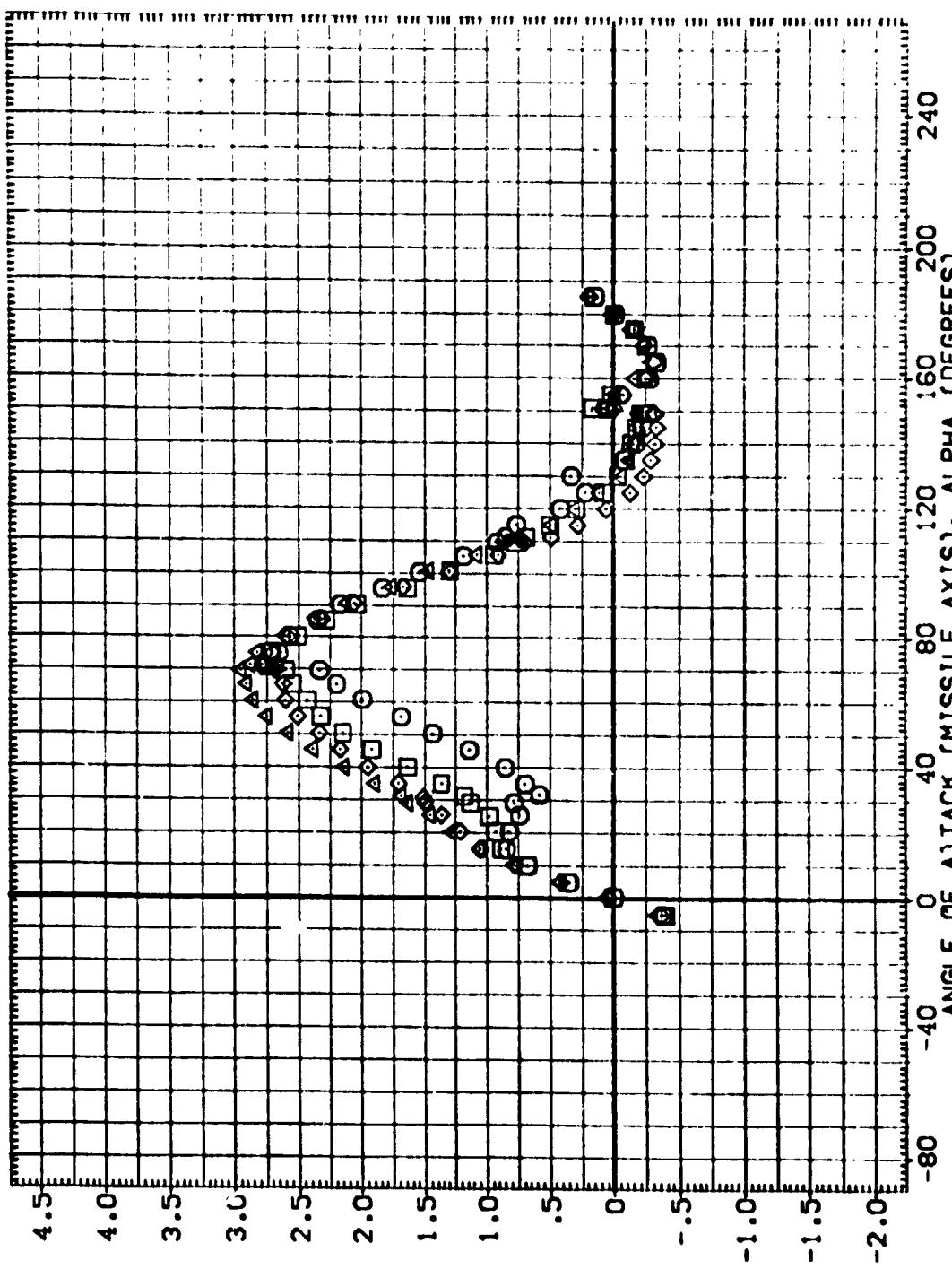
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-1 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

RH 100 .
10. 10. 1.100
315. .
O□◊△

L_{REF} 594.1
1406.
IN. 300.
IN. XT
IN. YT
IN. ZT

1100
80 FT.



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CL/MM

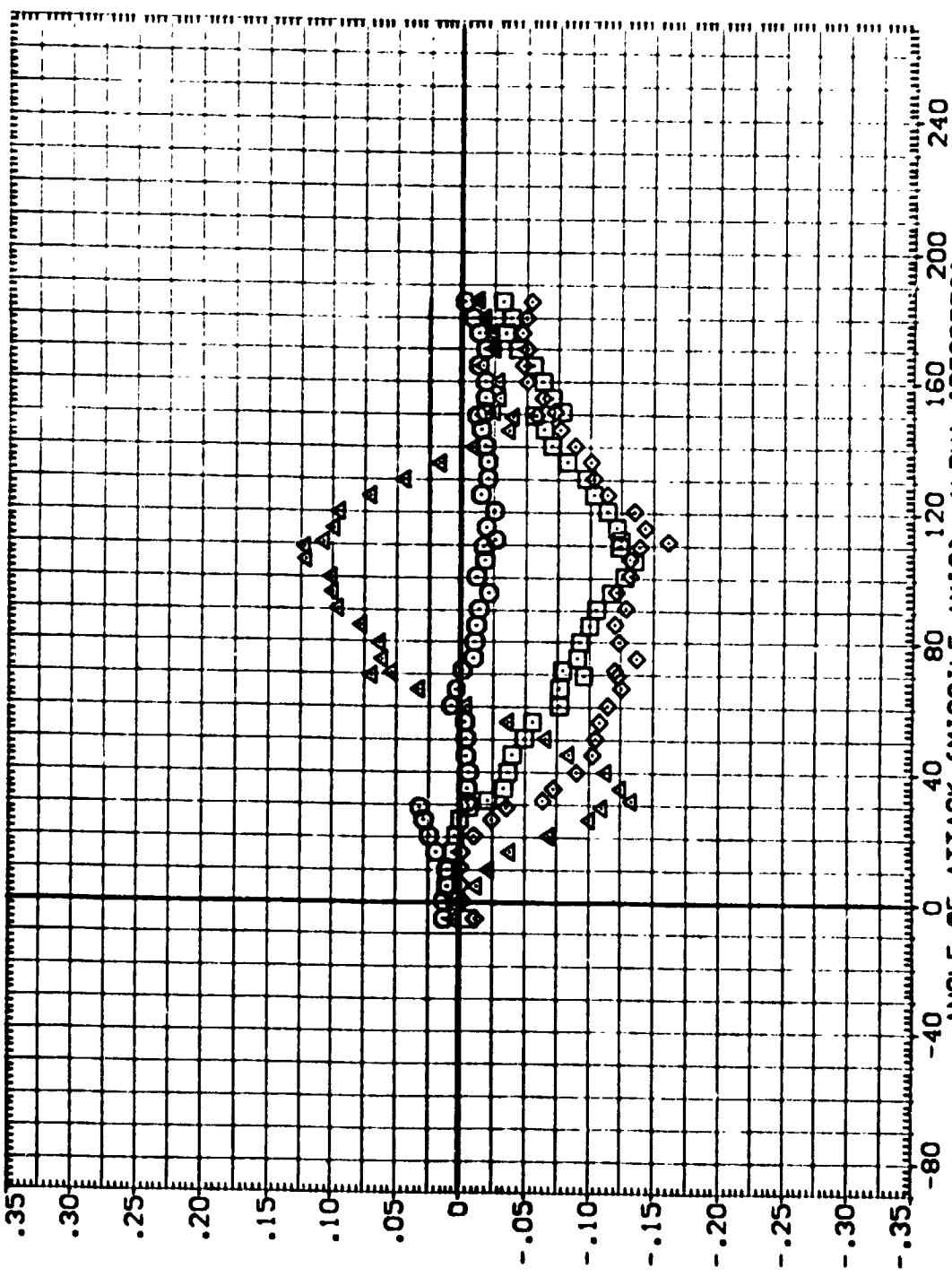
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

P_{TRIC V}
10.100 1.100
45.
90.
135.
0□◊△

REF.
LREF.
BREF.
XMP.
SCALE

REF.
LREF.
BREF.
XMP.
SCALE



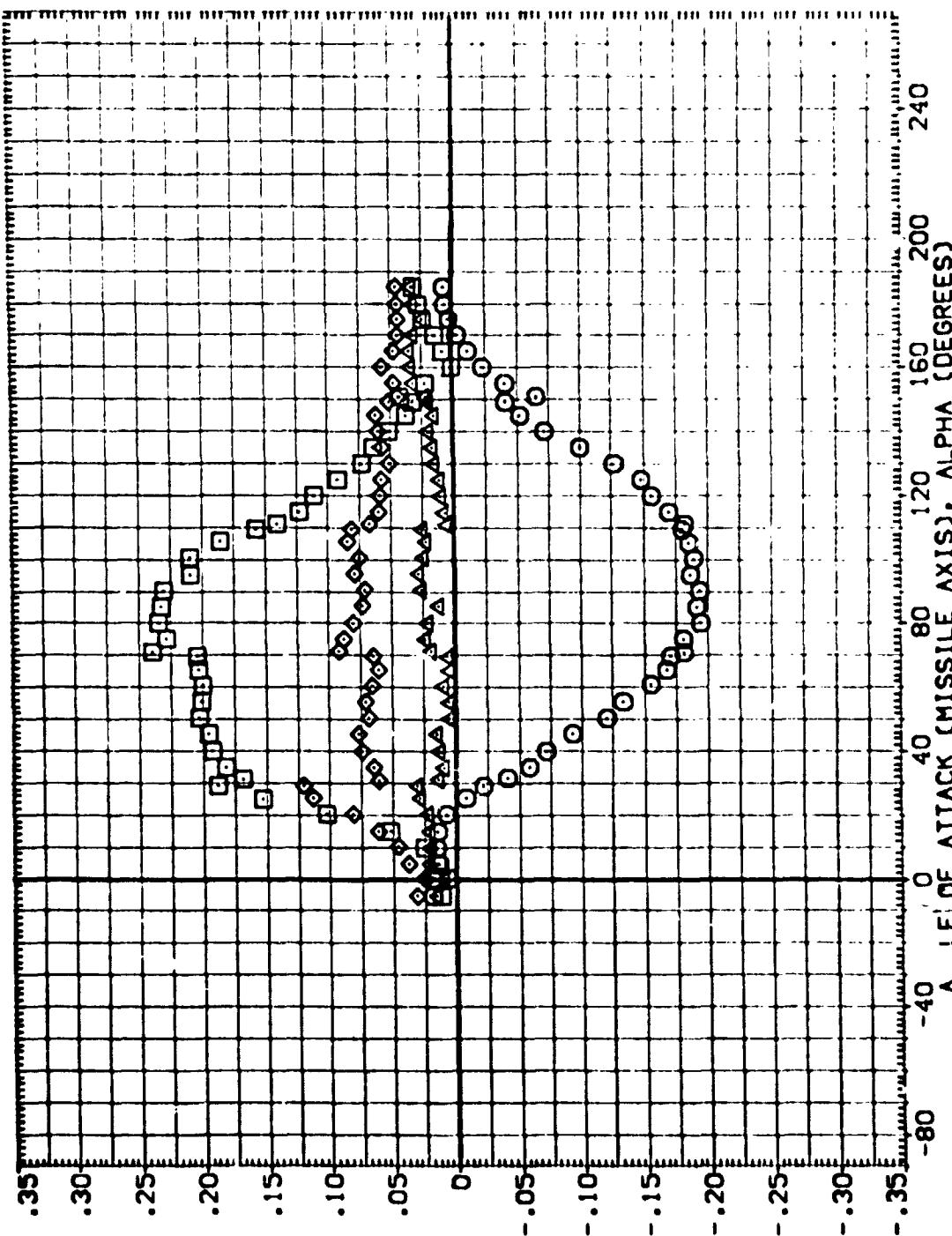
SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMOI)

PHI. 180. HUCA 10. TRIC V 1.160

YION 50.FT.
IN.
IN.
IN.XT
IN.YT
IN.ZT
REF 330.
REF 140S.
XMAP
SCALE



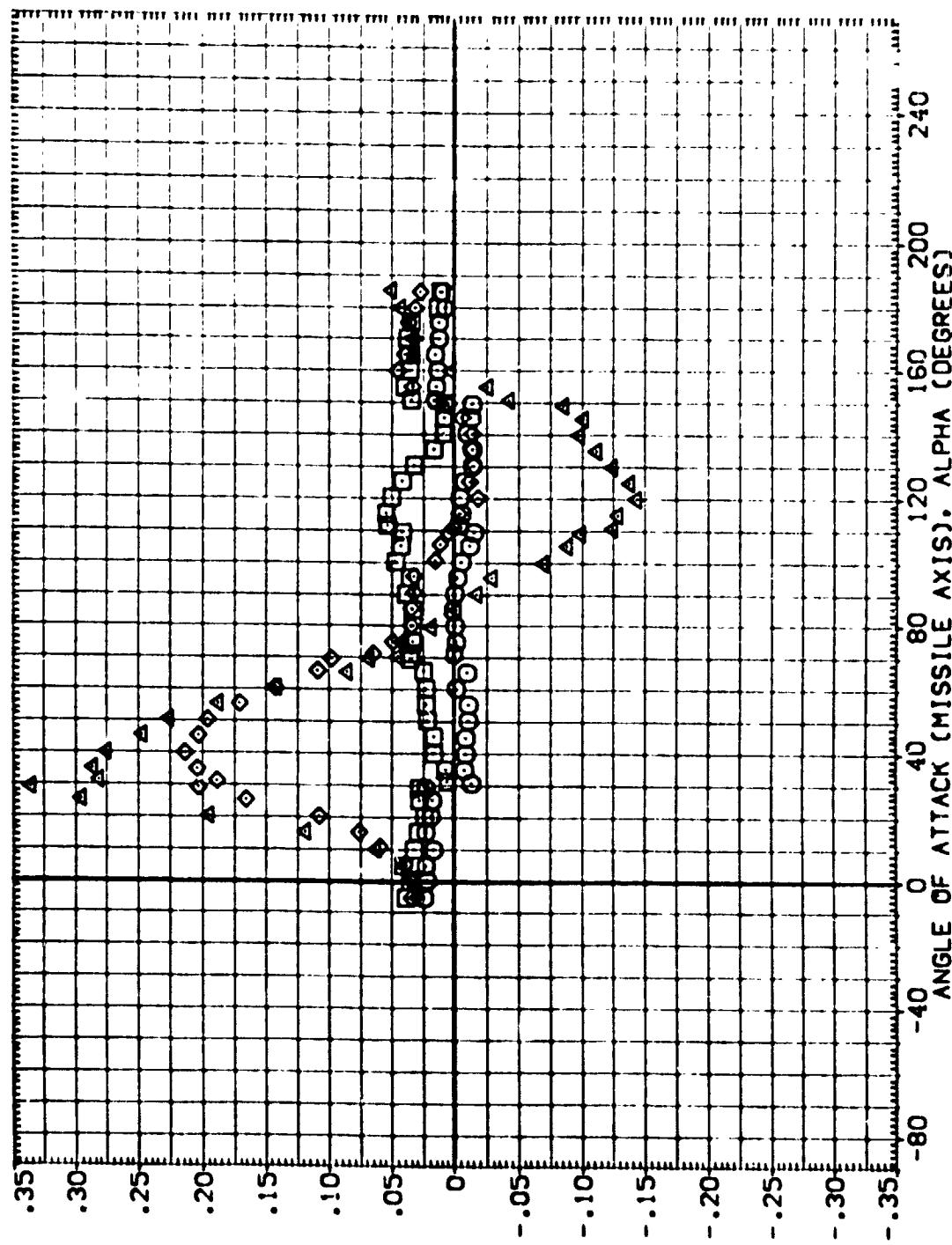
SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

FIG. 4 COEFFICIENTS VS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMOI)

PHI₁
45.
90.
135.
 P₁ TRIC V
10.400 S₁
1.100

RECEIVE INF.
594.1
SQ.FT.
LREF 330.
RREF 330.
XREF 146.
YREF 2740.
ZREF
SCALE



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

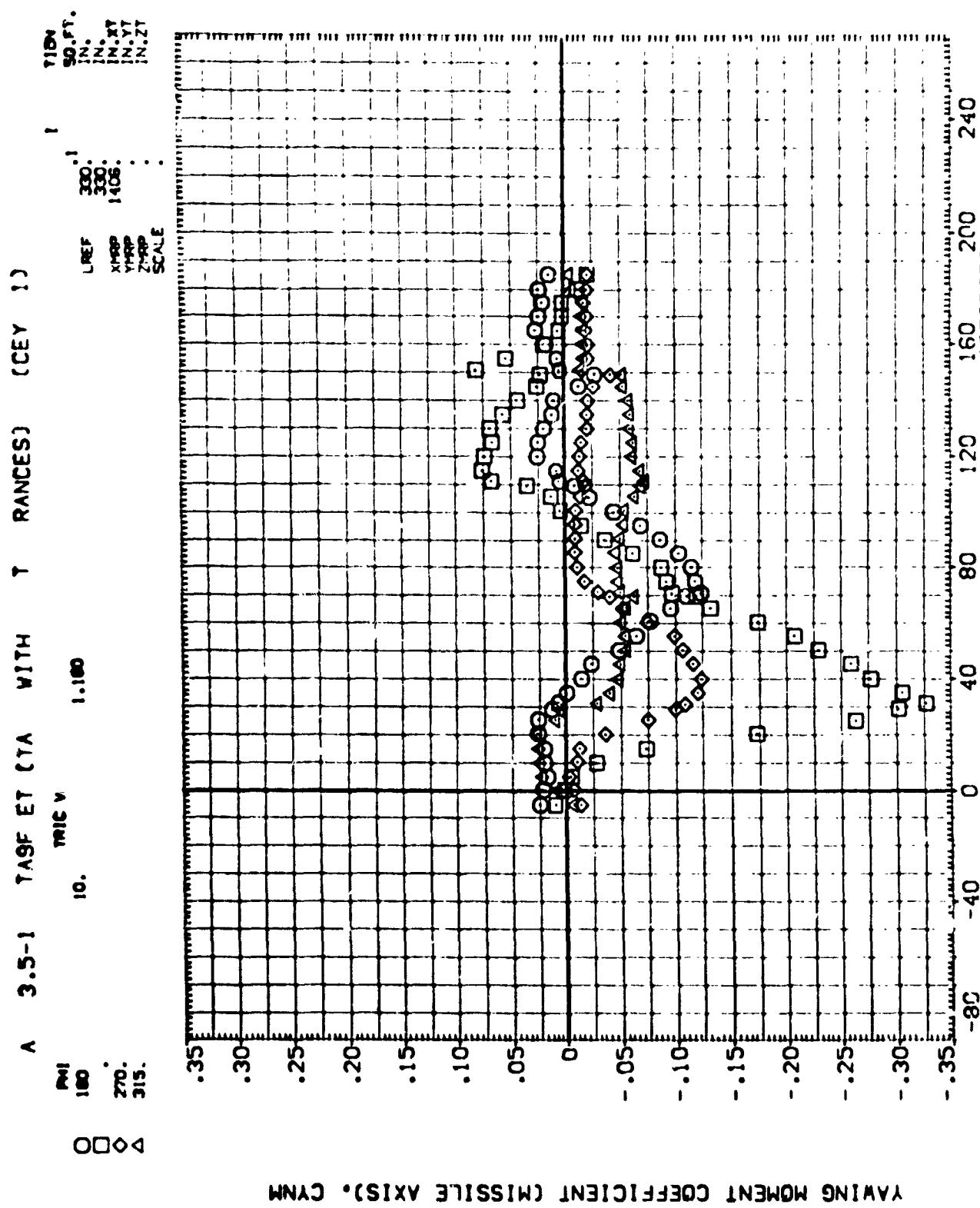


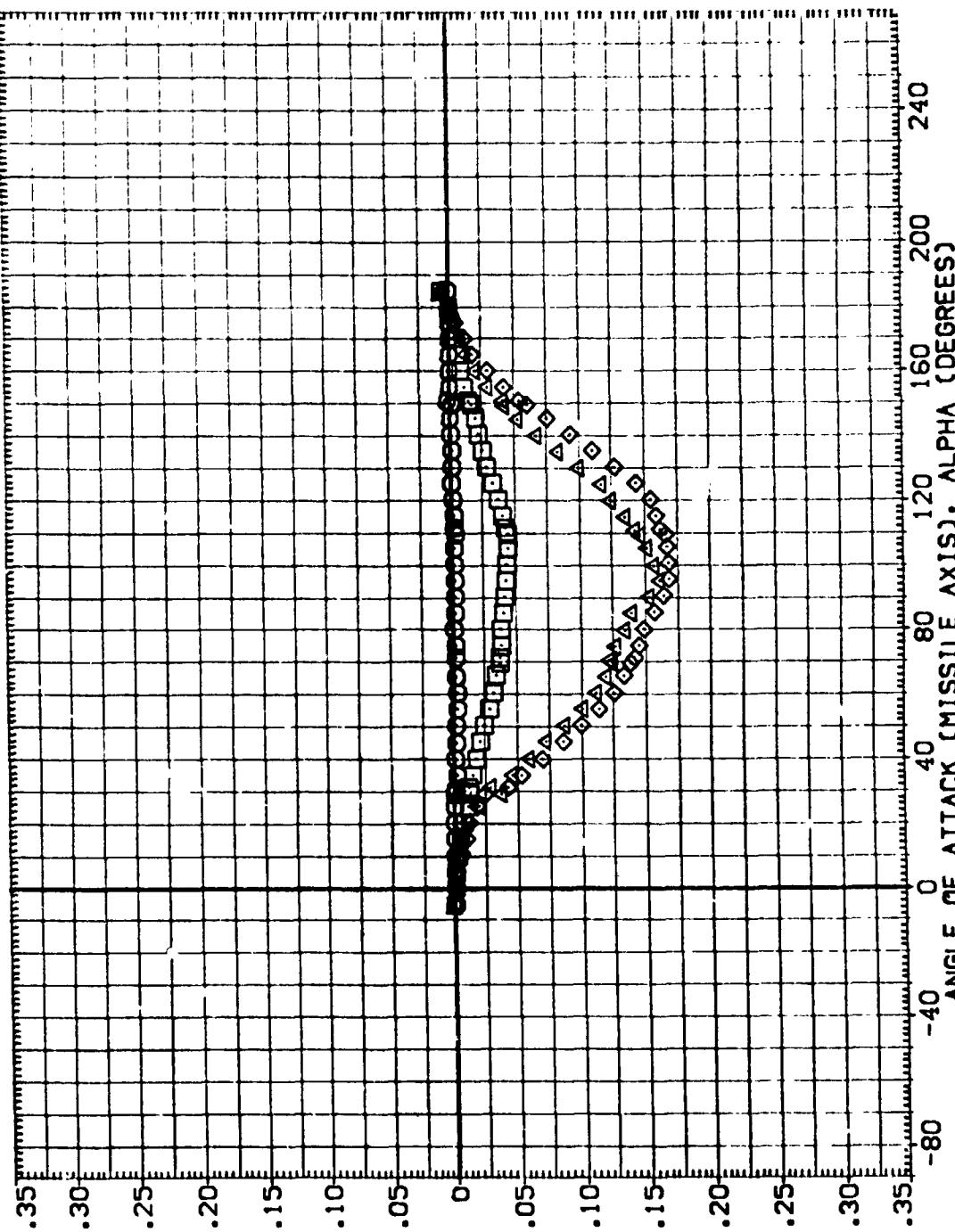
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

PAGE 1C

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CCFYMO1)

PARAMETRIC VALUES
 PHI : 45.
 R/L : 10.400
 1.160
 90.000
 135.000

REFERENCE INFORMATION
 SREF : 594.370 SO.FT.
 LREF : 330. IN.
 BREF : 350. IN.XT
 XMRP : 1406. IN.YT
 YMRP : ZMRP : IN.ZT
 SCALE :



ROLLING MOMENT COEFFICIENT (MISSILE AXIS). CBL

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

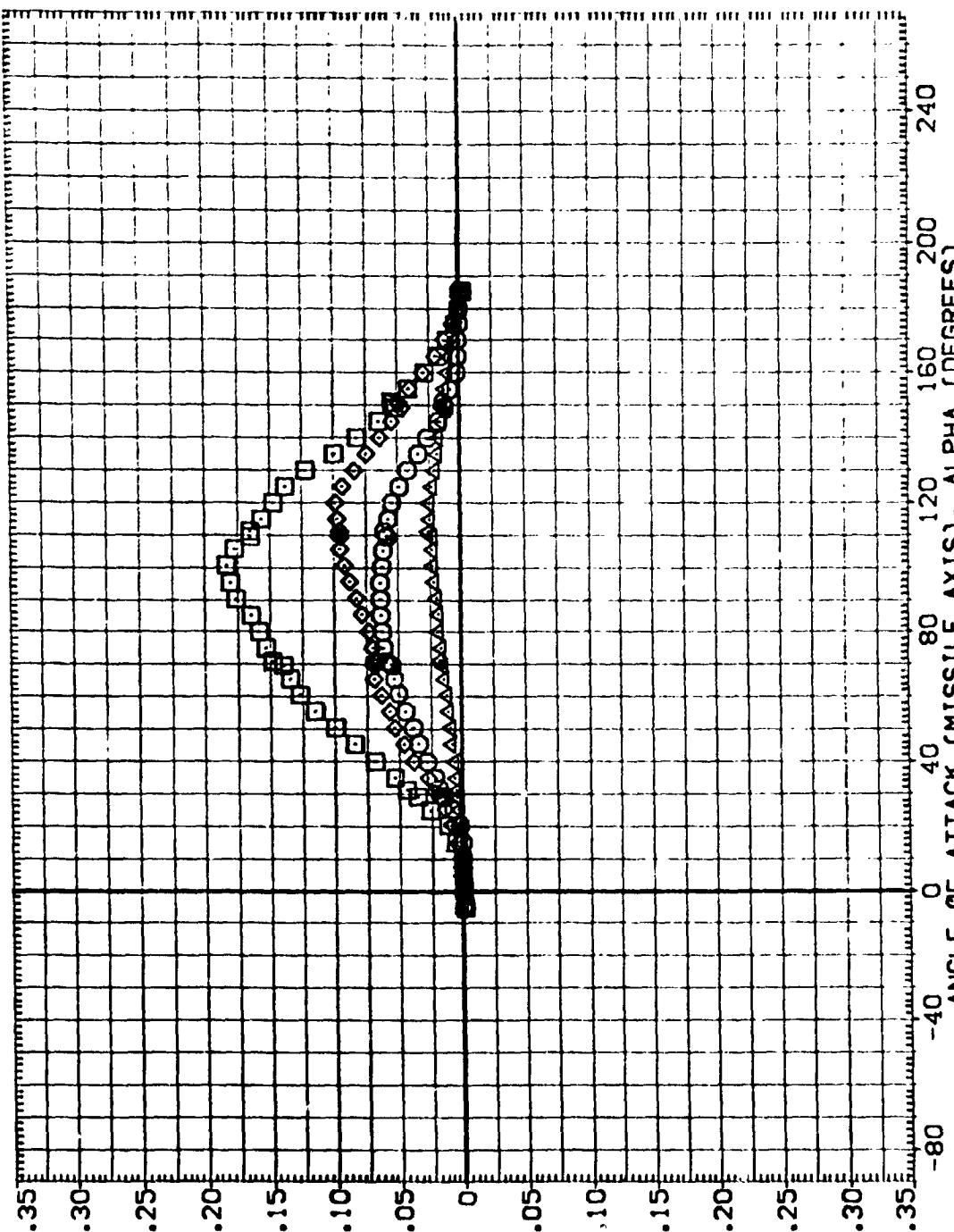
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

PHI	P	TRIC VALUES	REFL
180.		10,400	1,160
225.			
270,000			
315.			

□ ◻ ◇ ◄

SREF
LREF
BREF
XMRP
YMRP
ZMRP
SCALE

REFERENCE INF
SFA, 1350
60.FT.
N.
N.XT
N.YT
N.ZT



ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO1)

PARAMETRIC VALUES
10.400
1.160

PHI : 45.
80.
135.
REF : 10.400
LEF : 1.160
XREF : 1406.
YREF : .2000
SCALE : .1

○□◇△

CENTER OF PRESSURE LOCATION, XCP/L

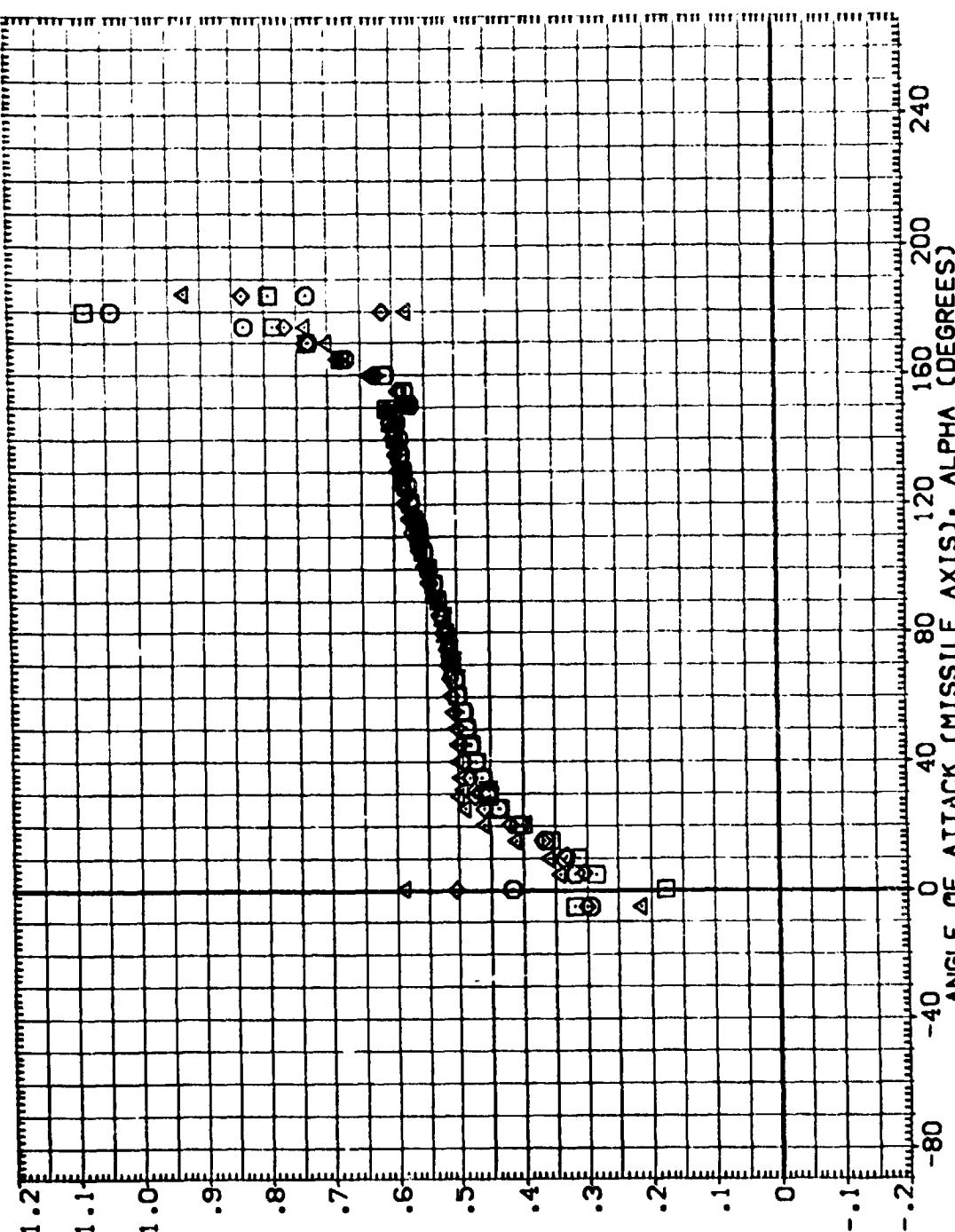


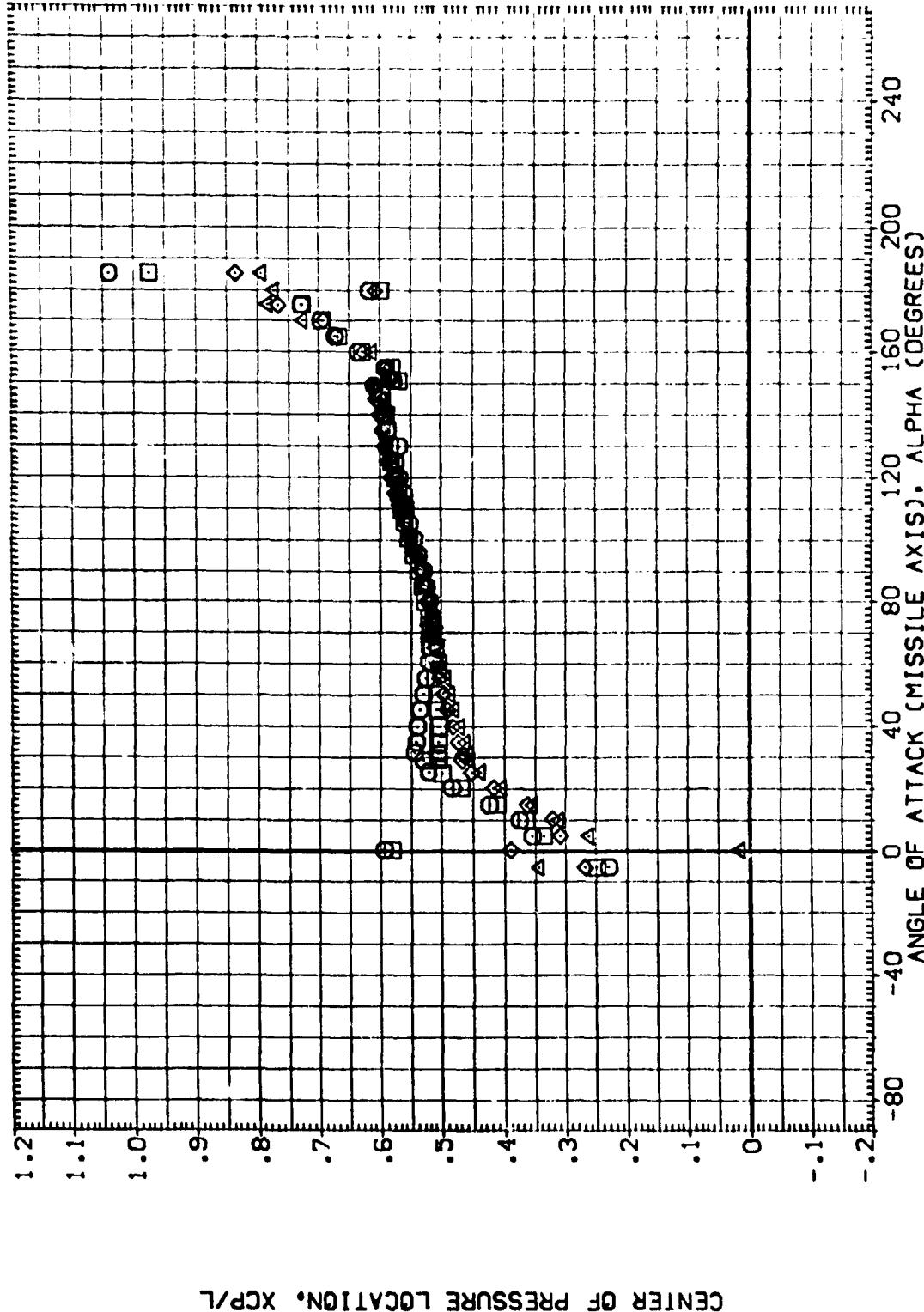
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES)

(CEYMO1)

PARAMETRIC VALUES
 Φ_1
 180.
 225.
 270.000
 315.000

REFERENCE INFORMATION
 SREF 594.1360 SD.FT.
 LREF 330. IN.
 BREF 330. IN.
 XMRP 1406. IN.XT
 YMRP 240. IN.YT
 ZMRP 240. IN.ZT
 SCALE . .



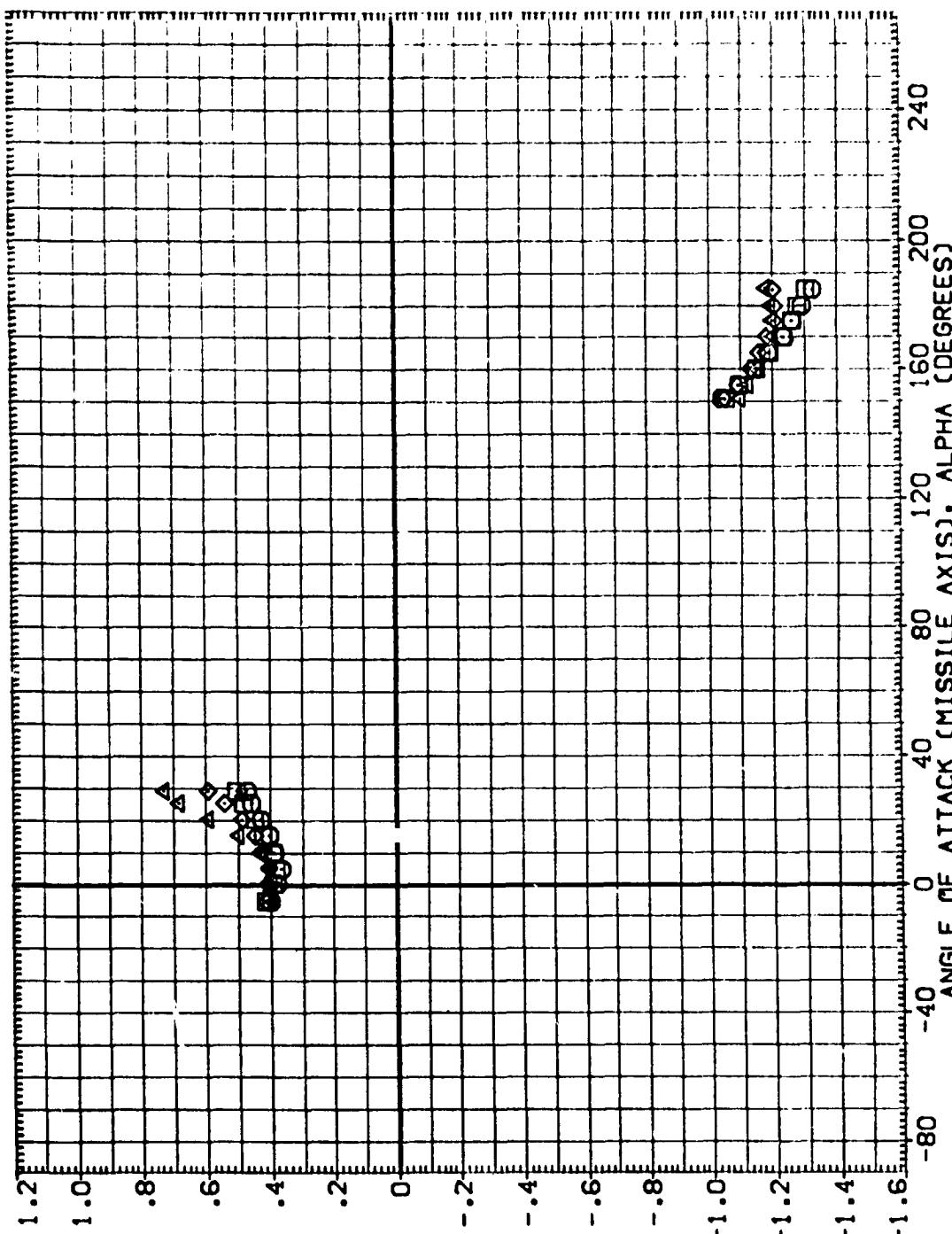
CENTER OF PRESSURE LOCATION, XCP/L

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (DEYMO1)

PARAMETRIC VALUES
 PHI : 45.
 10.400 RNL 1.160
 90. 135.000
 O □ ◇ △

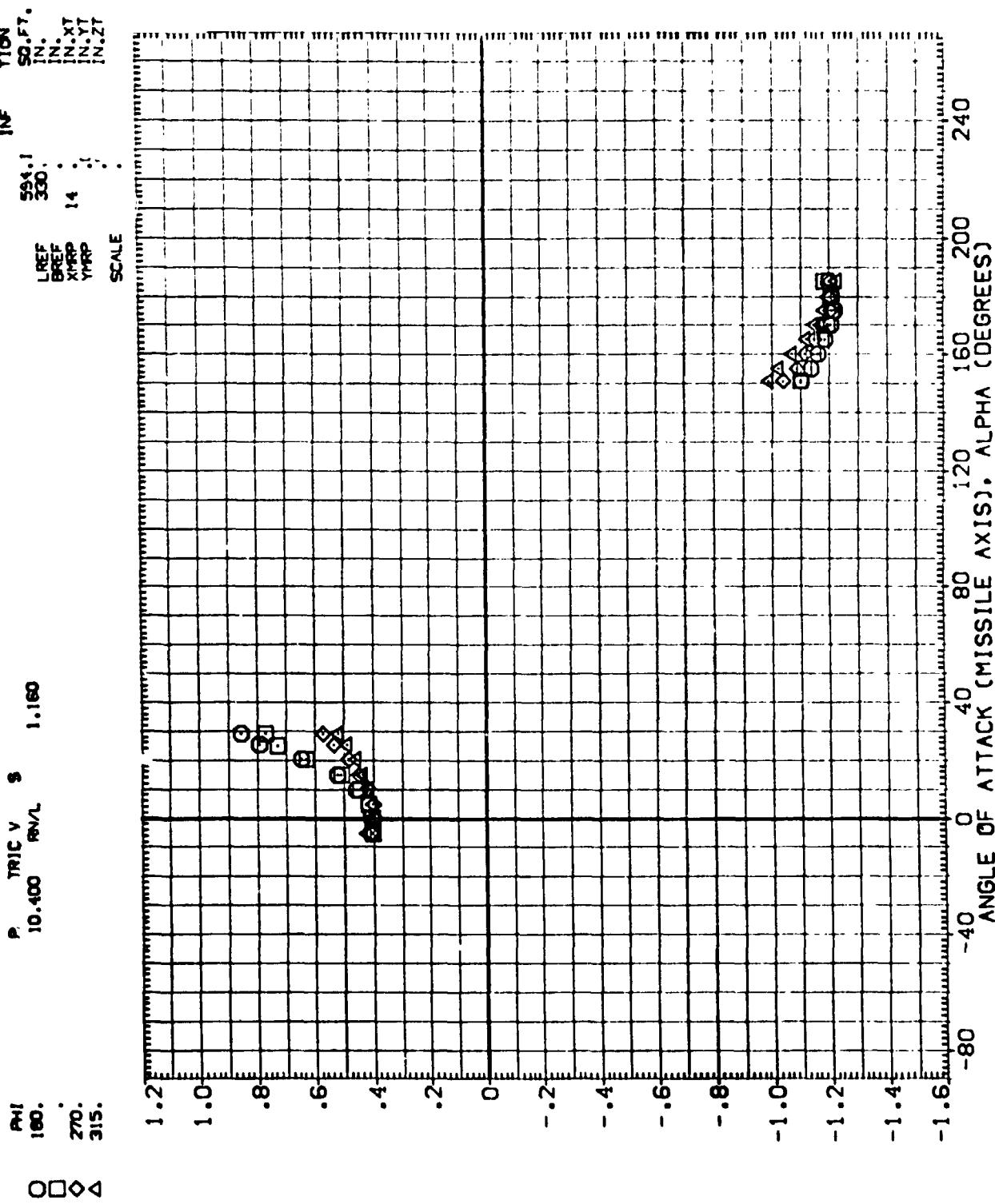
REFERENCE INFORMATION
 SREF 594.1360 IN. FT.
 LREF 230. IN.
 BREF 330. IN.
 XMRP 1405. IN.XT
 YMRP : IN.YT
 ZMRP : IN.ZT
 SCALE :



FOREBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAF

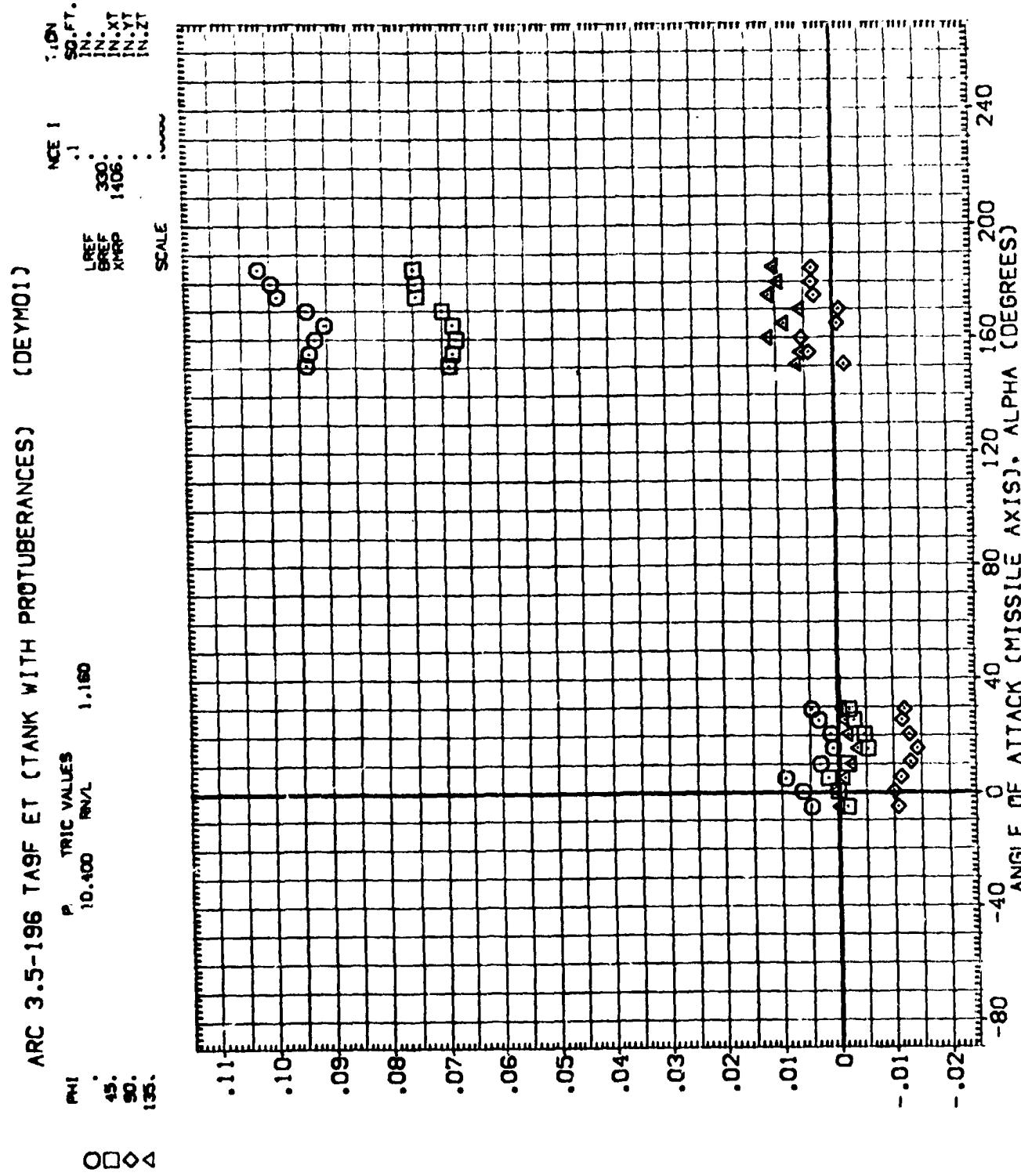
FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (DEYMO1)



FOREBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS), CAF

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK



BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAB

FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

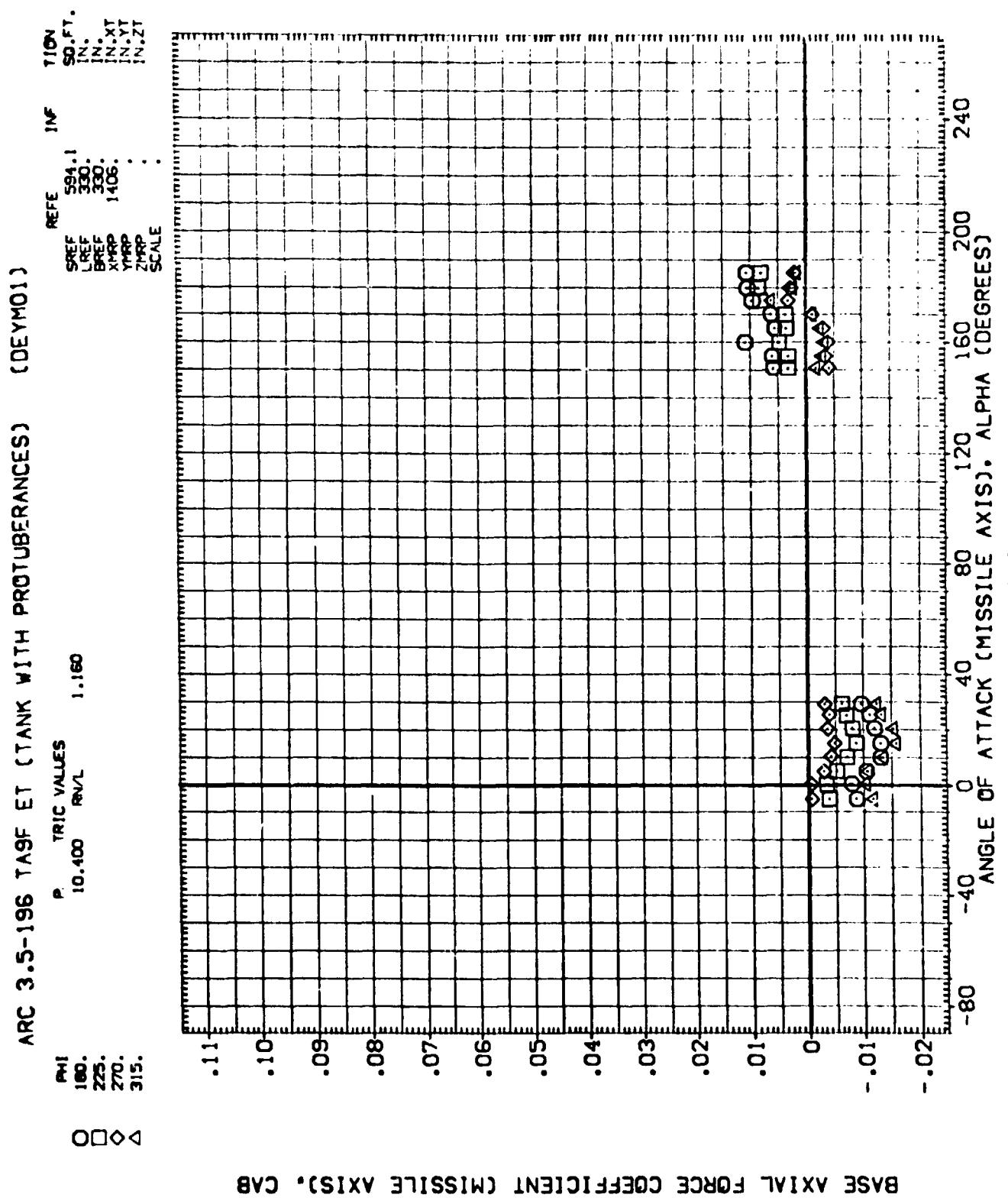


FIG. 4 COEFFICIENTS VERSUS ANGLE OF ATTACK

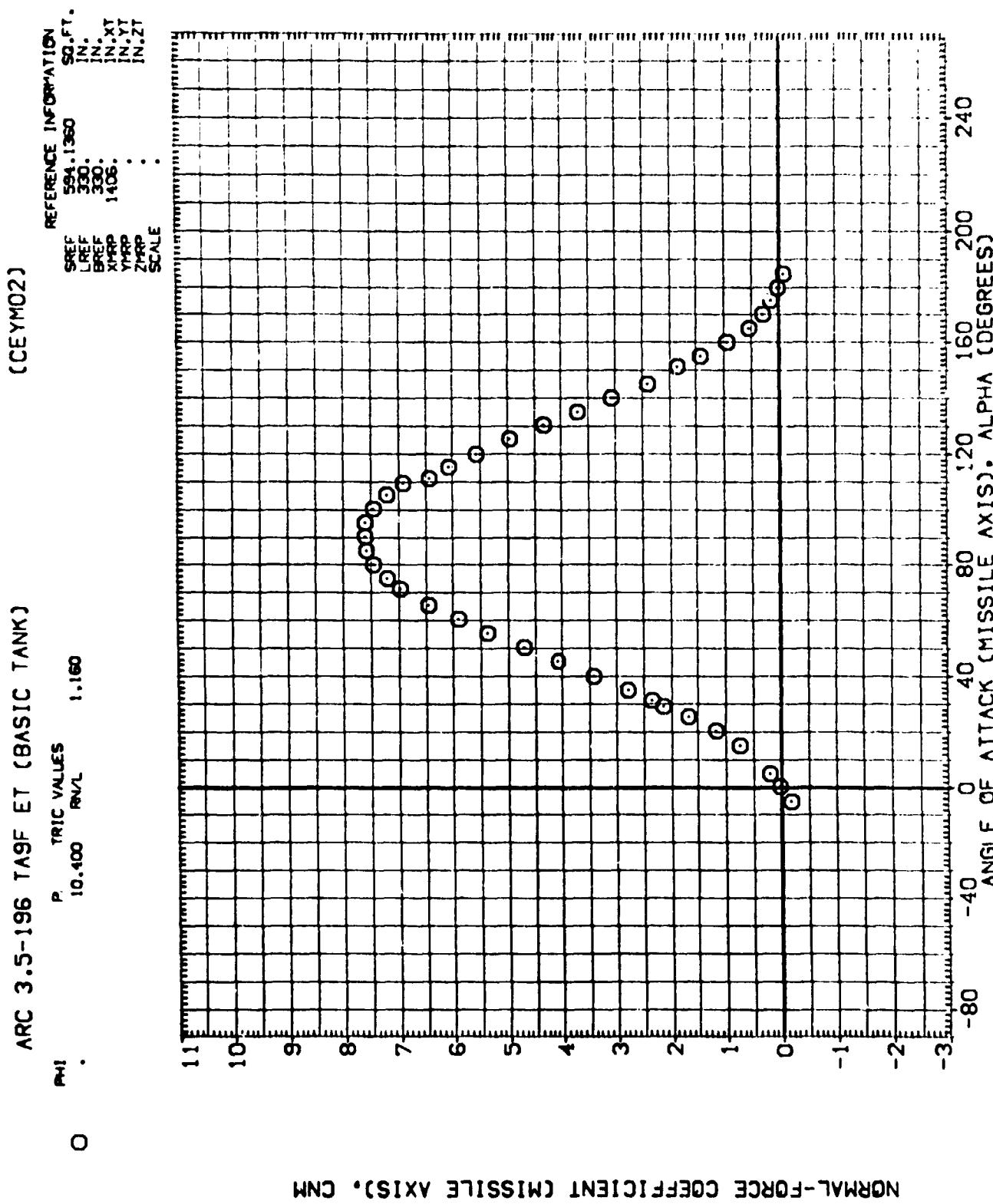
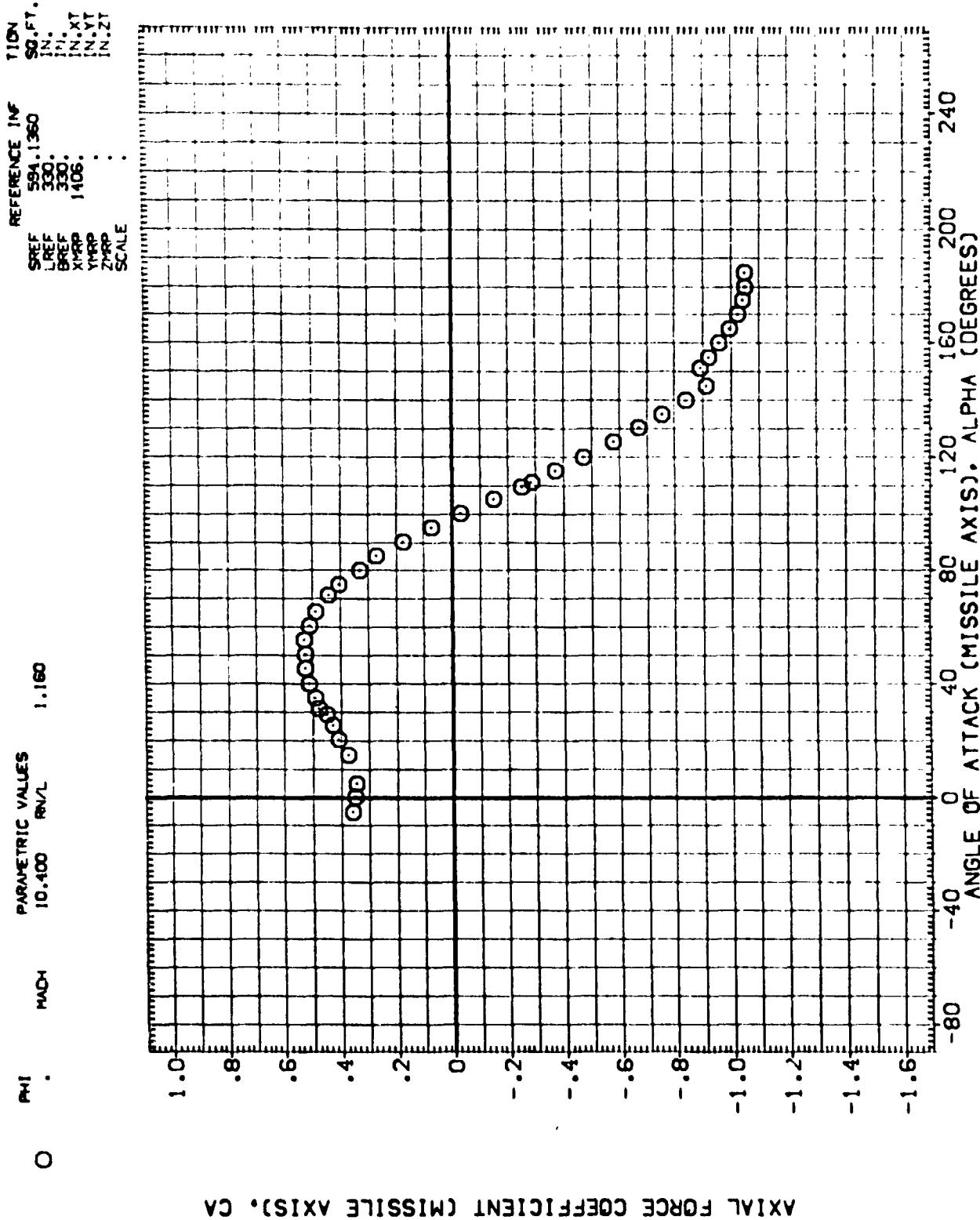


FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (BASIC TANK)
 PARAMETRIC VALUES
 MACH 10.400 ROLL 1.160

(CE YM02)



AXIAL FORCE COEFFICIENT (MISSILE AXIS). CA

FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

TION
 REF. SC.FT.
 SREF 594.1350
 LREF 330.
 BREF 330.
 XMPP 1406.
 YMPP .
 ZMPP .
 SCALE .

PARAMETRIC VALUES
 MACH 10.400 ROLL 1.160

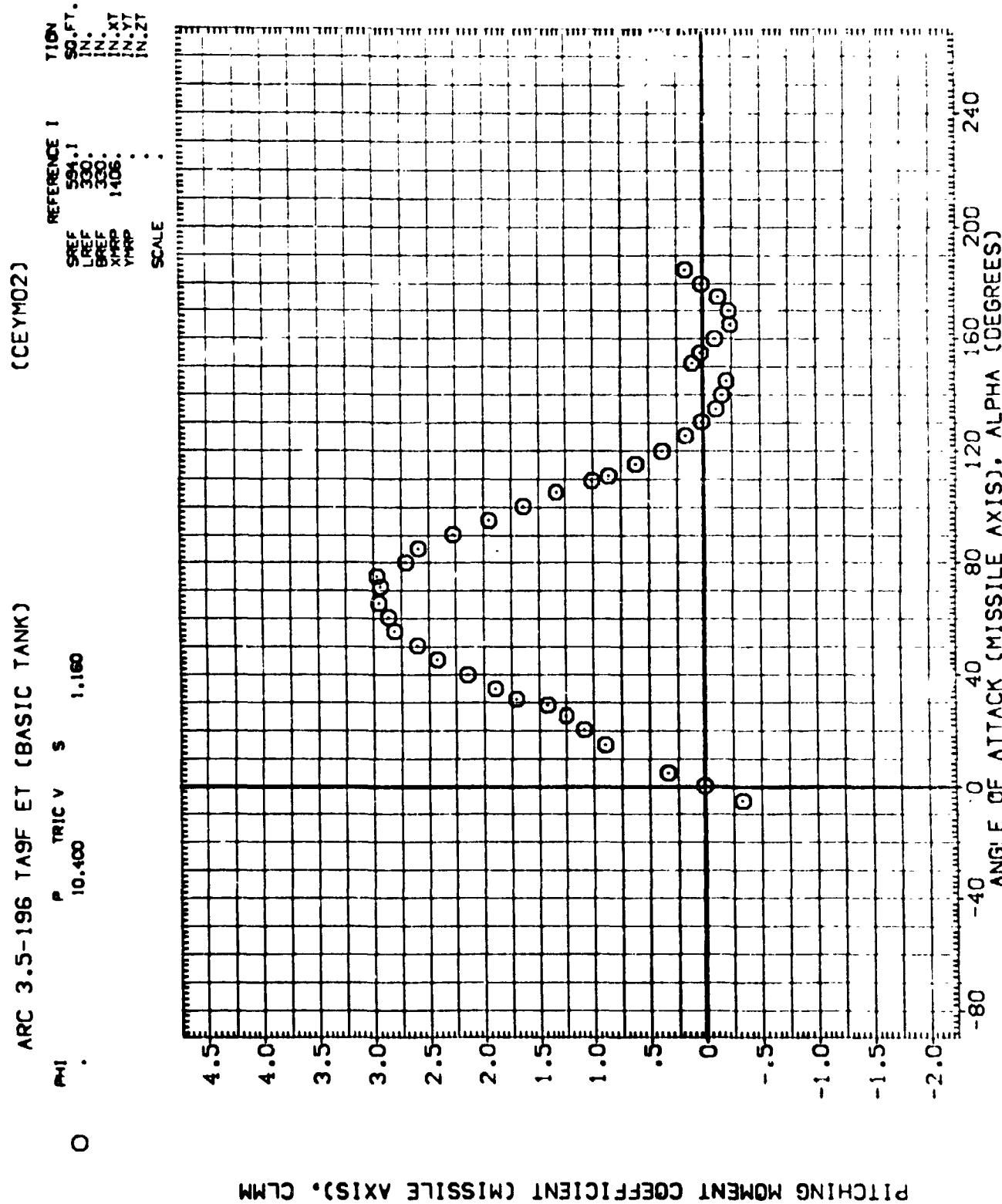


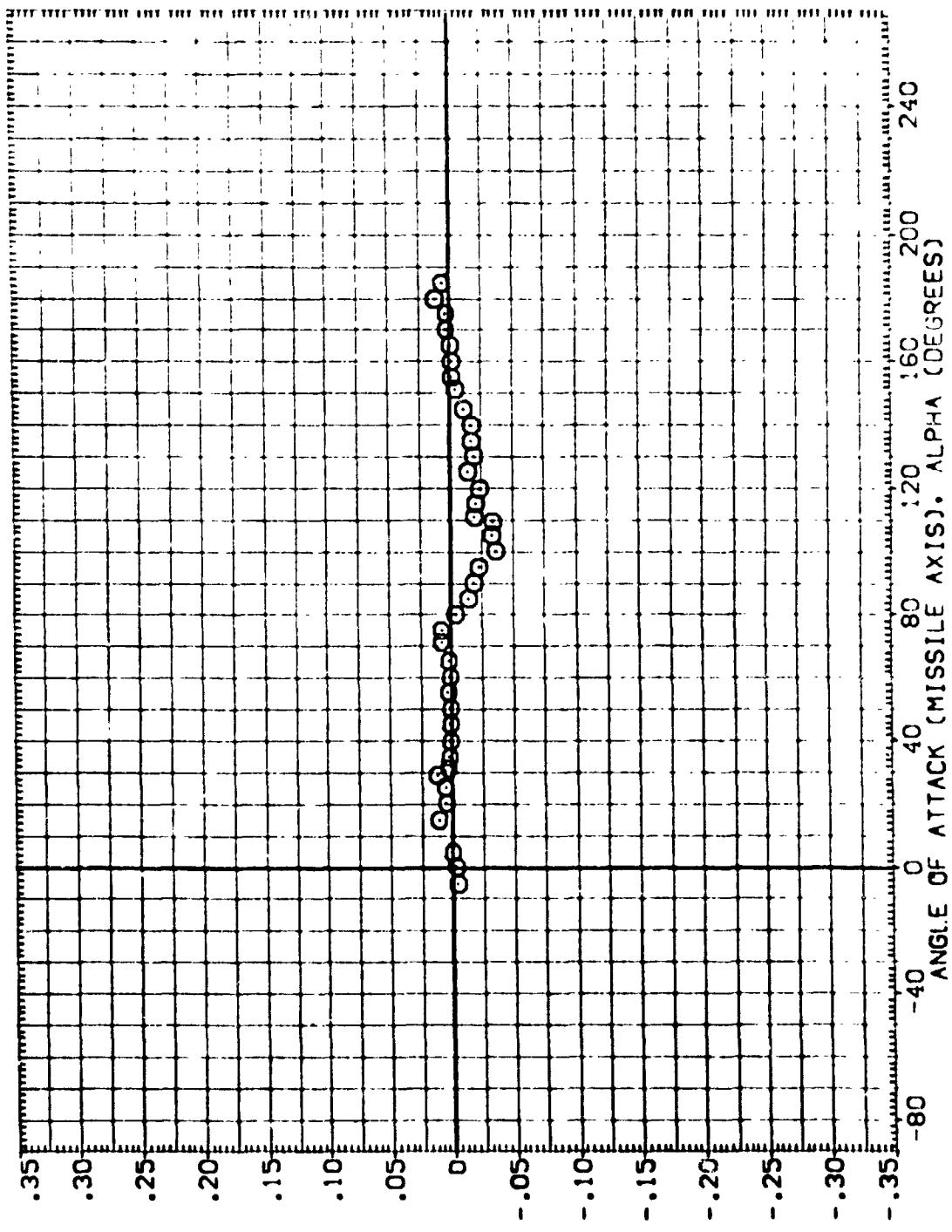
FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-196 TAGF ET (BASIC TANK)

(CE YMO2)

P_{TRIC} VALUES
10,400 RNL 1,160

REFERENCE INFORMATION
LREF 594,1350 IN.
BREF 330. IN.
YRPP 1406. IN.
ZRPP N.YT
SCALE N.ZT



SIDE-FORCE COEFFICIENT (MISSILE AXIS). CM

FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-196 TAGF ET (BASIC TANK)

(CEYMM02)

WIND TRIM VAL 1.100

REFERENCE SURFACE
SREF 594.1
LREF 330.
BREF 320.
XHPP 1406.
YHPP .
ZHPP .
SCALE .

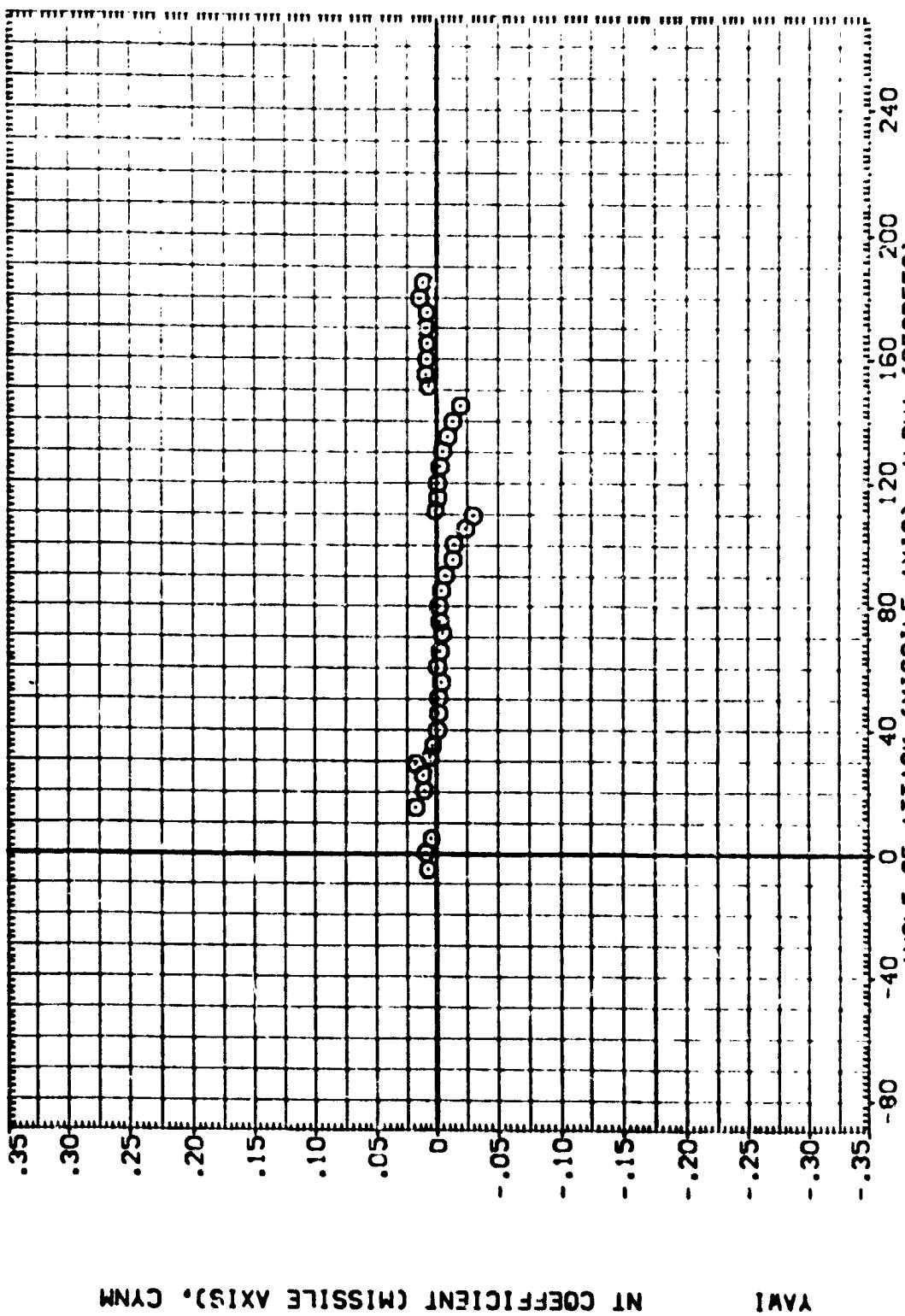
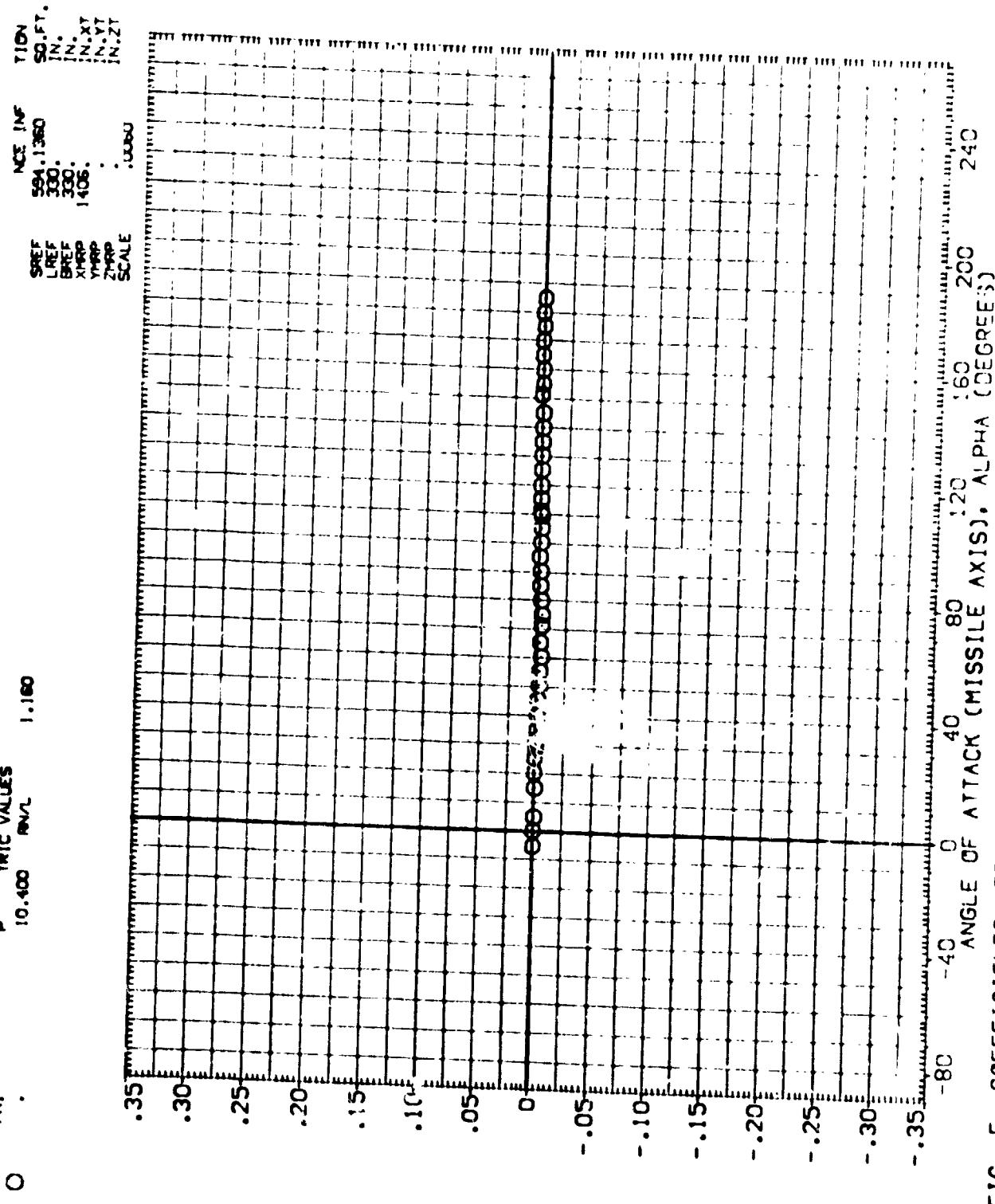


FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (BASIC TANK)

O MI. P TRIC VALUES
10.400 10.160

(CCEYMO2)



ROLLING MOMENT COEFFICIENT (MISSILE AXIS). C

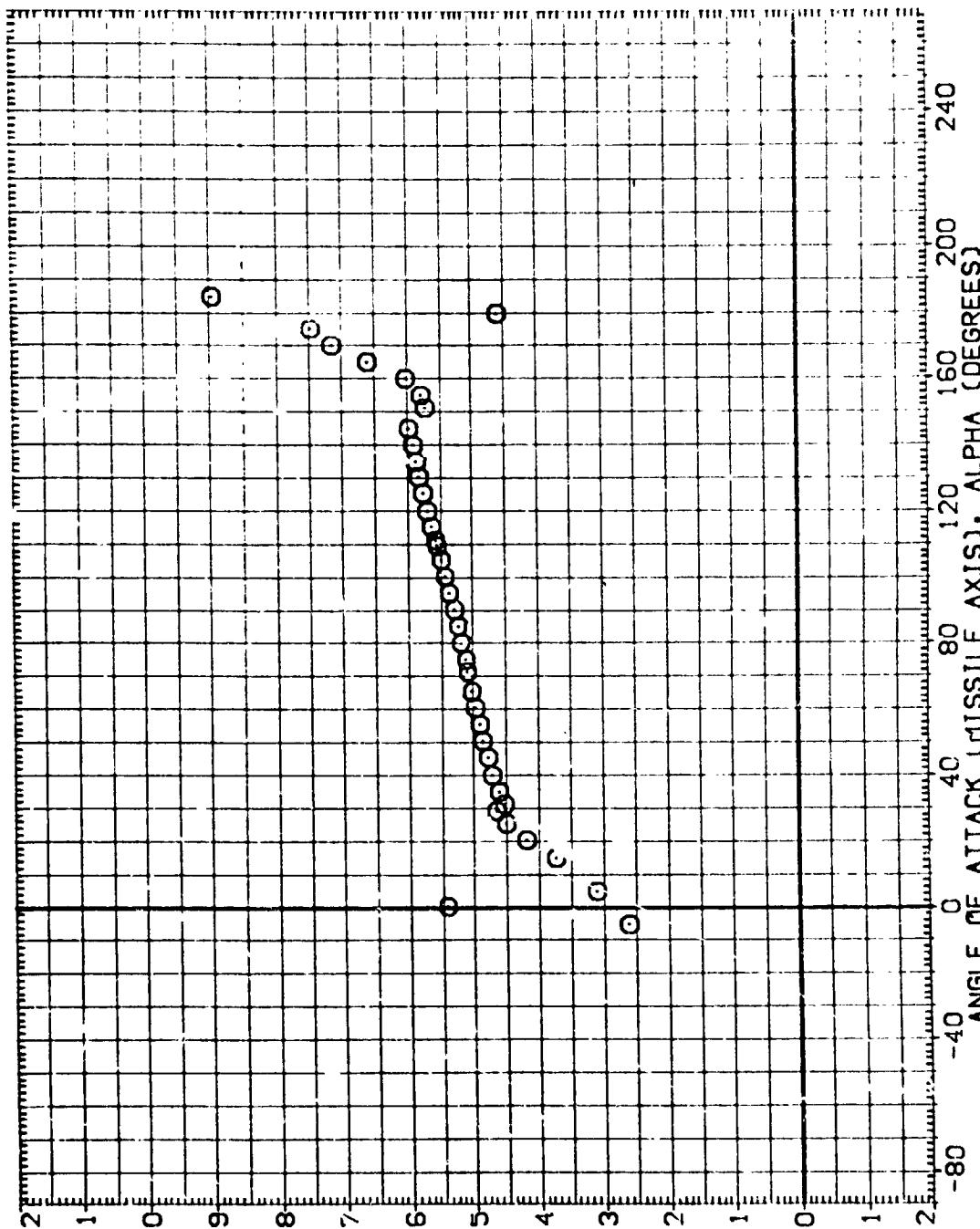
FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (BASIC TANK)

ρ_{HI} .000 MACH 10.400 RNU 1.160

(CEYMOZ)

REFERENCE SURFACE
SREF 594.1
LREF 330.
BREF 330.
XMRP 1466.
YMRP 700.
ZMRP 1.
SCALE 1.



CENTER OF PRESSURE LOCATION, CPL

FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5--196 TAGF ET (BASIC TANK)

(DEYMO2)

PARAMETRIC VALUES

MACH	10.400	RNL	1.160
------	--------	-----	-------

REFERENCE INFORMATION

SREF	594.1360	SO.FT.
LREF	350.2000	IN.
BREF	350.2000	IN.
XREF	1406.0000	IN.XT
YREF	.0000	IN.YT
ZREF	.0060	IN.ZT
SCALE		

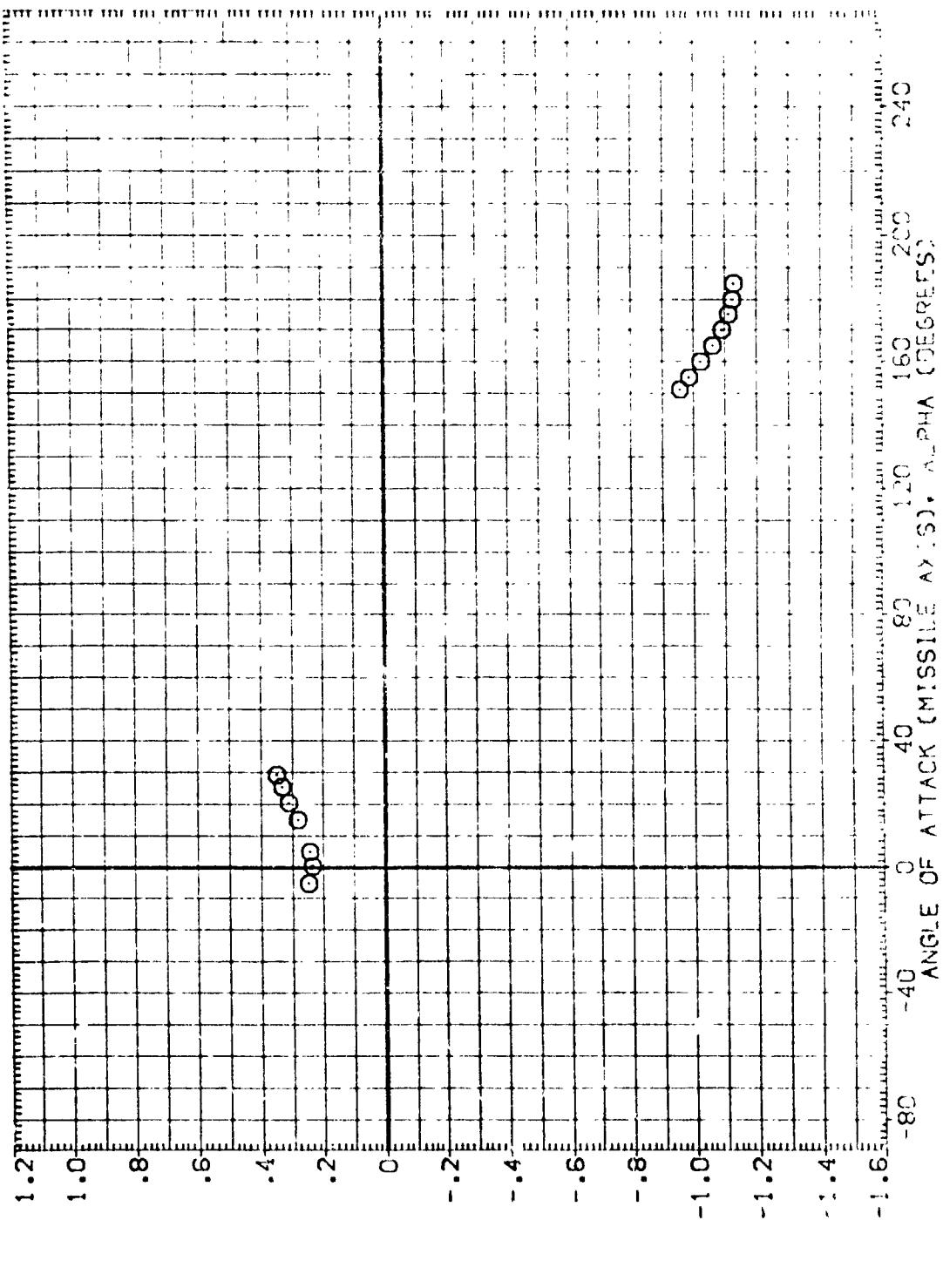


FIG. 3 COEFFICIENTS VERSUS ANGLE OF ATTACK

FIG. 3 COEFFICIENTS VERSUS ANGLE OF ATTACK

MAG

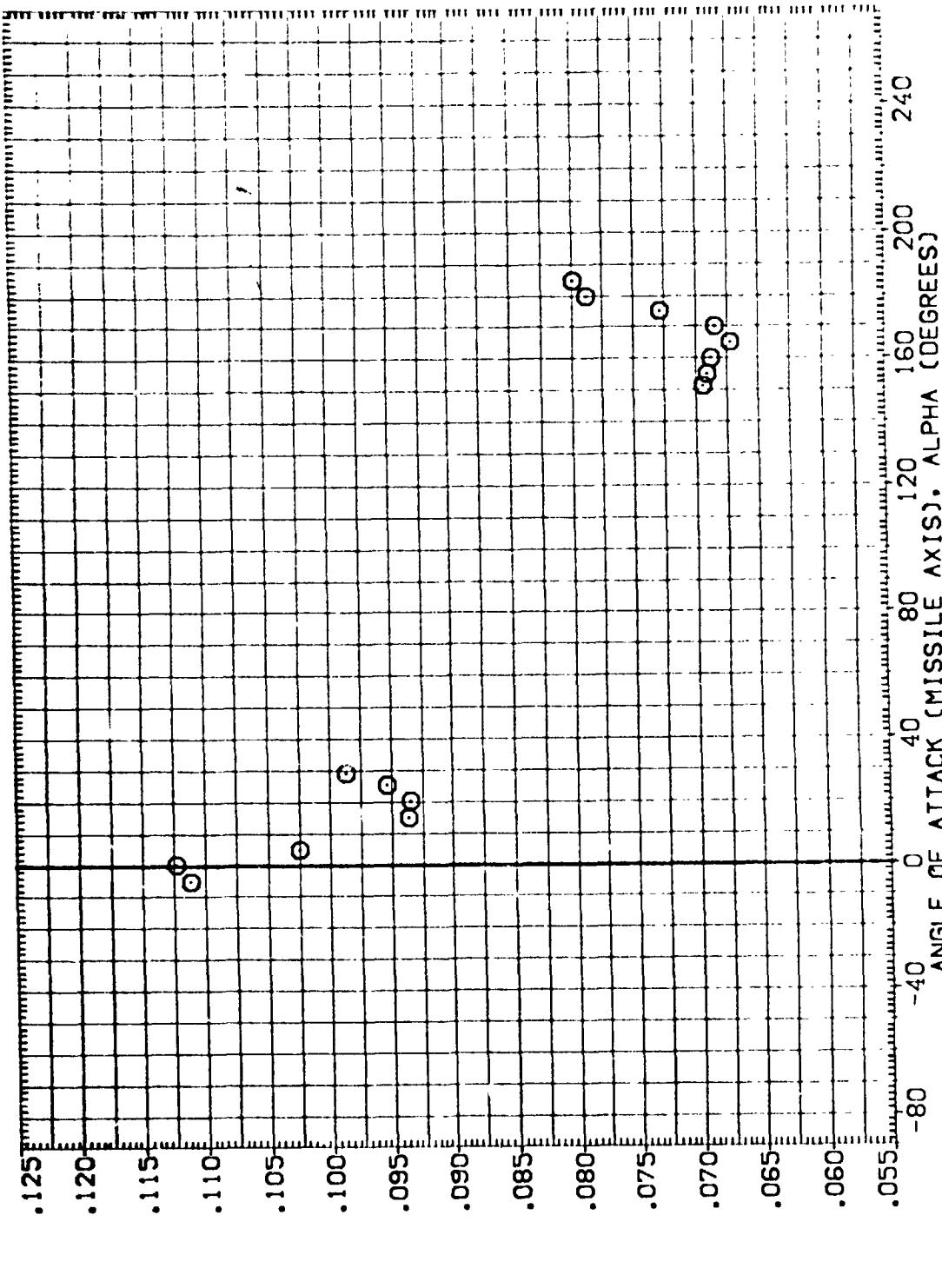
26

ARC 3.5-196 TAGF ET (BASIC TANK)

(DEYMM02)

PHI . MACH 10.400 RNL 1.160

PARAMETRIC VALUES
REFERENCE INF.
SREF 594.1360
LREF 330.
BREF 330.
XHPP 1405.
YHPP
ZHPP
SCALE



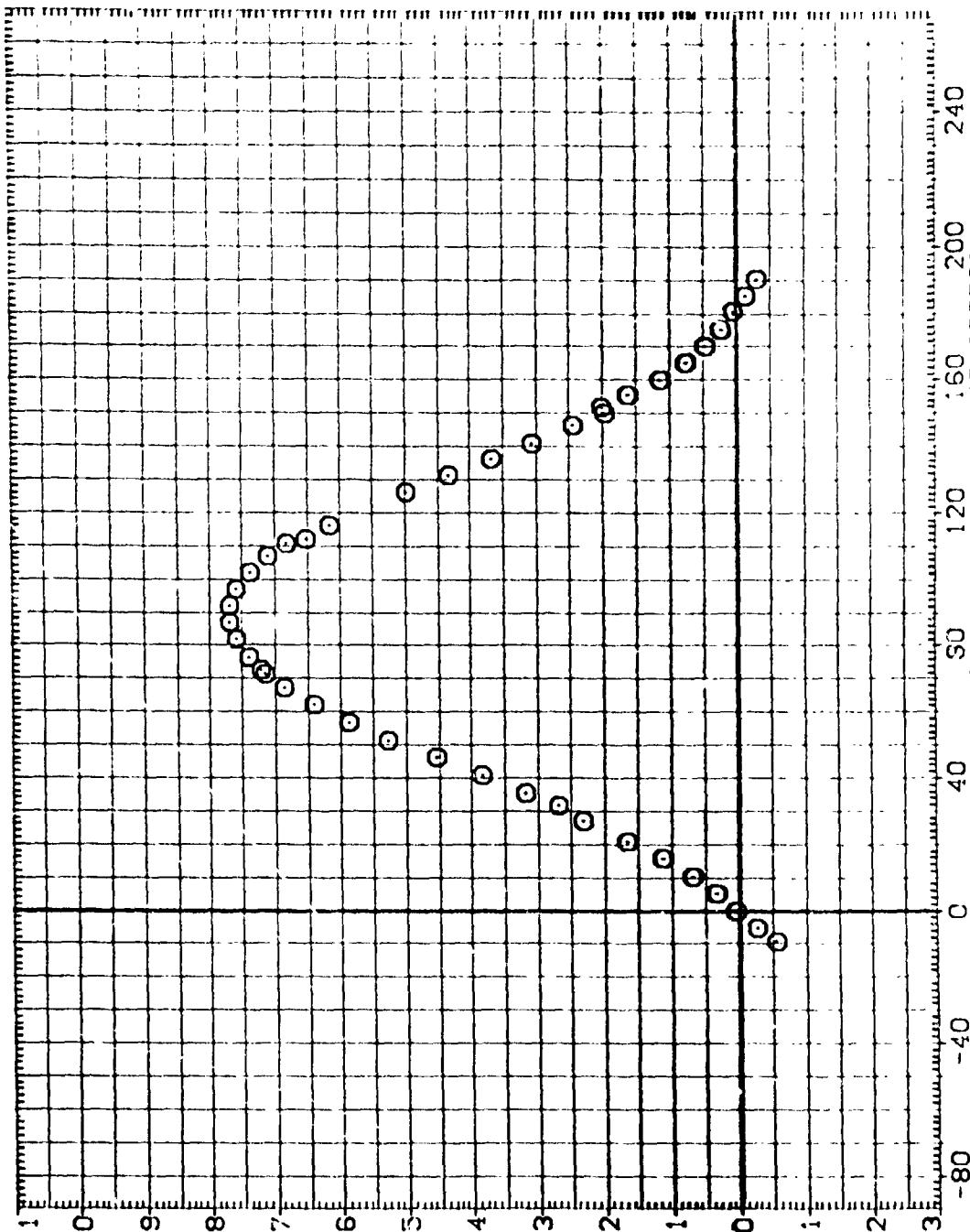
BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS), CAB

FIG. 5 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO3)

PHI
180.000 MACH 5.300 RVAL 3.810

REFERENCE INFORMATION
SQ.FT.
REF 594.1360
LREF 330.
BREF 330.
IN.XT 146.
IN.YT
IN.ZT
SCALE



NORMAL-F0 E COEFFICIENT (MISSILE AXIS), CNM

FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

PAGE 28

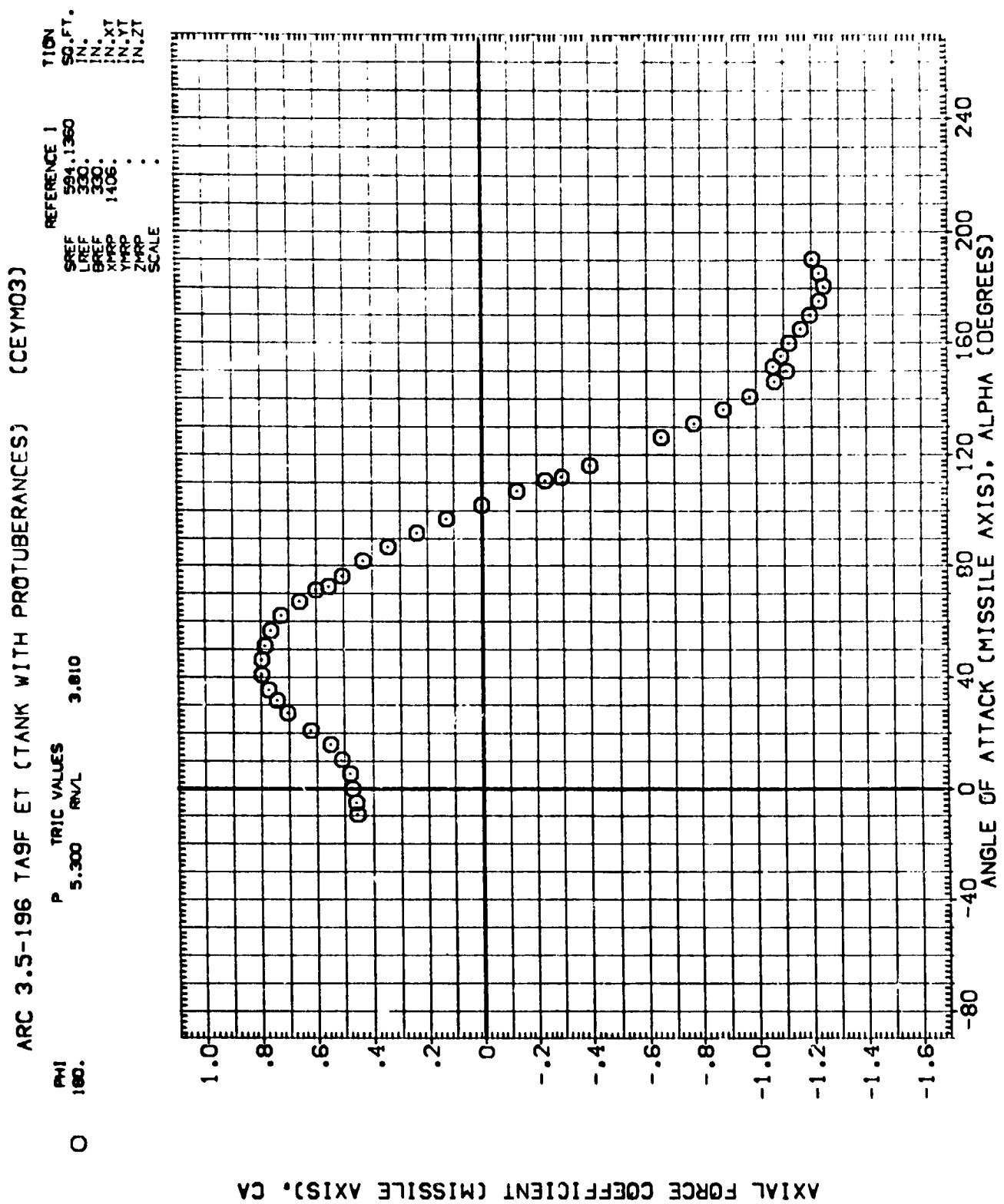
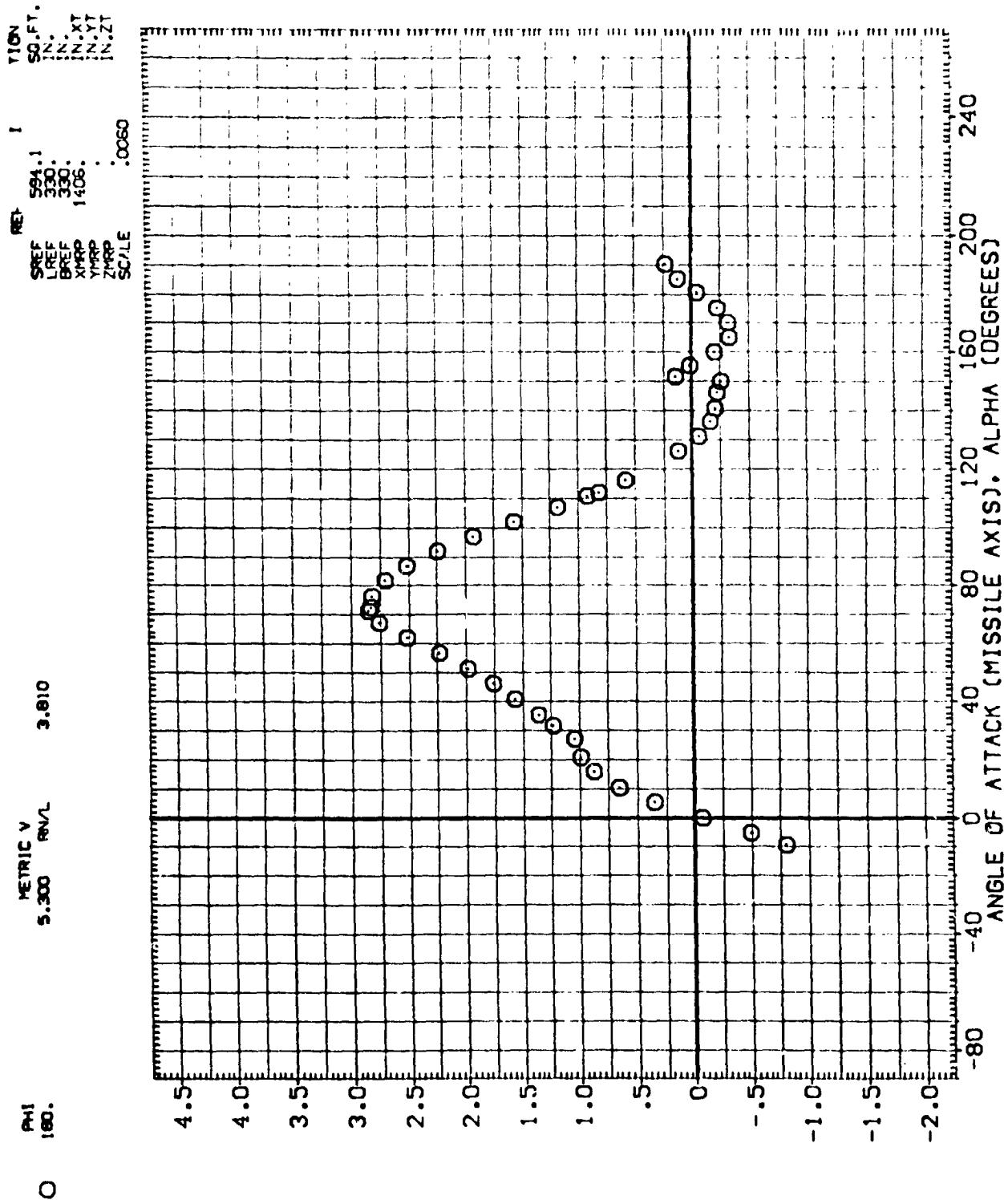


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO3)



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLMM

FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMM03)

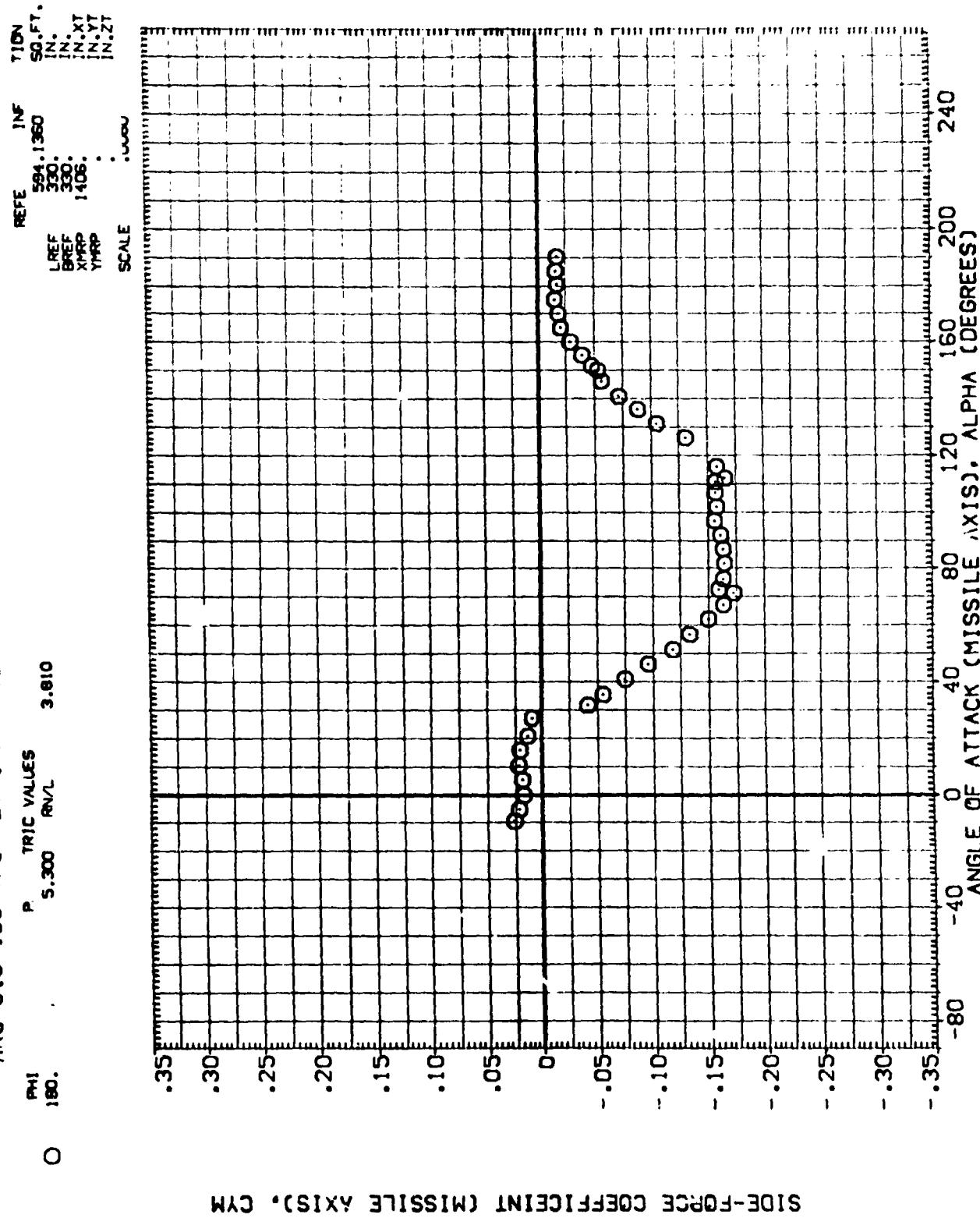


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO3)

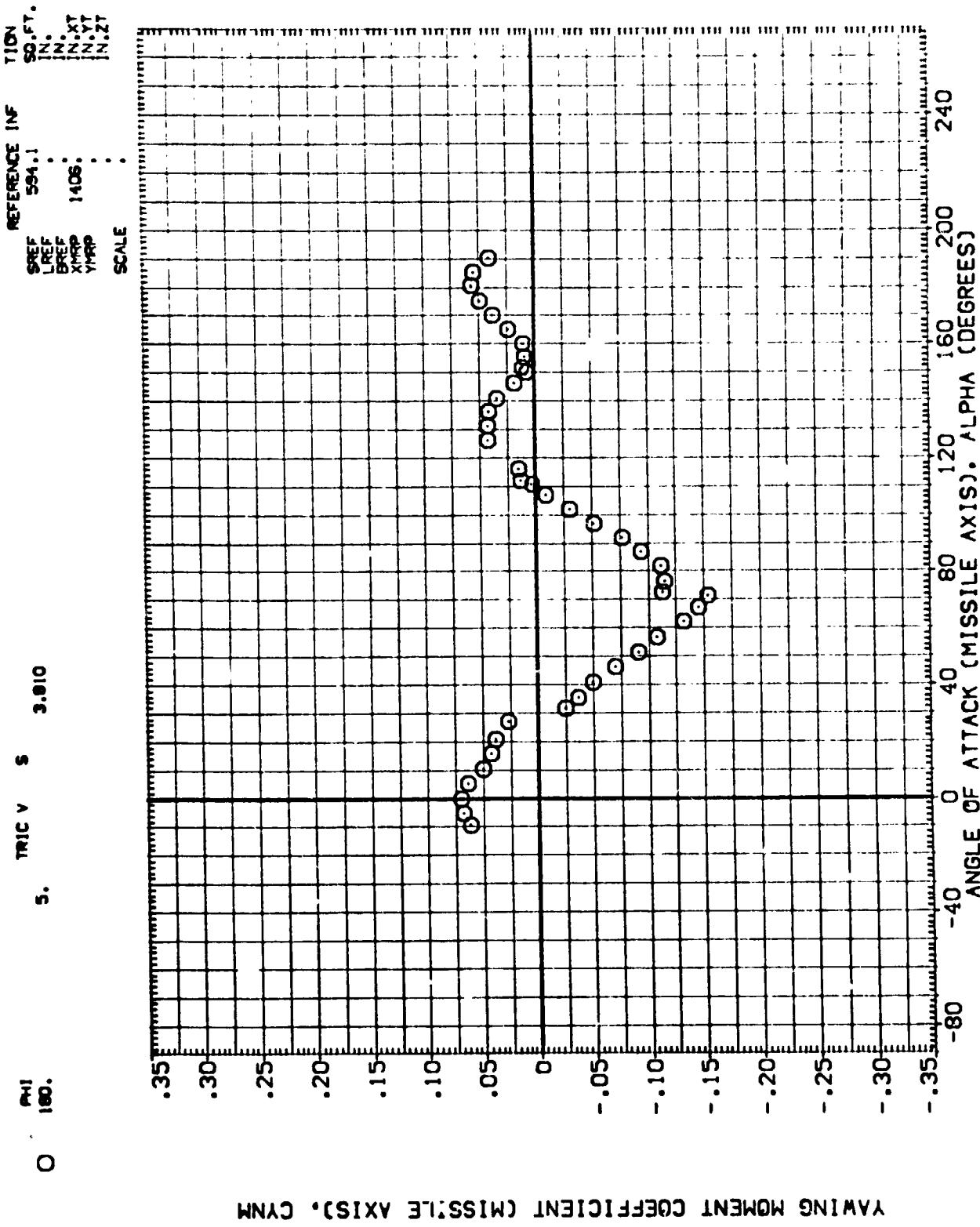


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO3)

PHI
180.
PARAMETRIC VALUES
5.
RNL
3.810

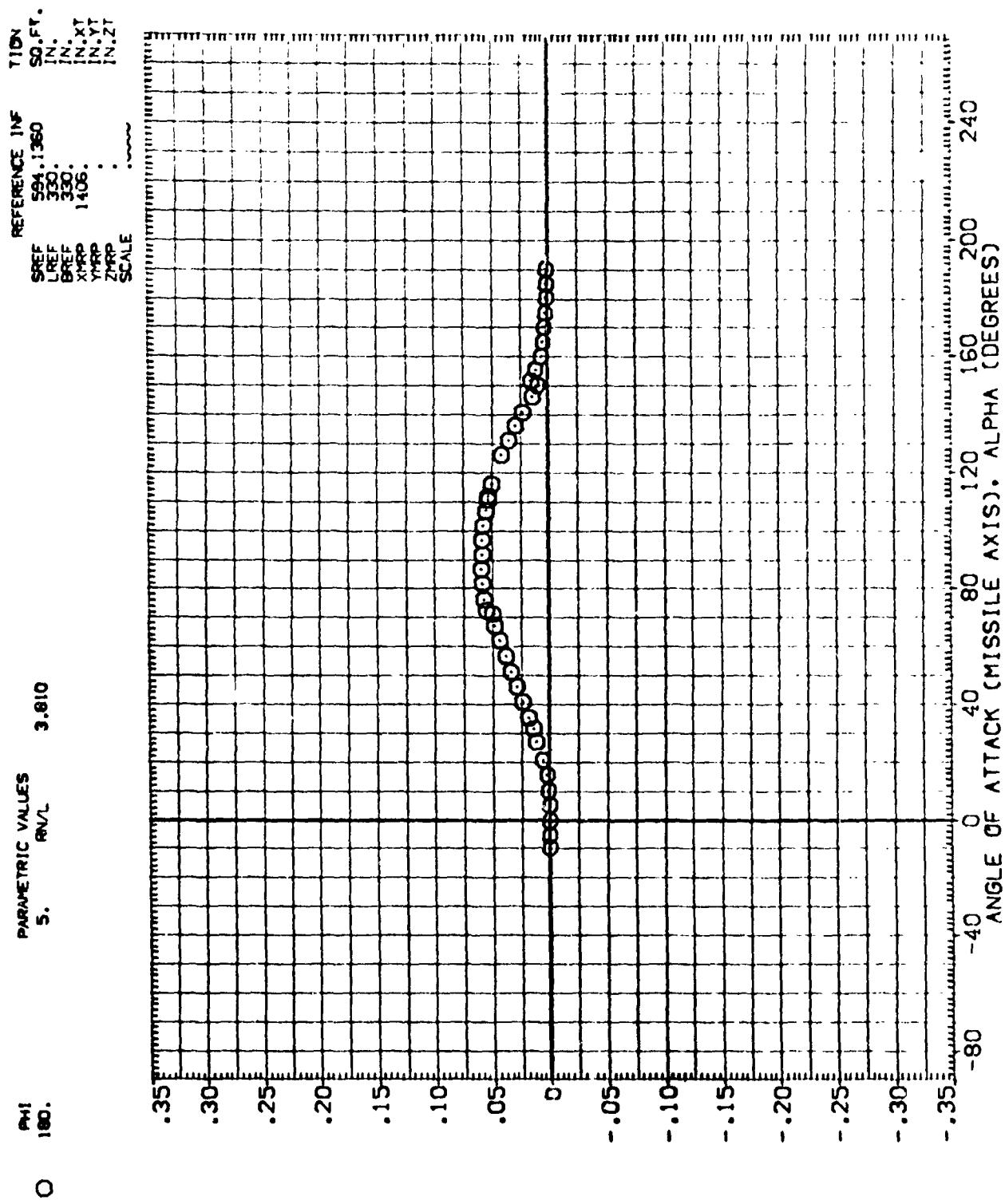


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

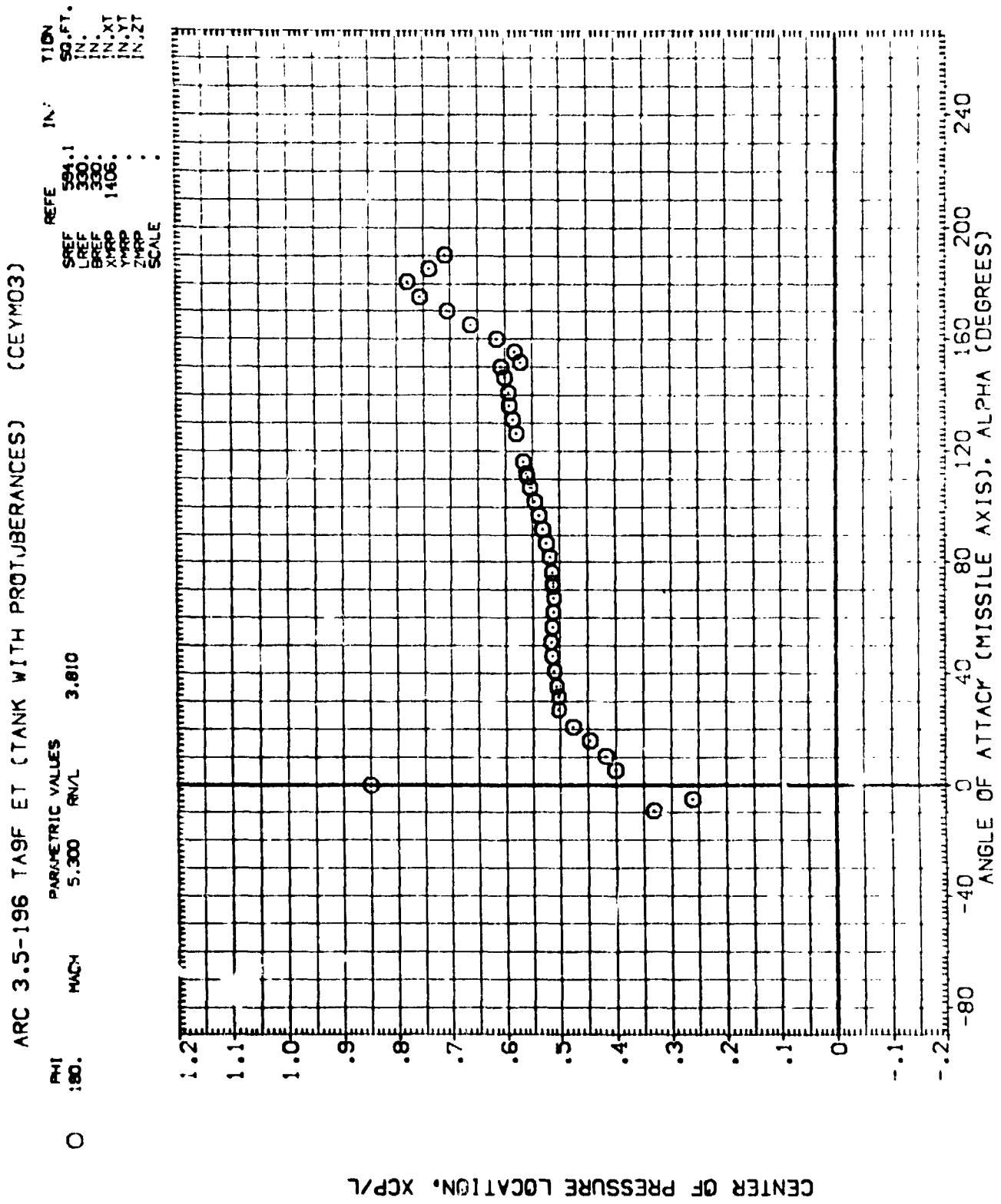


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (DEYMO3)

PARAMETRIC VALUES
PHI₁₀₀ 5.300 RNL 3.810

REFERENCE INFORMATION
LREF 554.1
BREF 330.
XHPP 330.
YHPP 140.
ZHPP .
IN. X1 IN.
IN. Y1 IN.
IN. Z1 IN.

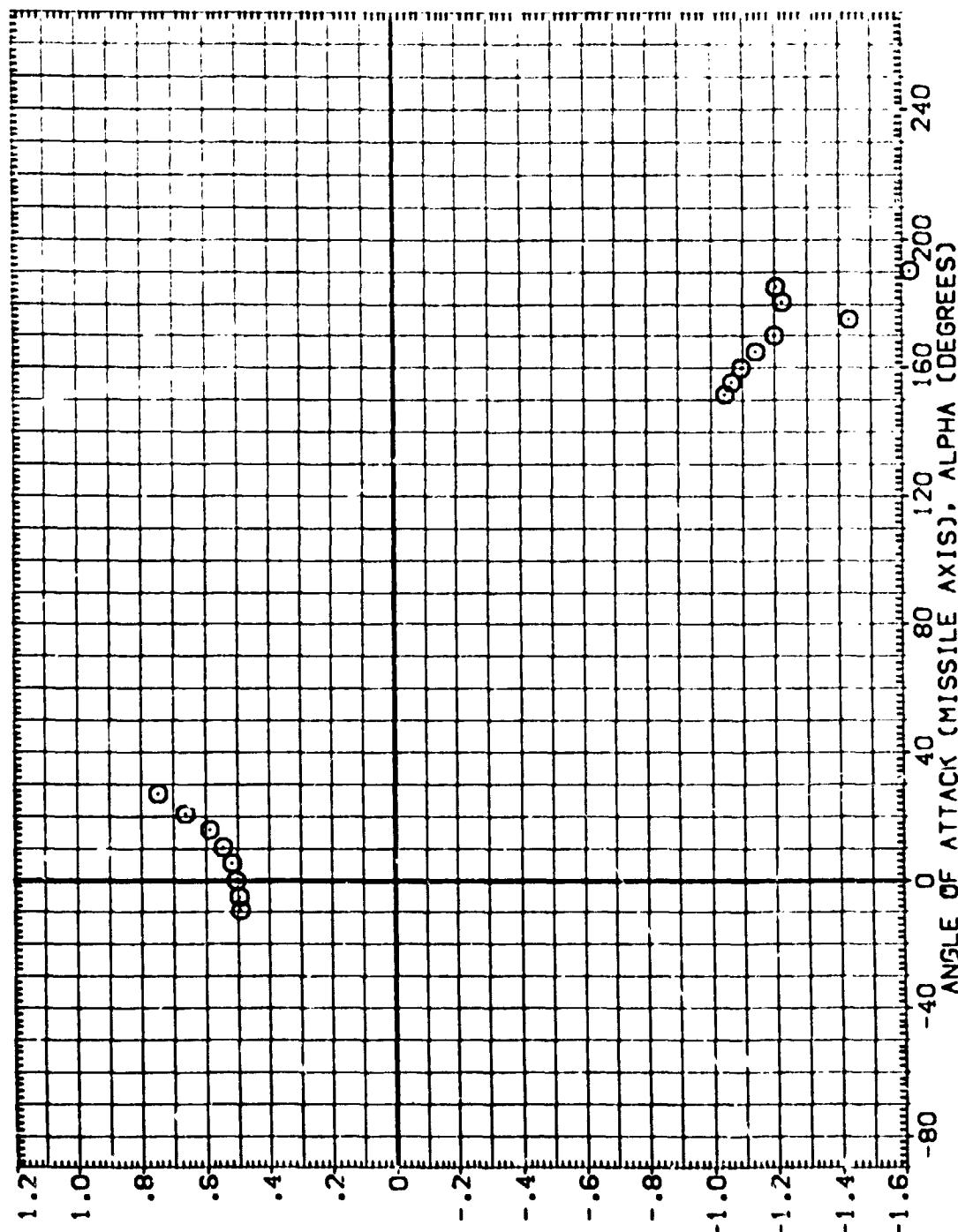
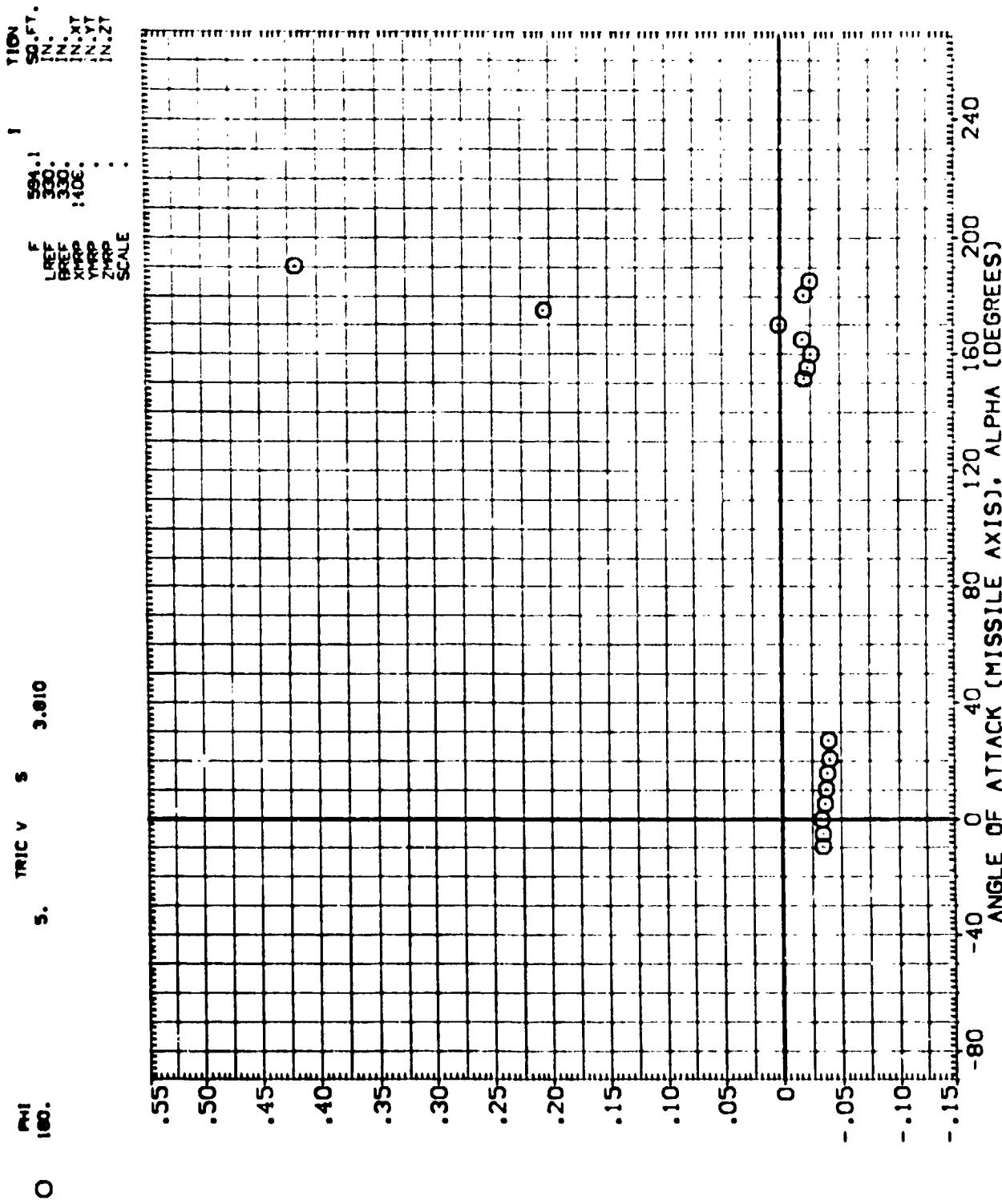


FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

A 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (DEYMO3)



BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS), C_{AB}

FIG. 6 COEFFICIENTS VERSUS ANGLE OF ATTACK

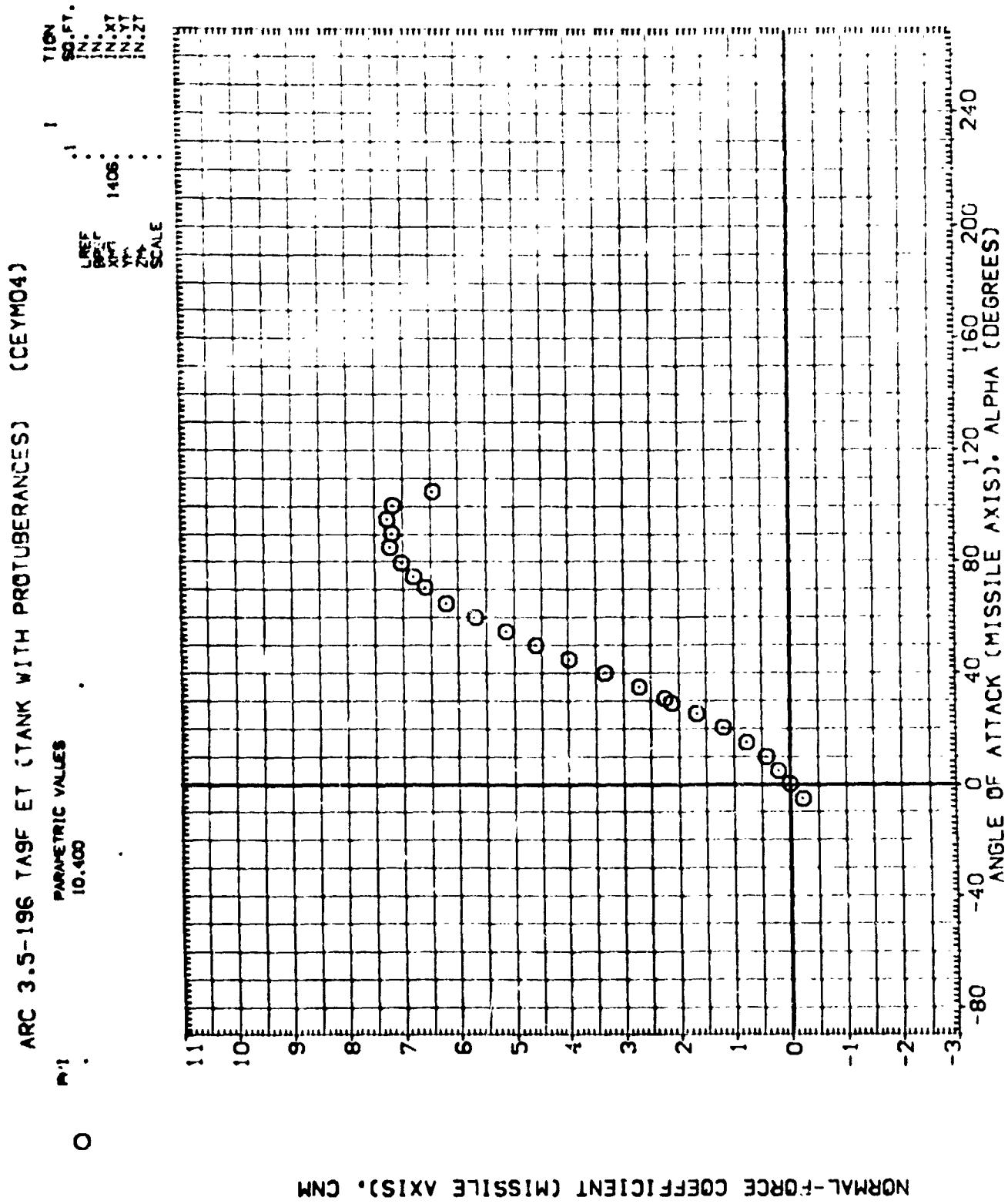


FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

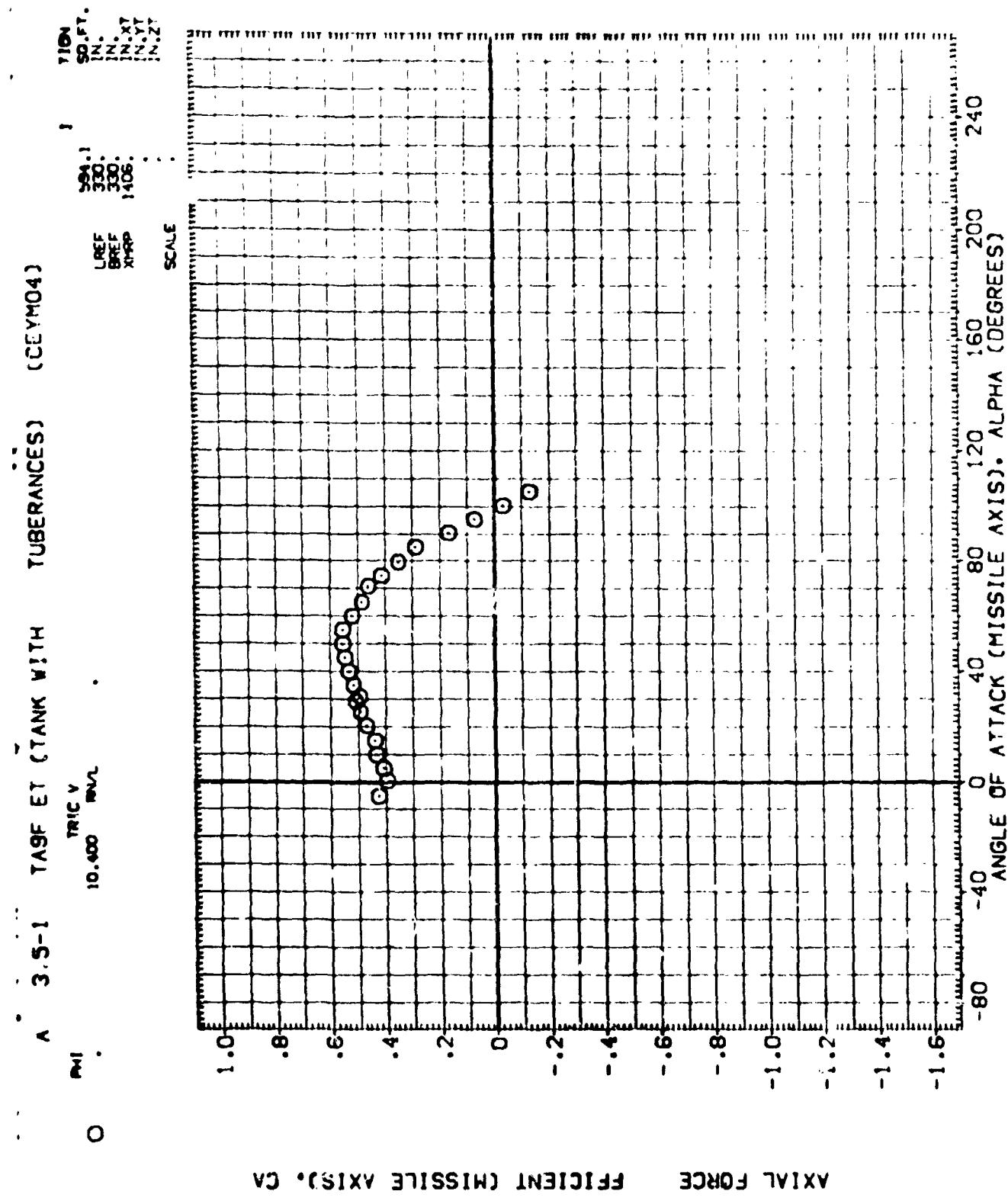


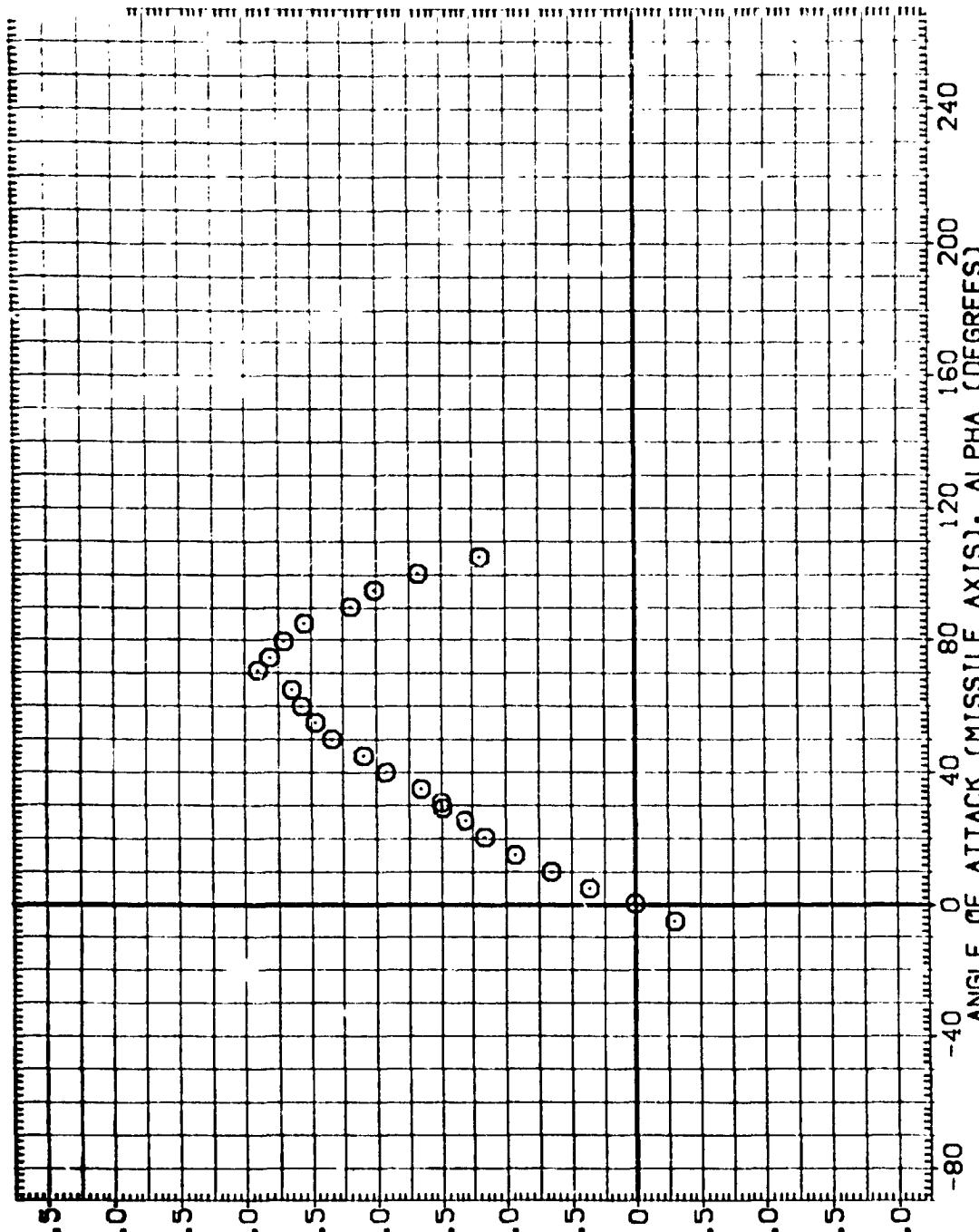
FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET TANK WITH PROTUBERANCES) [CEYMO4]

PARAMETRIC VALUES
10.400 RNL

REFERENCE INF
SQ.FT.
IN.
IN.XT
IN.YT
IN.ZT

SREF
LREF
BREF
XHPP
YHPP
ZHPP
SCALE



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CL

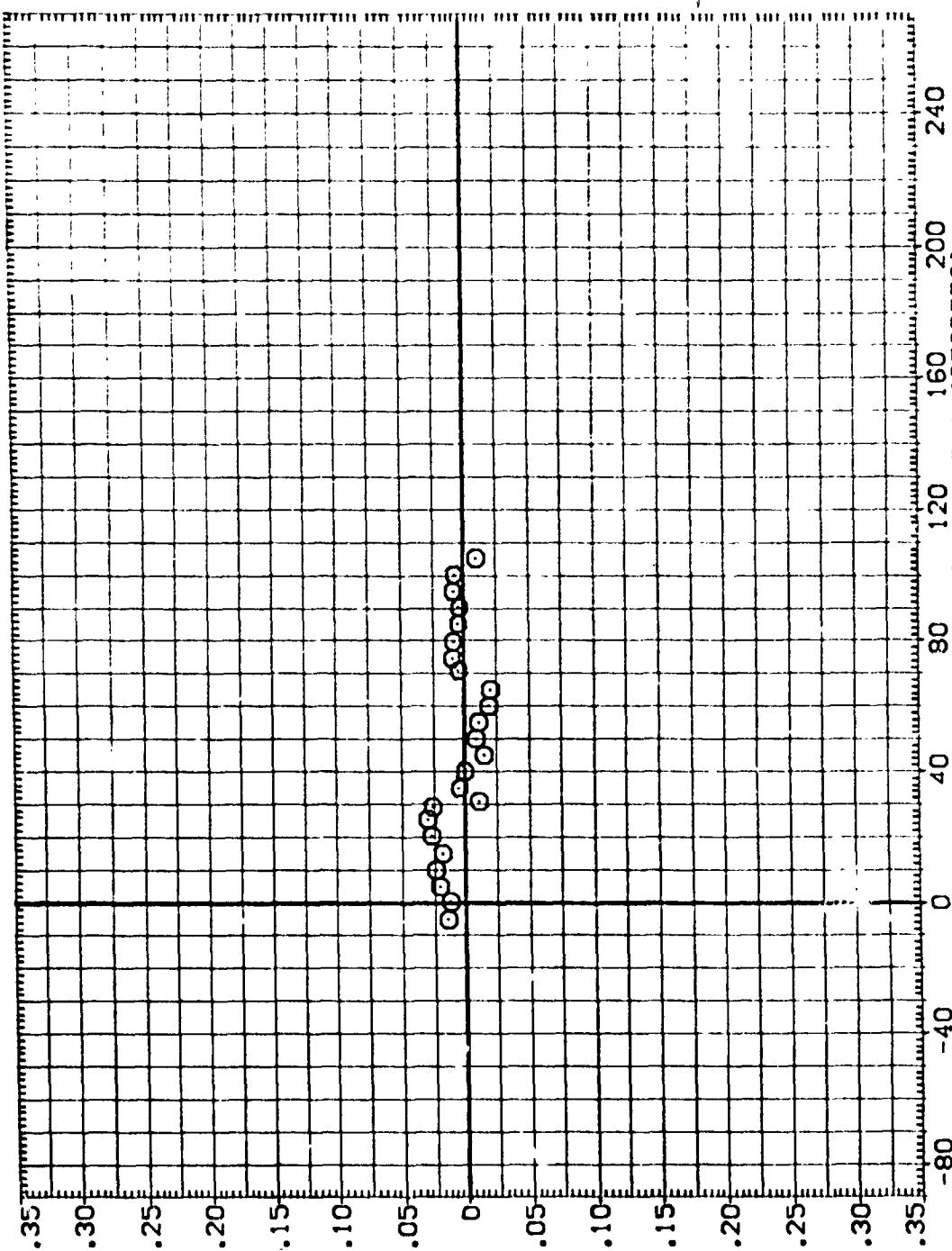
FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO4)

Φ TRIC VALUES
10.400 IN/L

TION
SO.FT.

SREF 594.1360
LREF 330.
BREF 330.
XMRP 146.
YMRP
ZMRP
SCALE



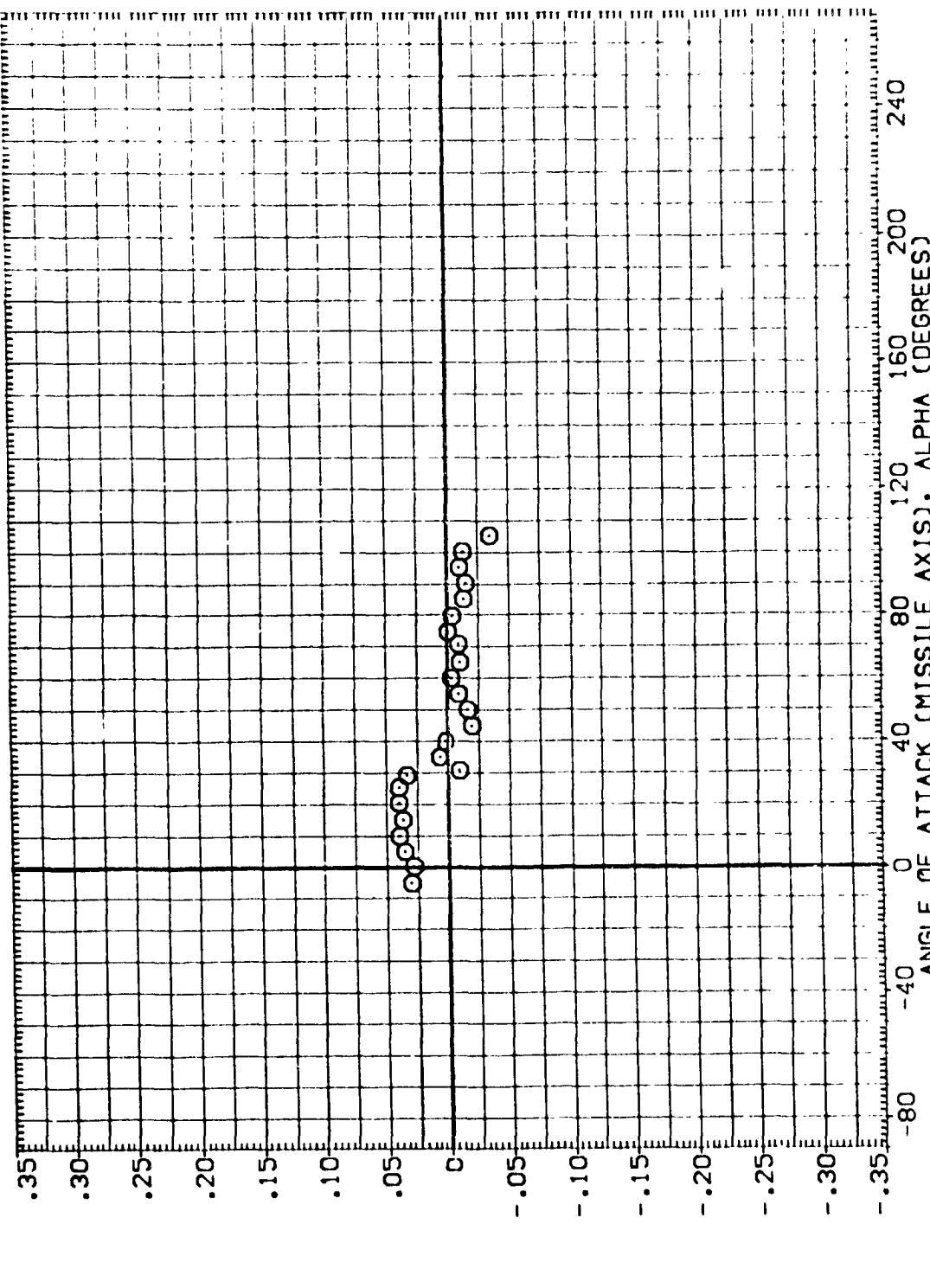
SIDE-FORCE COEFFICIENT (MISSILE AXIS). CYM

FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO4)

PARAMETRIC VALUES
 PHI .000 MACH 10.400 RNL 0

REFERENCE INF TION
 SREF 594.1360 SG. FT.
 LREF 330. IN.
 BREF 330. IN.
 XMRP 1408. IN.XT
 YMRP .0000 IN.YT
 ZMRP .0000 IN.ZT
 SCALE



YAWING MOMENT COEFFICIENT (MISSILE AXIS). CYNM

FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET TANK WITH PROTUBERANCES) (CEYMO4)

PHI
0.000 MACH 10.400 RNL .390

PARAMETRIC VALUES
REF.
LREF
BREF
XMP
YMP
ZMP
SCALE

REFERENCE INF

SQ.FT.

IN.

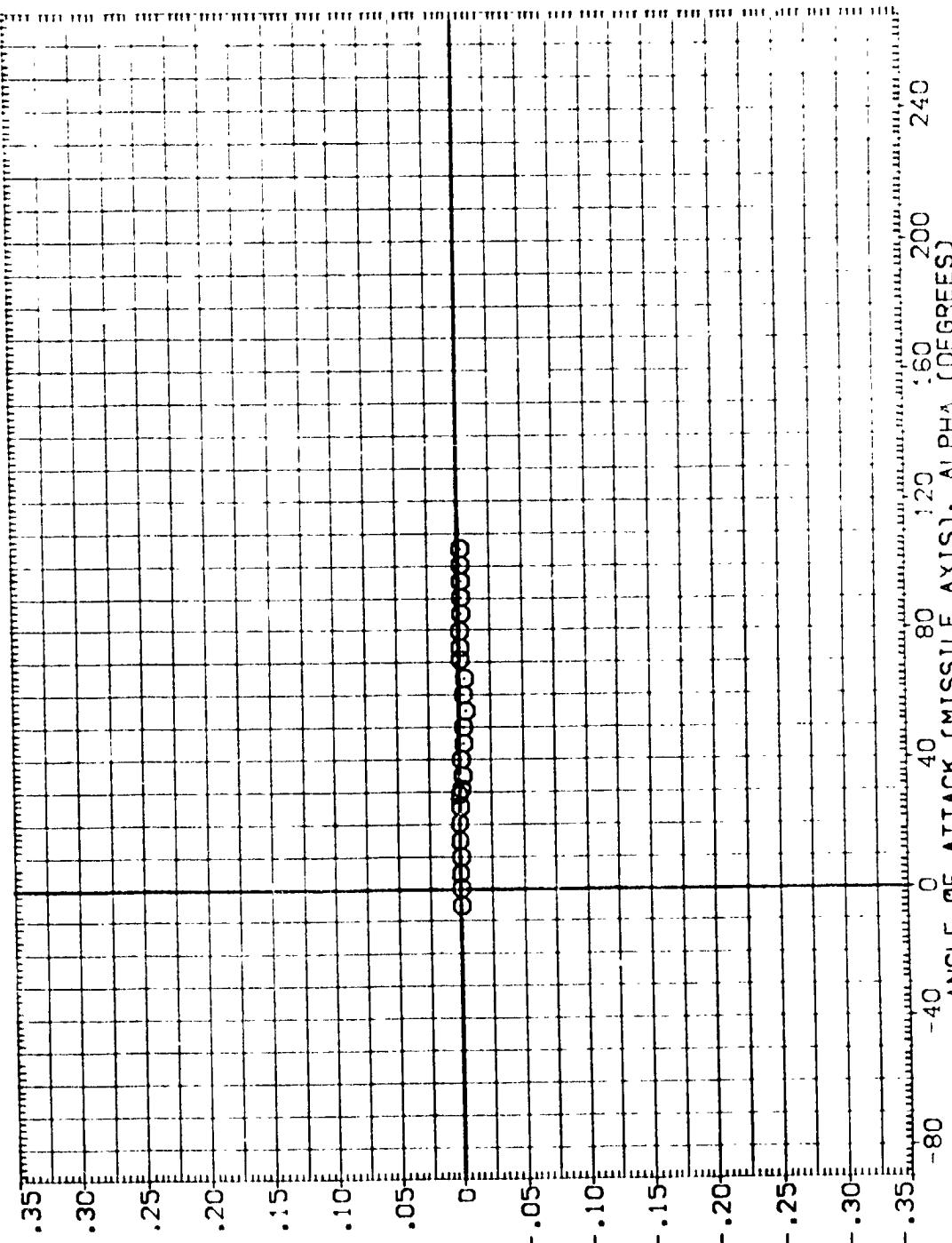
IN.

IN.XT

IN.YT

IN.ZT

.00850

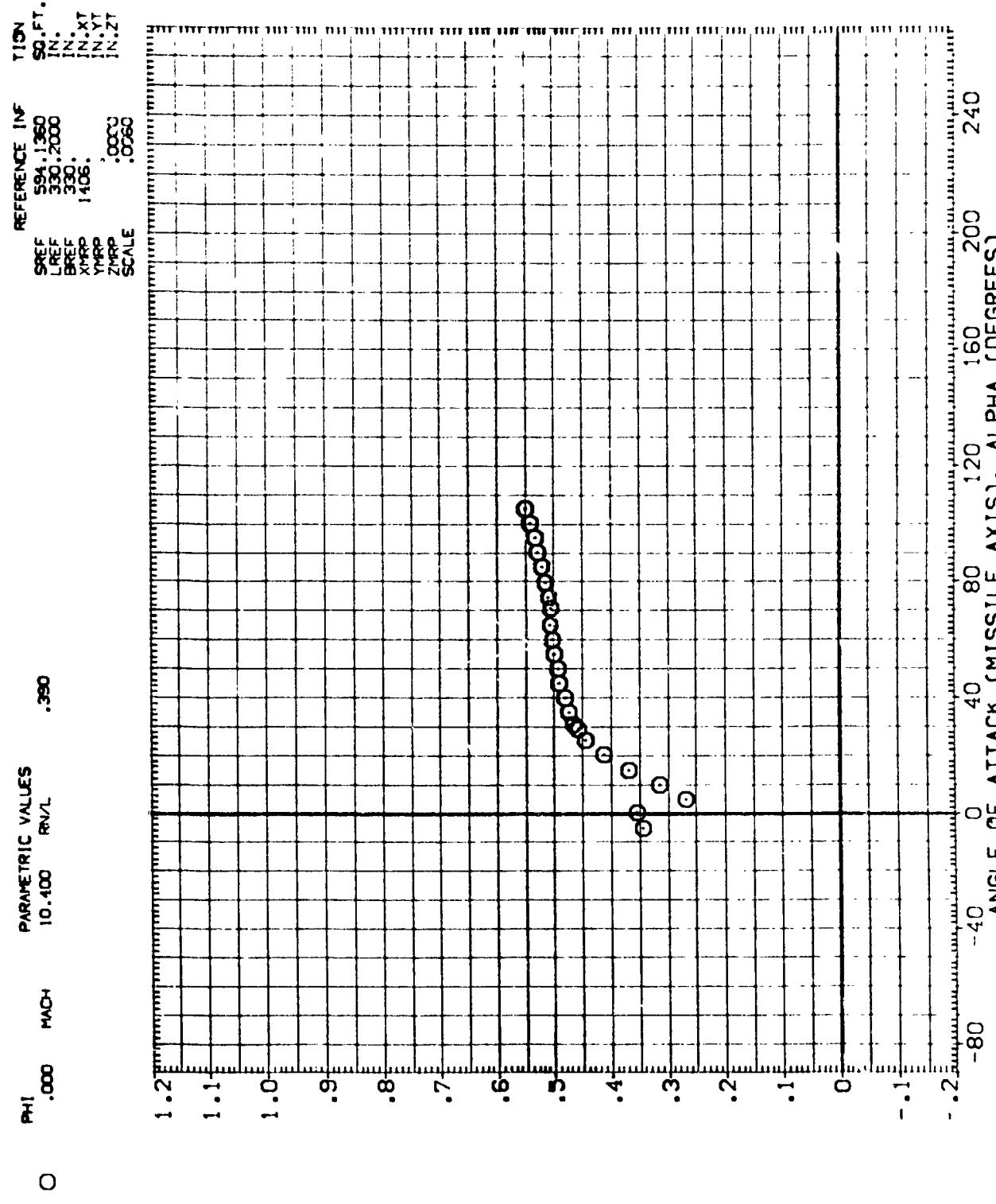


ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

PAGE 42

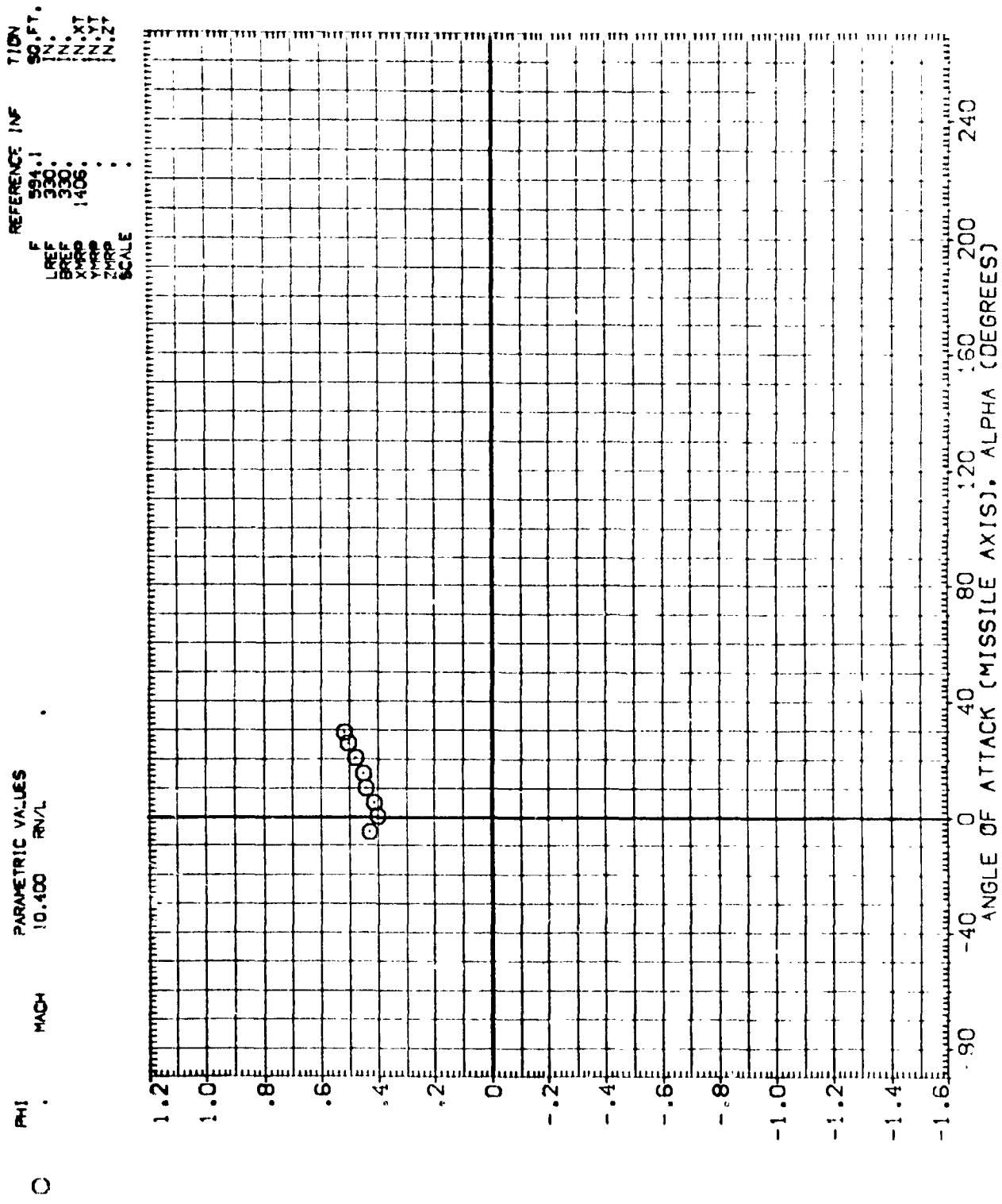
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO4)



CENTER OF PRESSURE LOCATION, XCP/L

FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (BEYMA4)



PAGE 44

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (BEYMA4)

PHI . MACH 10.400 P_A/V_A TRIC VALUES

REFERENCE IN
SO.FT.
SREF 594.1360
LREF 330.
BREF 330.
XMRP 1406.
YMRP 240
ZMRP 240
SCALE

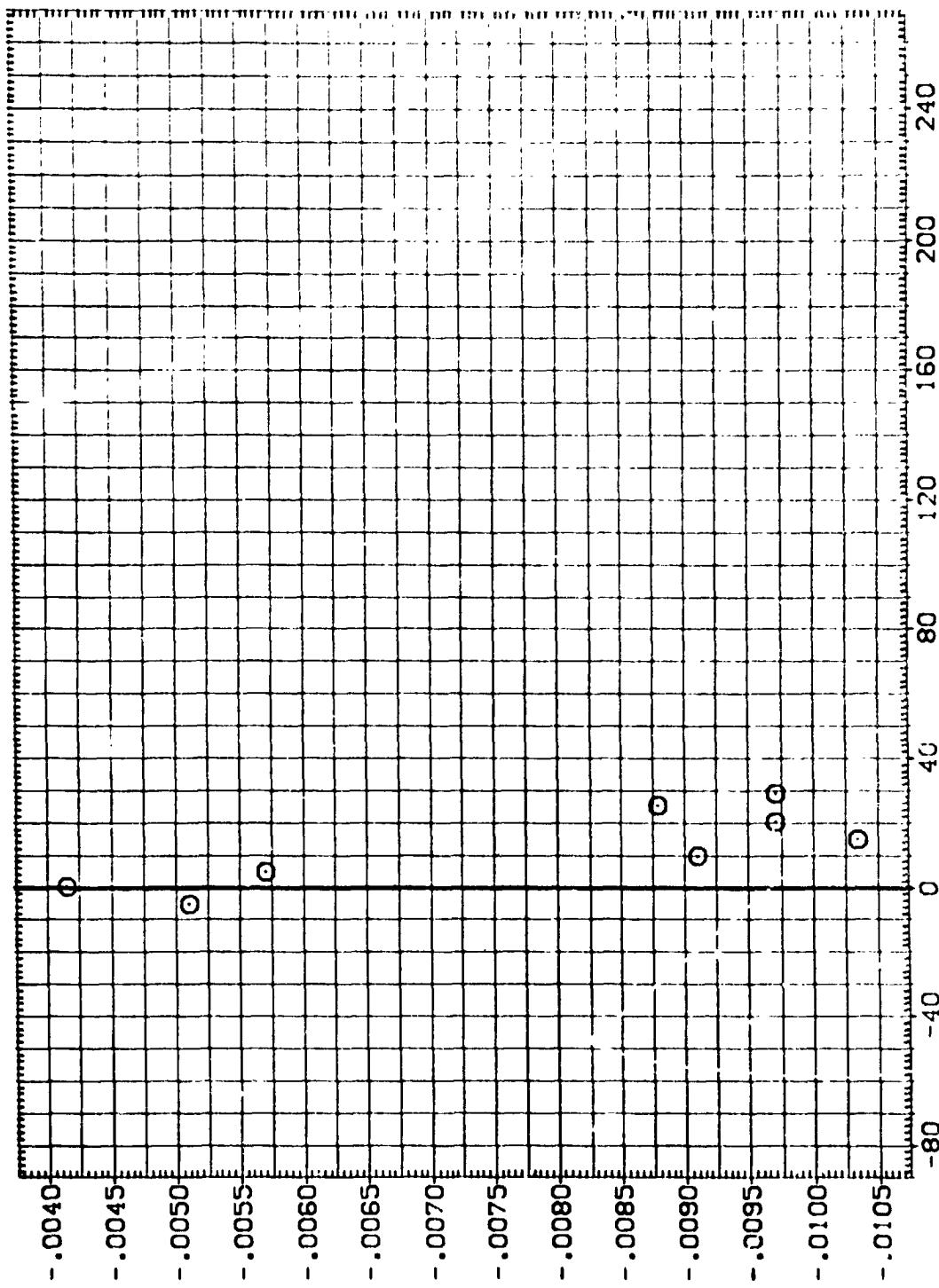


FIG. 7 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTRUSIONS) (CEYMO5)

PHI P TRIC VALUES 10.400 RVAL 1.740

11 10 9 8 7 6 5 4 3 2 1 0 -1 -2

TION SQ.FT. IN.

SREF 594.1360 IN.XT

LREF 330. IN.YT

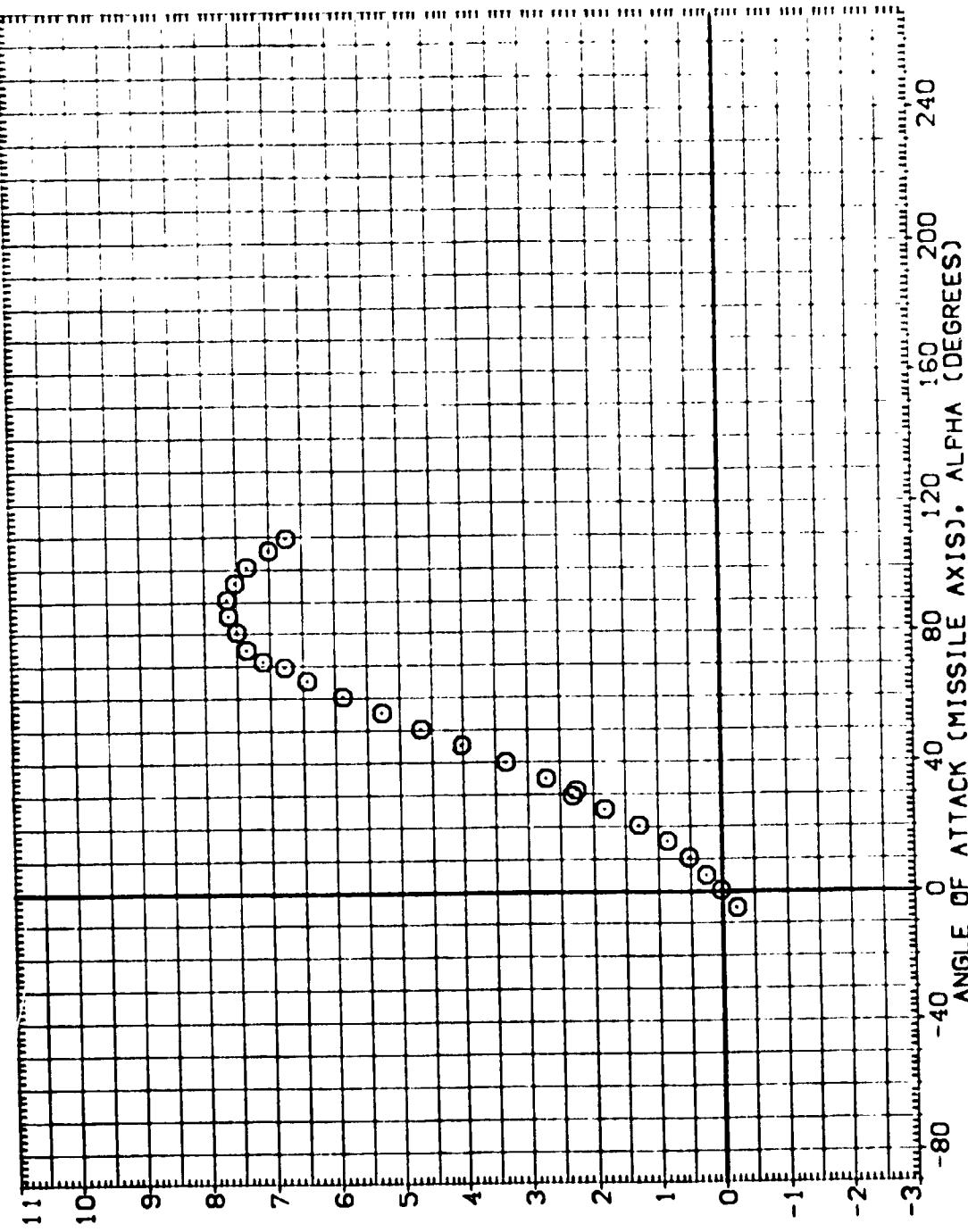
BREF 330. IN.ZT

XHPP 1406. IN.ZT

YHPP 2446. IN.ZT

ZHPP 1000. IN.ZT

SCALE



NORMAL-FORCE COEFFICIENT (MISSILE AXIS), CnM

FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

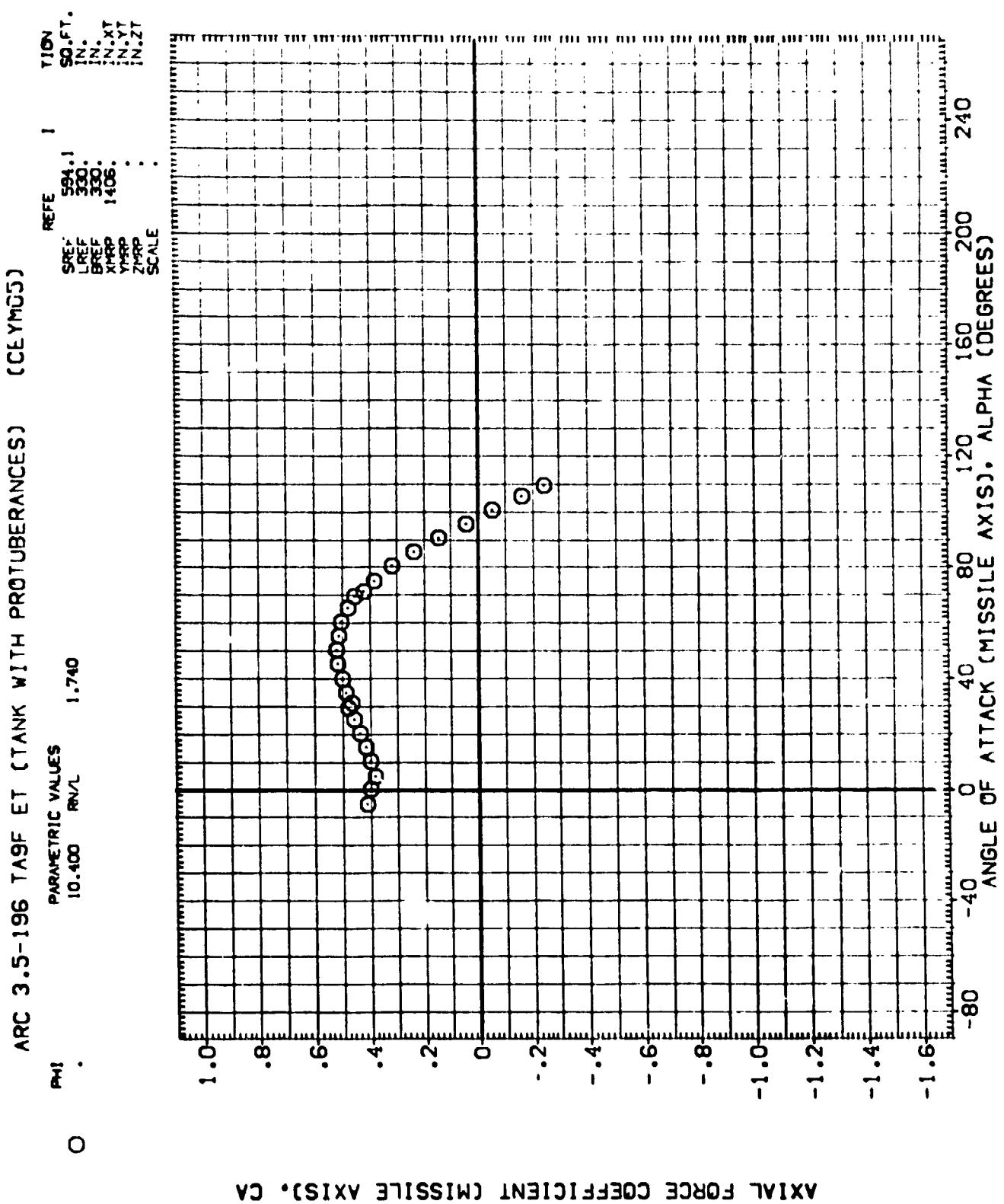
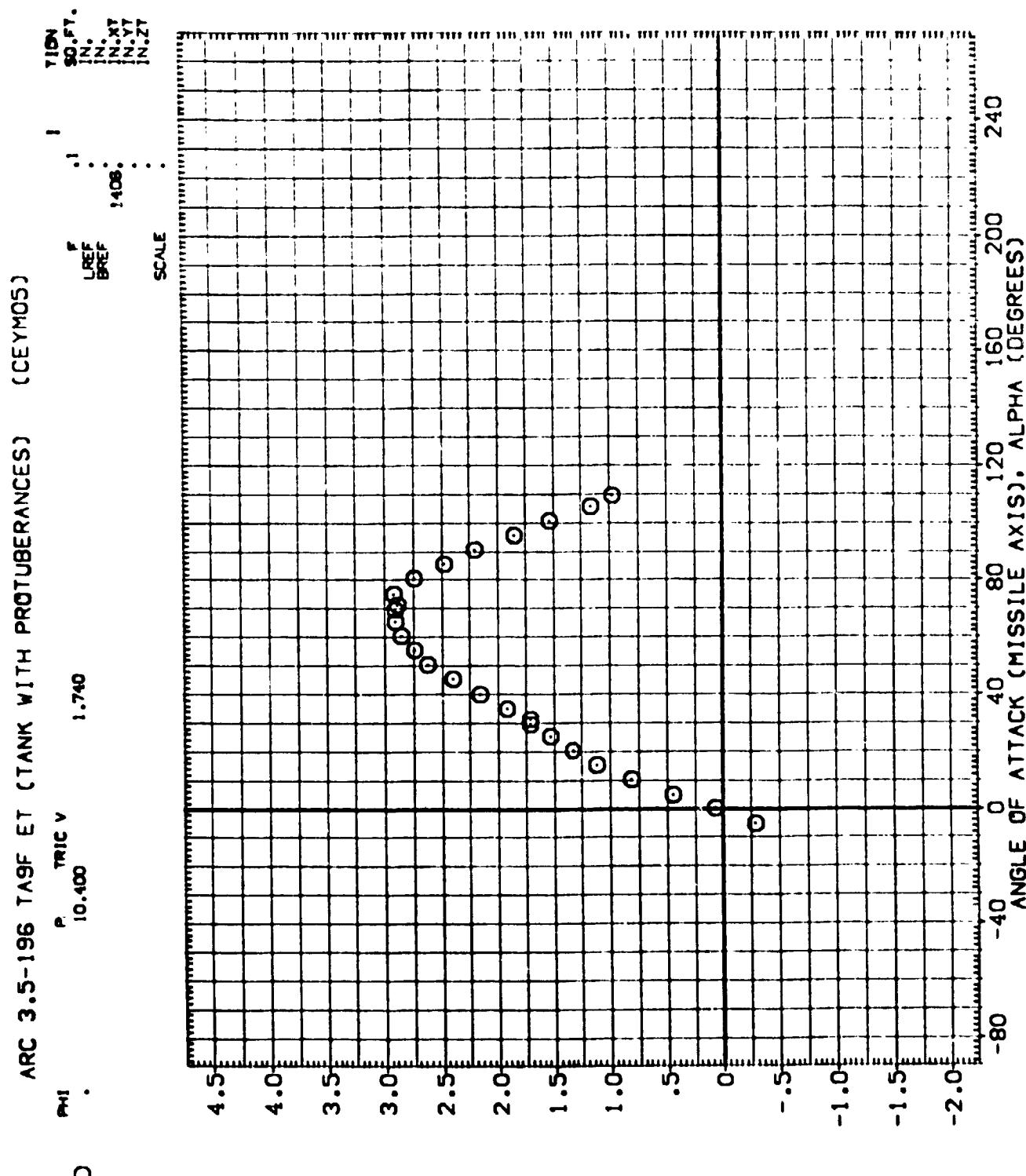


FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLM

FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

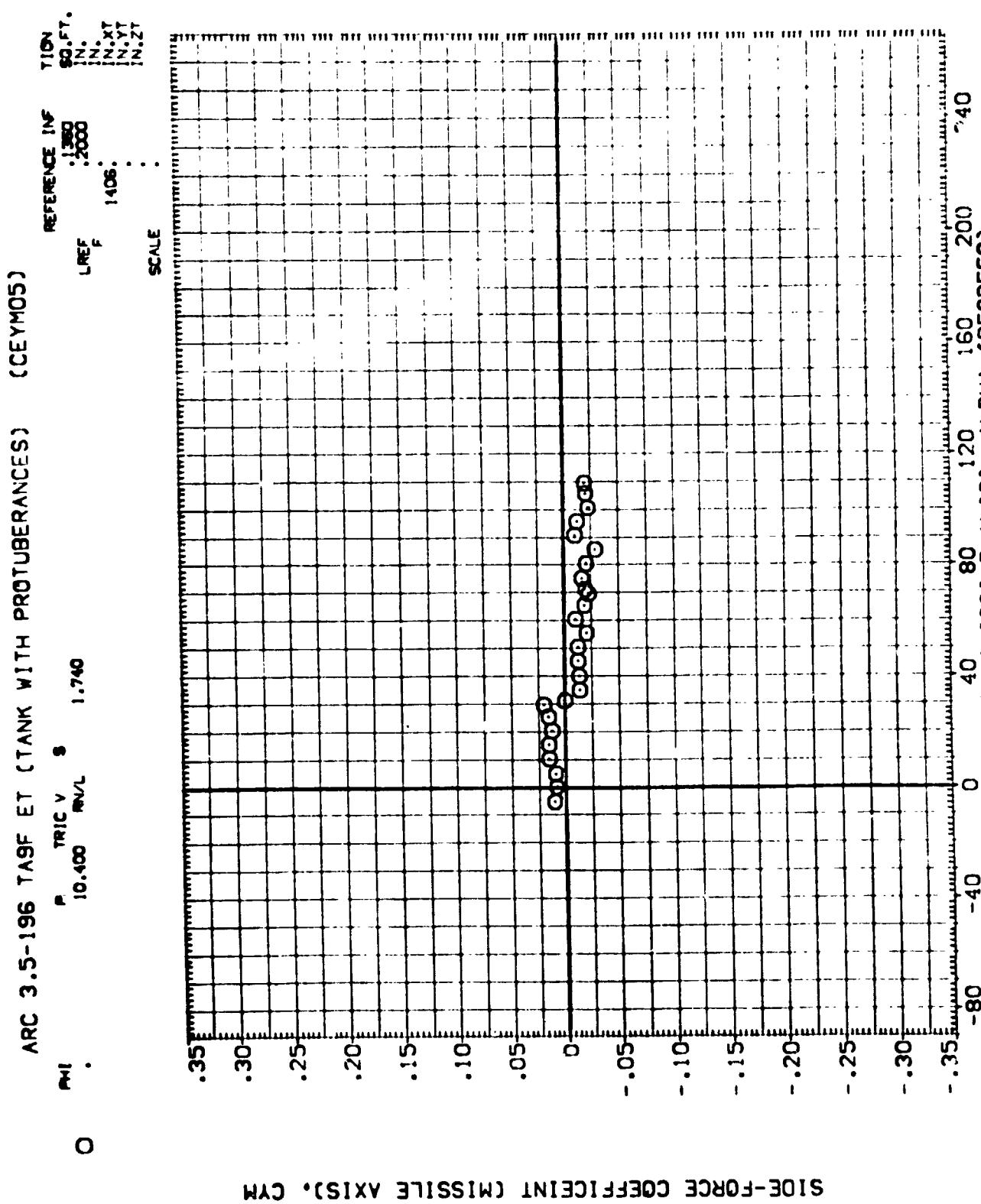


FIG. 8 COEFFICIENTS VE VS ANGLE OF ATTACK

APC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (CEYMO5)

PRO.
TRIC V
10.
1.740

LEEF
330.
146.

SCALE

IN.
IN. X
IN. Y
IN. Z

O

YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

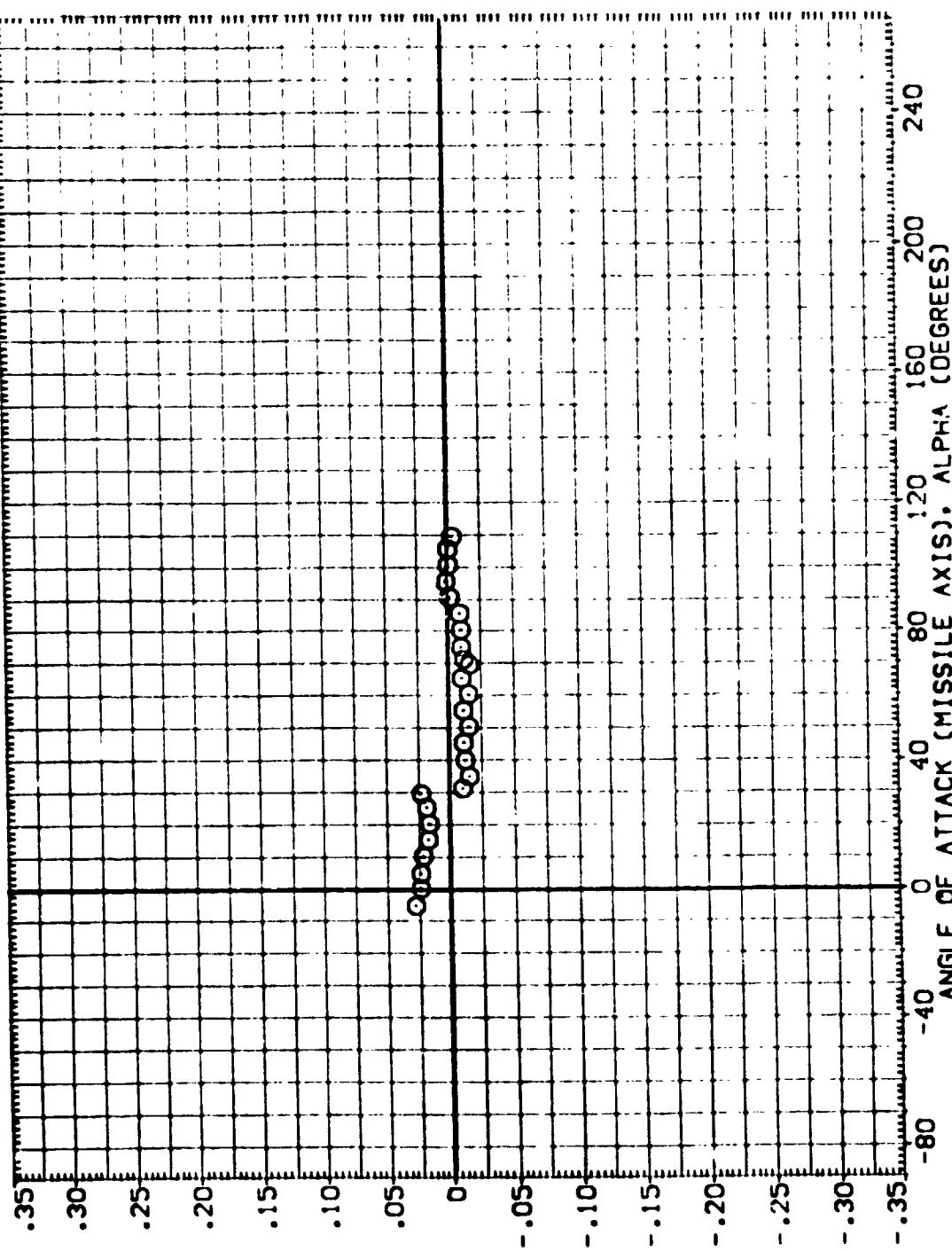


FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

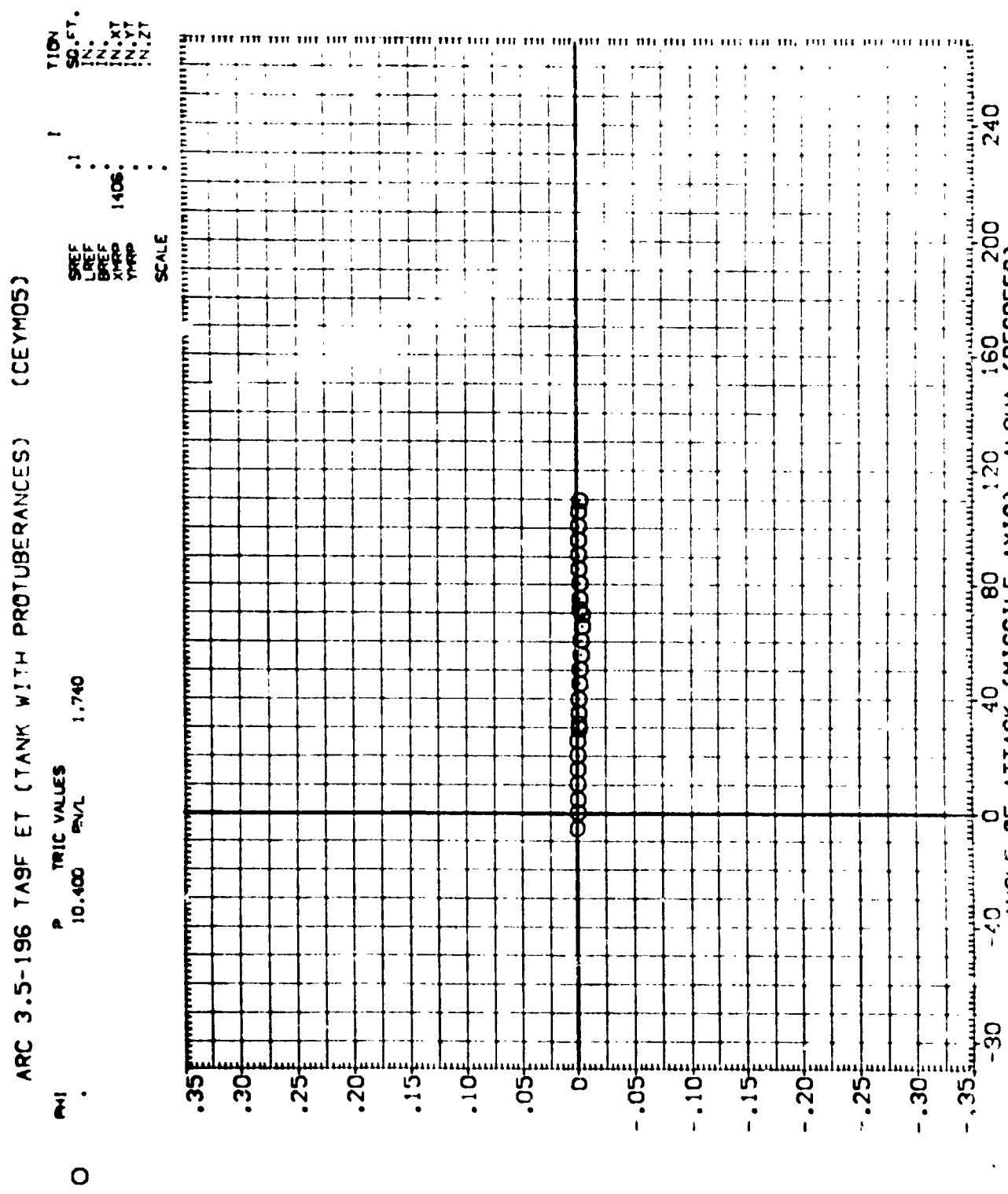
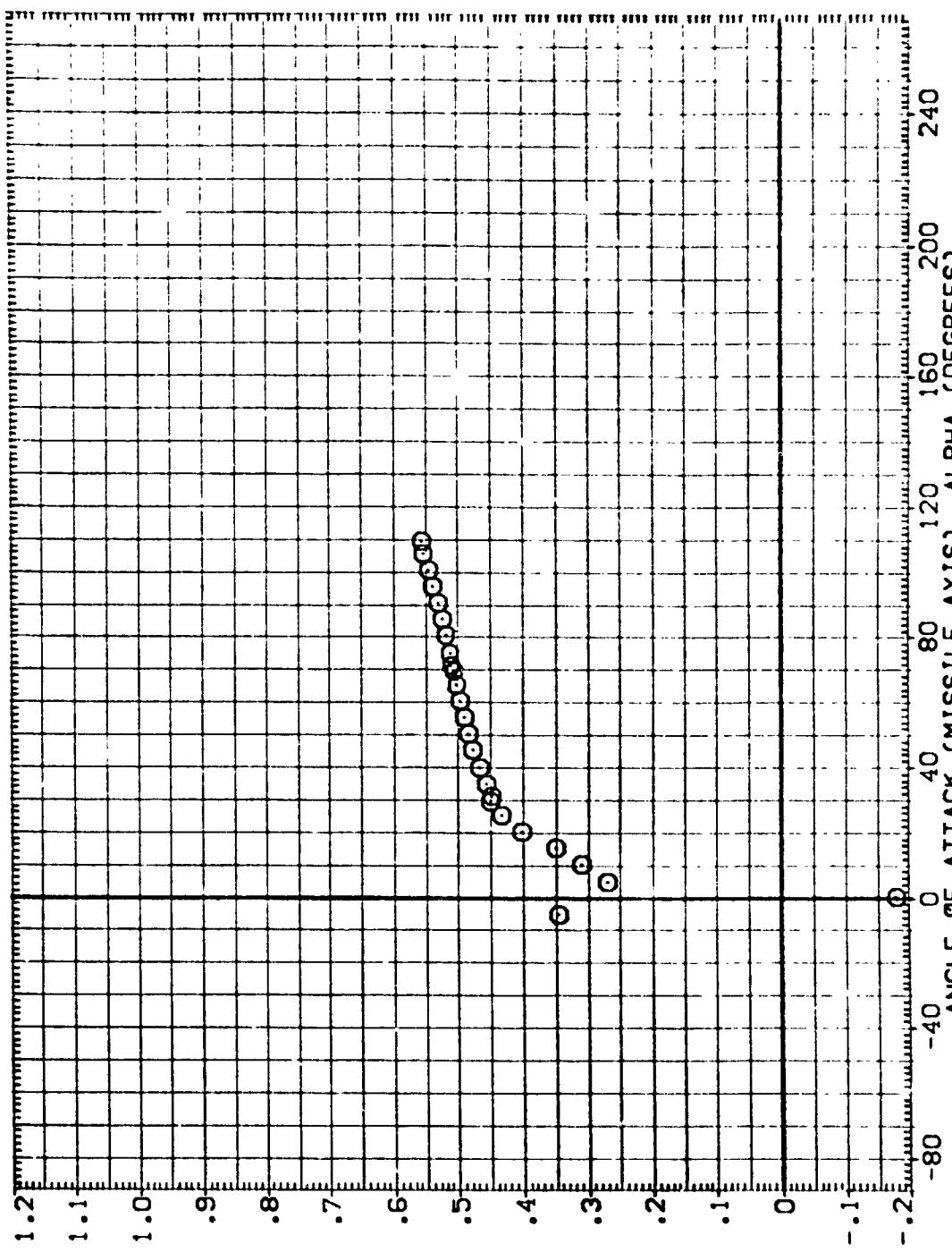


FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET CTANK WITH PROTUBERANCES) (CEYMO5)

PHI
PARAMETRIC VALUES
10.400 ANGL 1.740

REF 594.1
LREF 330.
BREF 330.
XMRP 1406.
YMRP 2400.
ZMRP 1000.
SCALE



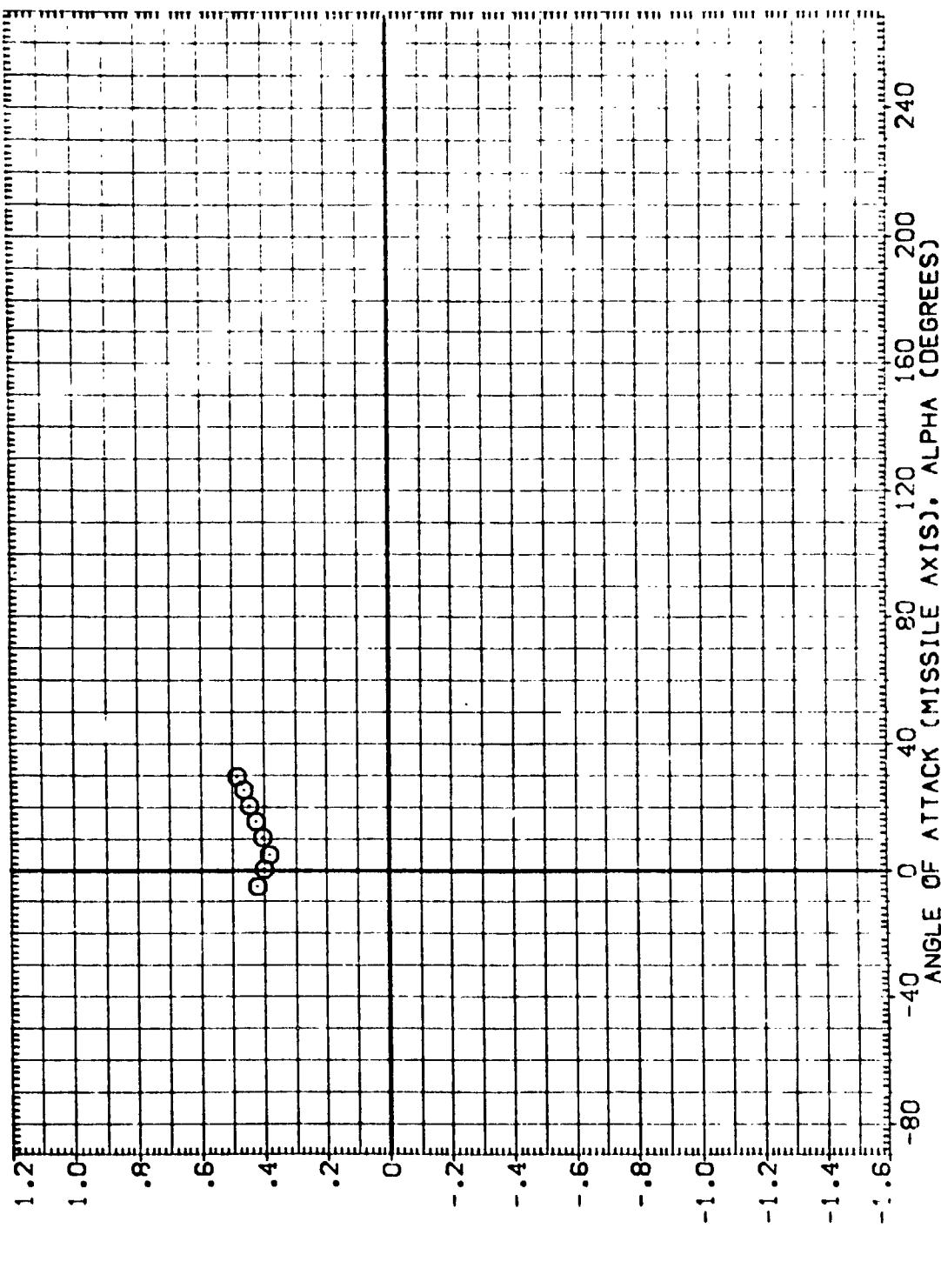
CENTER OF PRESSURE LOCATION, XCP/L

FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (BEYMAS)

PHI. MACH 10.41W RNSL 1.740

PARAMETRIC VALUES
REFERENCE INFORMATION
SREF 594.1
LREF 330.
BREF 330.
XMRP 146.
YMRP
ZMRP
SCALE



FOREBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAF

FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (BEYMAS)

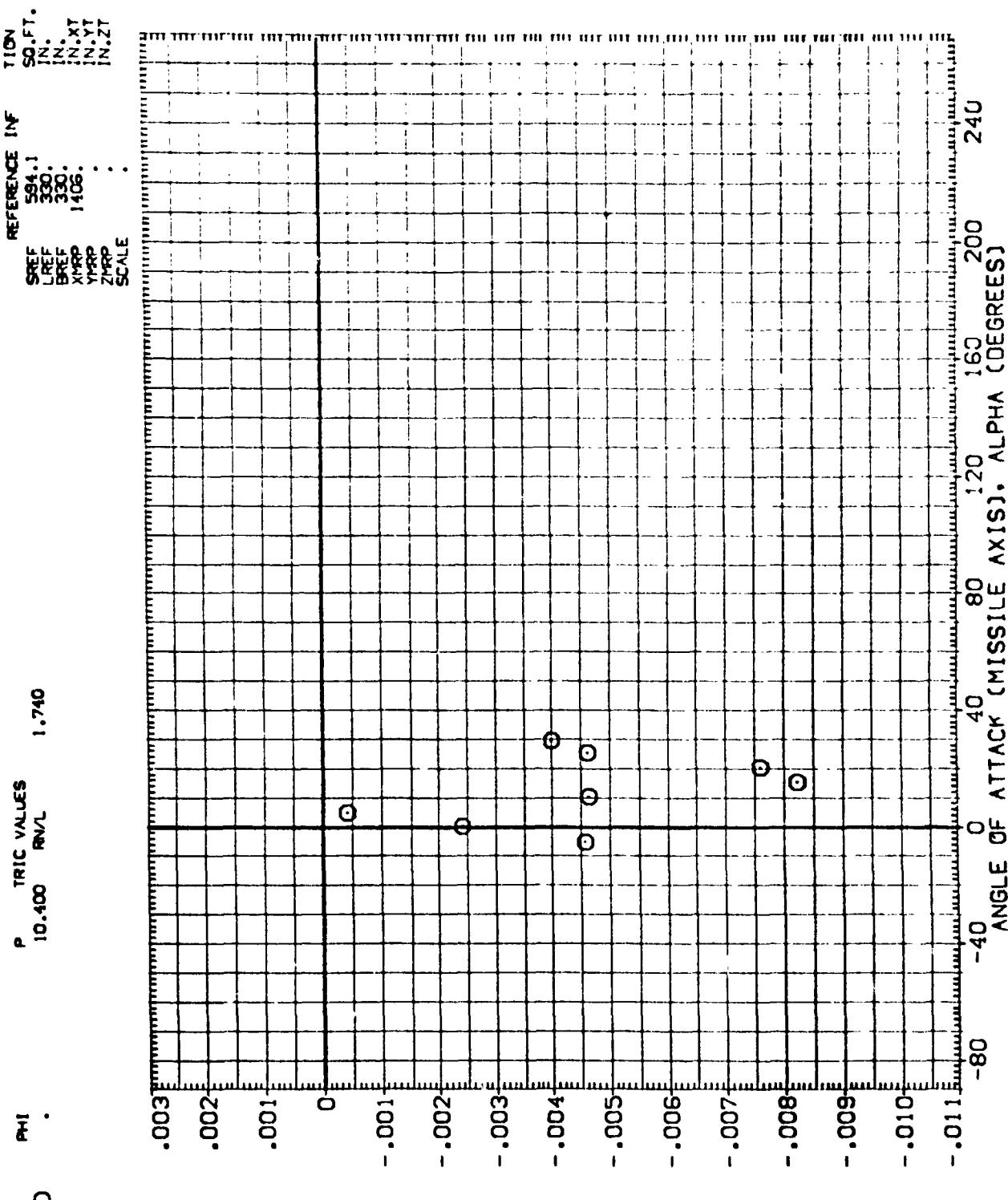


FIG. 8 COEFFICIENTS VERSUS ANGLE OF ATTACK

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	PARAMETRIC VALUES
-5.000	.000	10.400 RNU/L
5.000	.000	
10.000	.000	

○ □ ◇ △

REFERENCE INFORMATION
 SREF 594.1360 SQ.FT.
 LREF 330. IN.
 BREF 330. IN.
 XMRP 1406. IN.XT
 YMRP . IN.YT
 ZMRP . IN.ZT
 SCALE .

NORMAL-FORCE COEFFICIENT [MISSILE AXIS], CNM

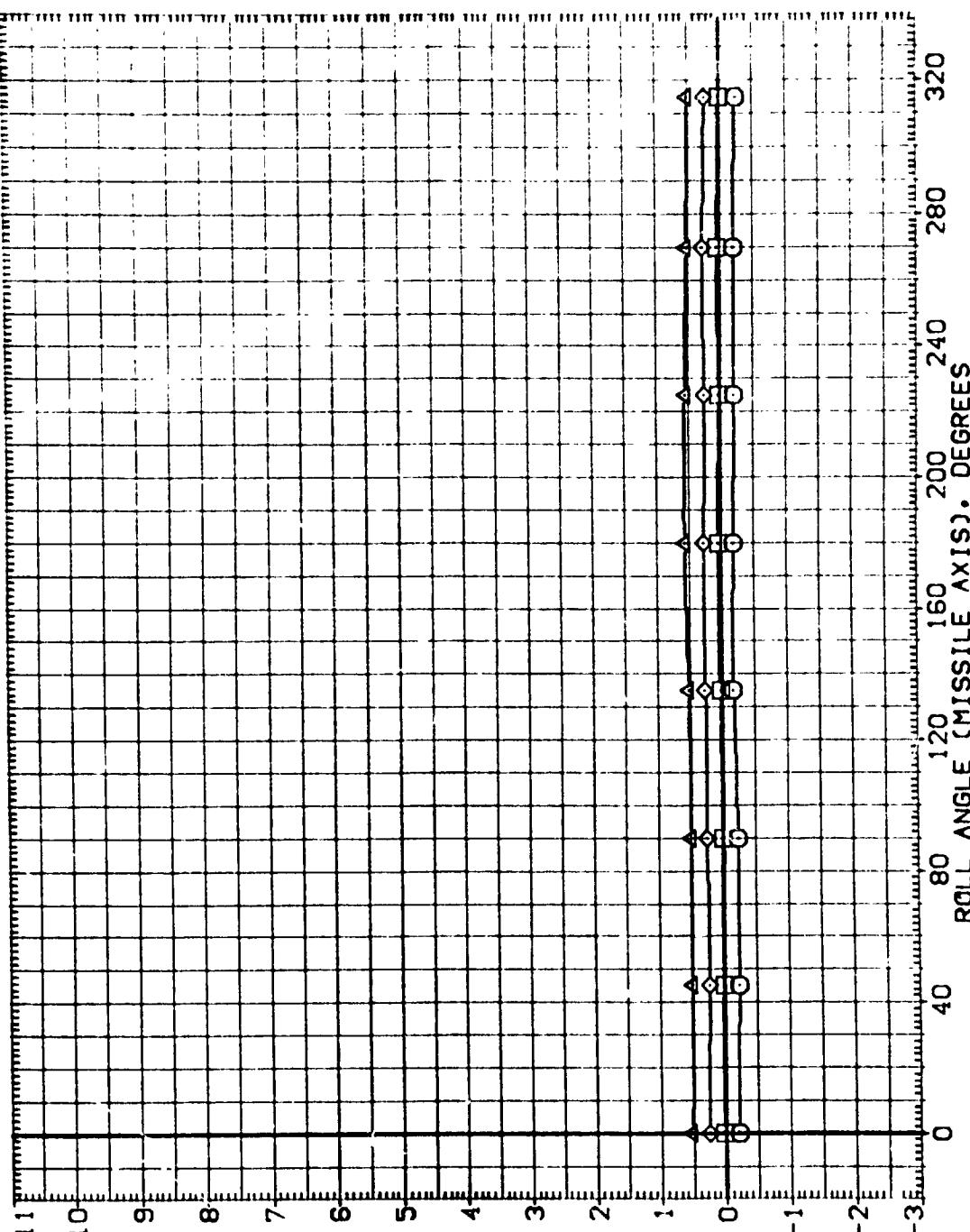
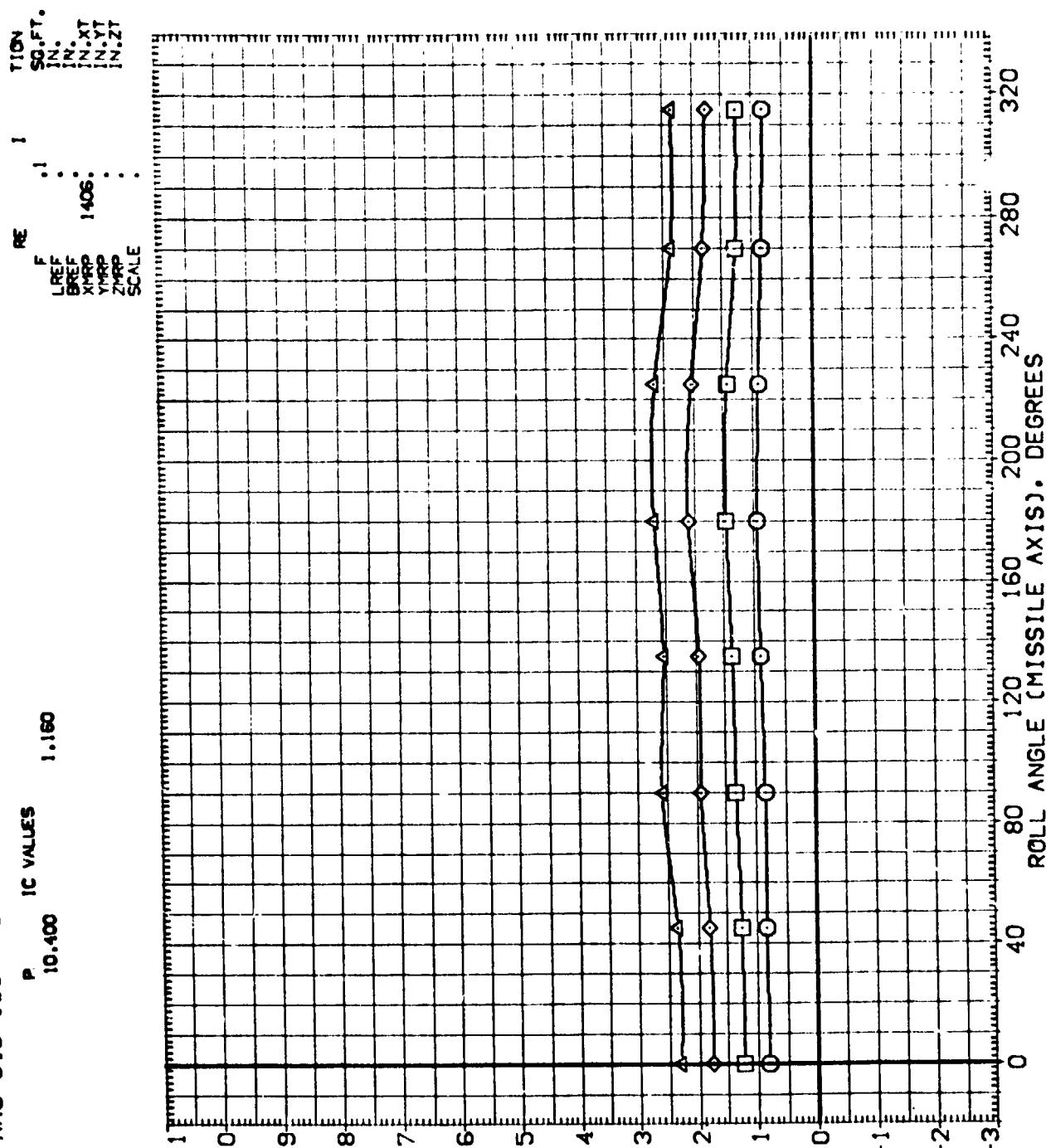


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMC1)

IC VALUES 1.160
 10.400 1.160
 15.
 20.
 25.
 30.
 O □ ◊ △



NORMAL-FORCE COEFFICIENT (MISSILE AXIS), CNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	PARAMETRIC VALUES
30.000		10.400 RNU 1.160
35.000		
40.000		
45.000		

REFERENCE	INF	TION
SREF	594.1360	SC.FT.
LREF	330.2000	IN.
SREF	330.2000	IN.X
X ² RPP	1406.0000	IN.Y
Y ² RPP	.0000	IN.Z
Z ² RPP	.0000	
SCALE	.0000	

O □ ◇ △

NORMAL-FORCE COEFFICIENT (MISSILE AXIS). CNM

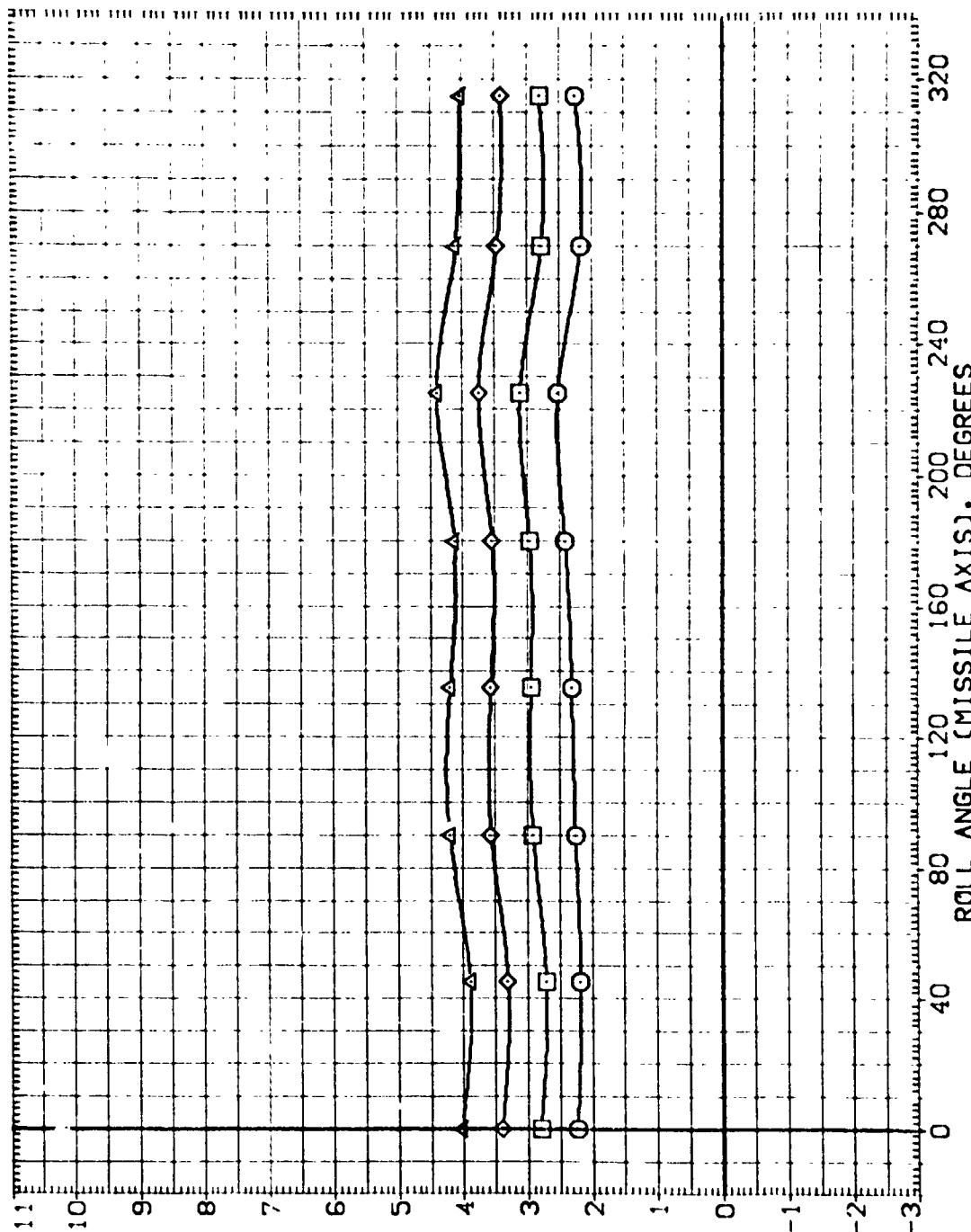


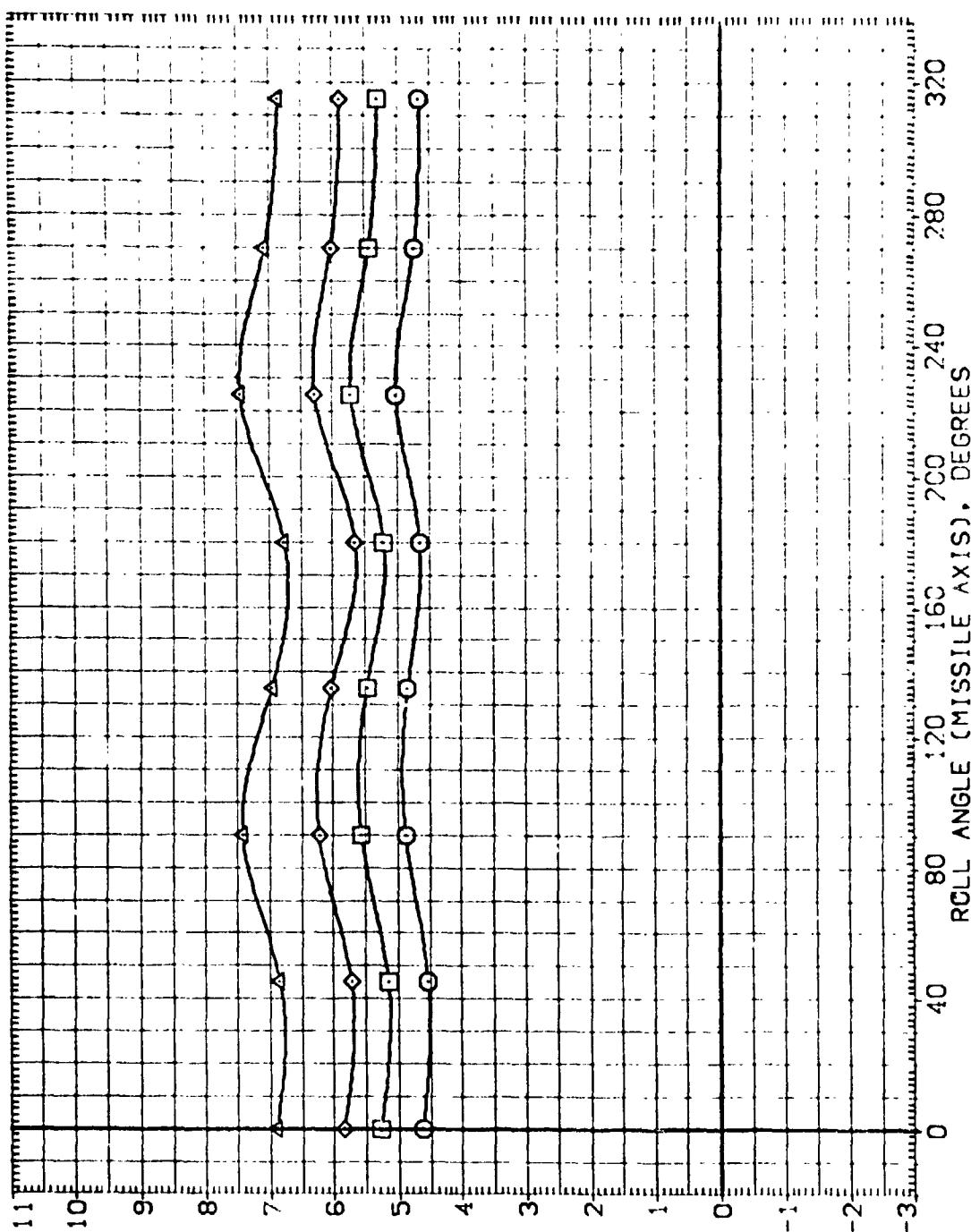
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) [NEYMO1]

PARAMETRIC VALUES
 ALPHA 50.000 MACH 10.400 ROLL 1.160

REFERENCE INFORMATION
 SREF 594.1360 SO.FT.
 LREF 330.2000 N.
 BPF 330.2000 N.
 KAPP 1406.0000 N.XT
 YAPP 0.0000 N.YT
 ZAPP .0000 N.ZT

SCALE



NORMAL-FORCE COEFFICIENT (MISSILE AXIS), CNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

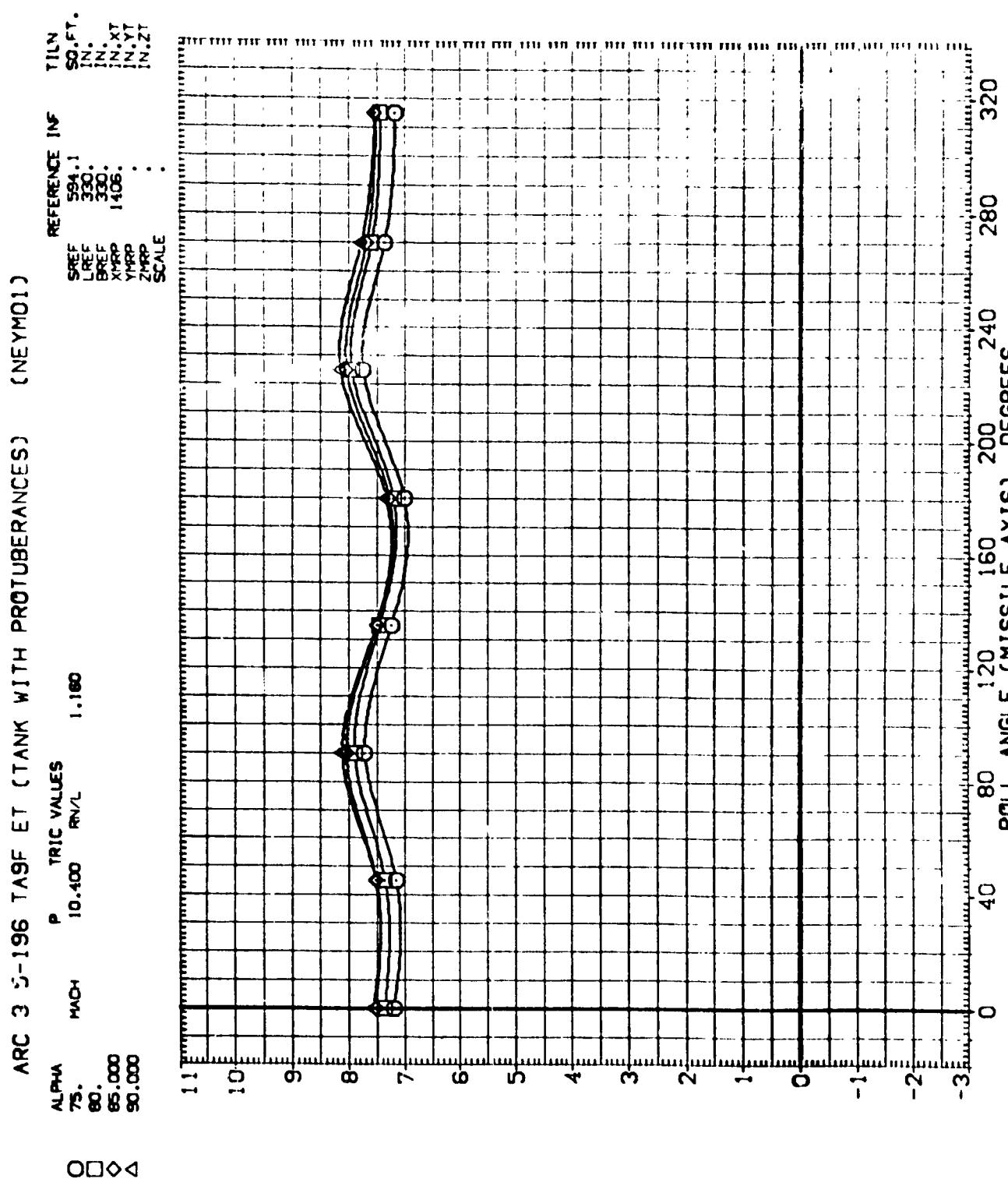


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

POLYTRIC VALUES
10,400 RNL 1.160

55.
100.
105.
110.000

□ ◇ △

TION
80. FT.
IN.
IN. XT
IN. YT
IN. ZT
SCALE

NORMAL-FORCE COEFFICIENT (MISSILE AXIS), CNM

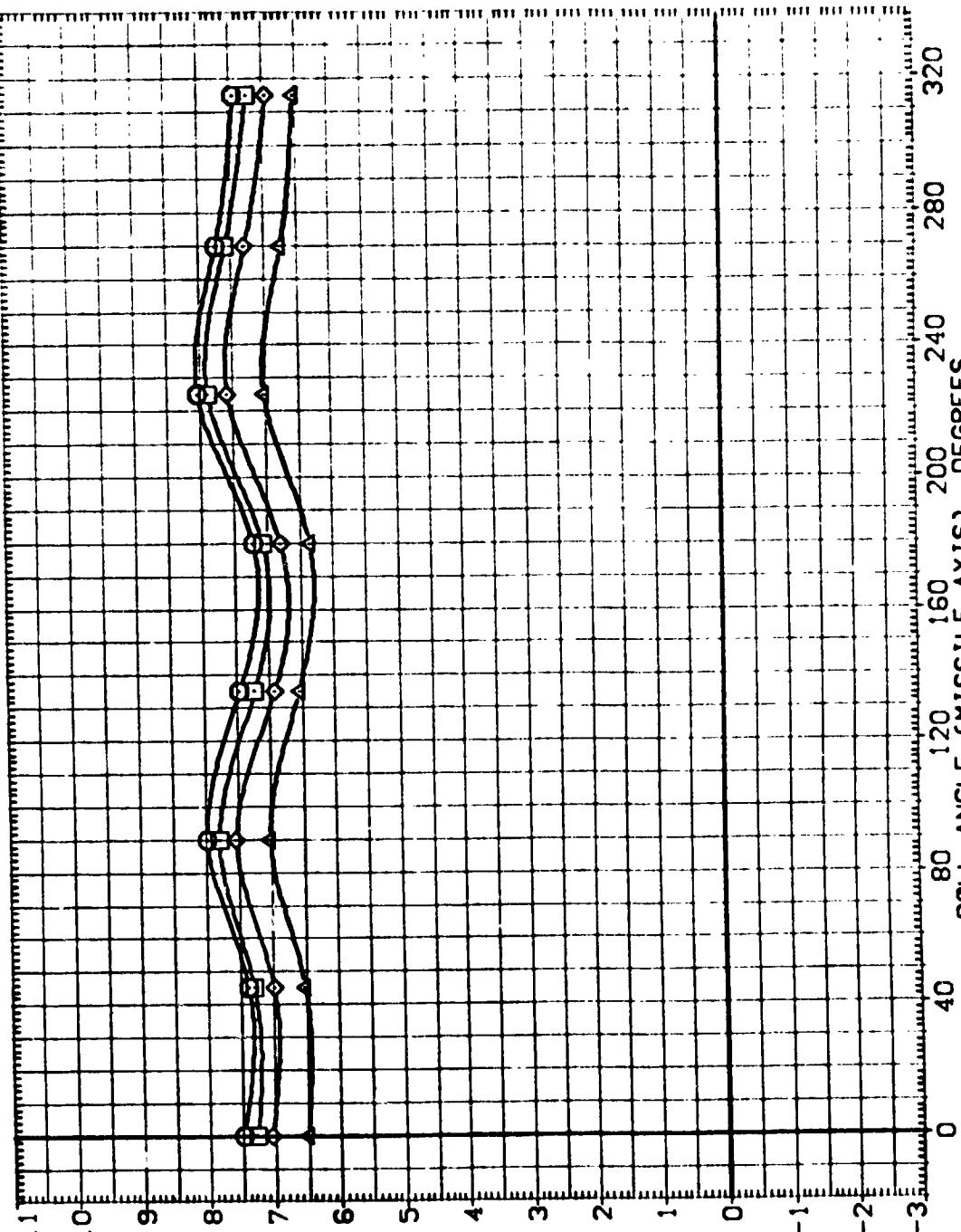


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

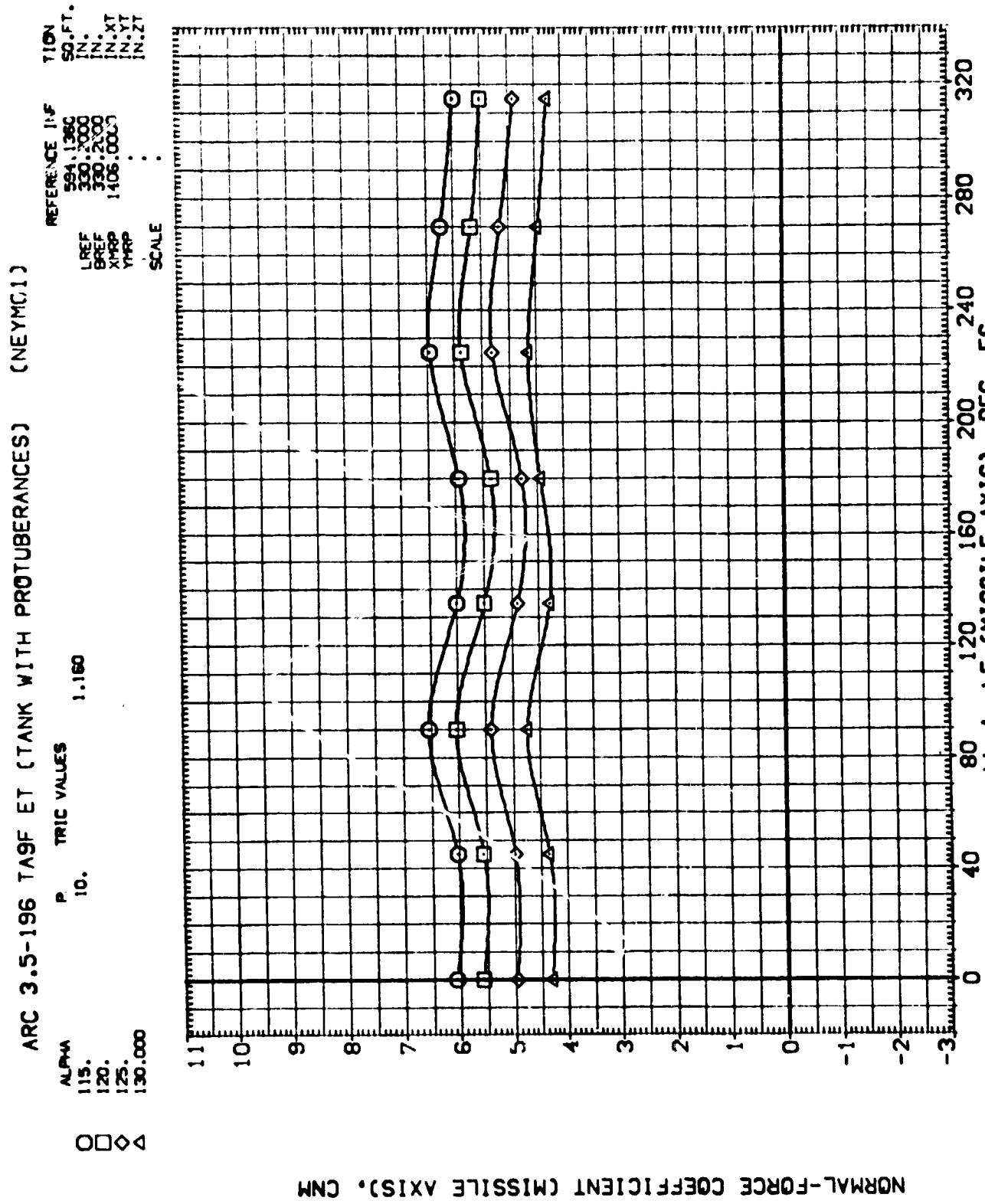


FIG. 9 COEFFICIENTS VE ANGLE OF L

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) [NEYMO1]

P TRIC VALUES
10,400 RNU/L 1.160

135.
140.
145.
150.

○ □ ◇ △

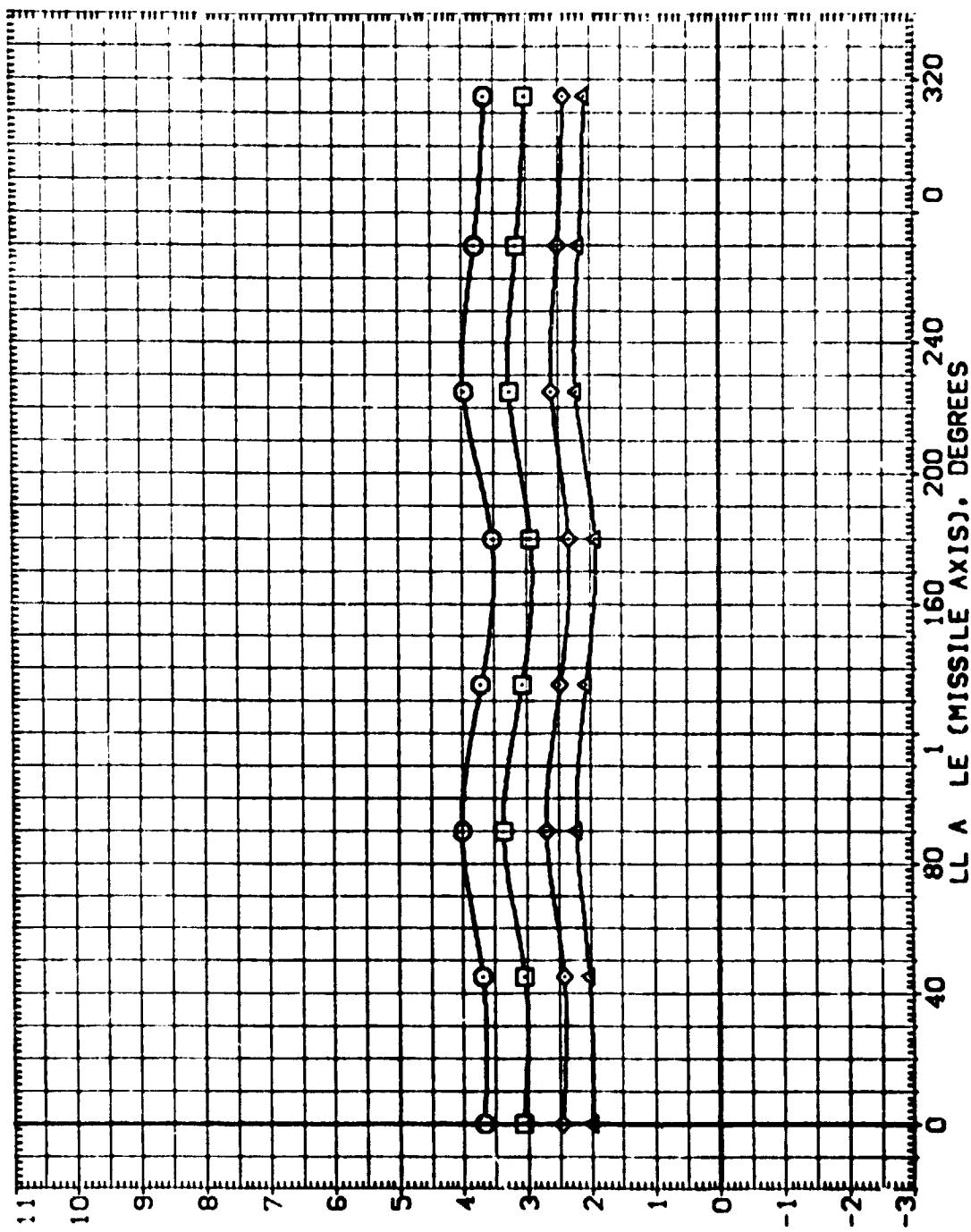


FIG. C EFFICIENTS VE A E OF L

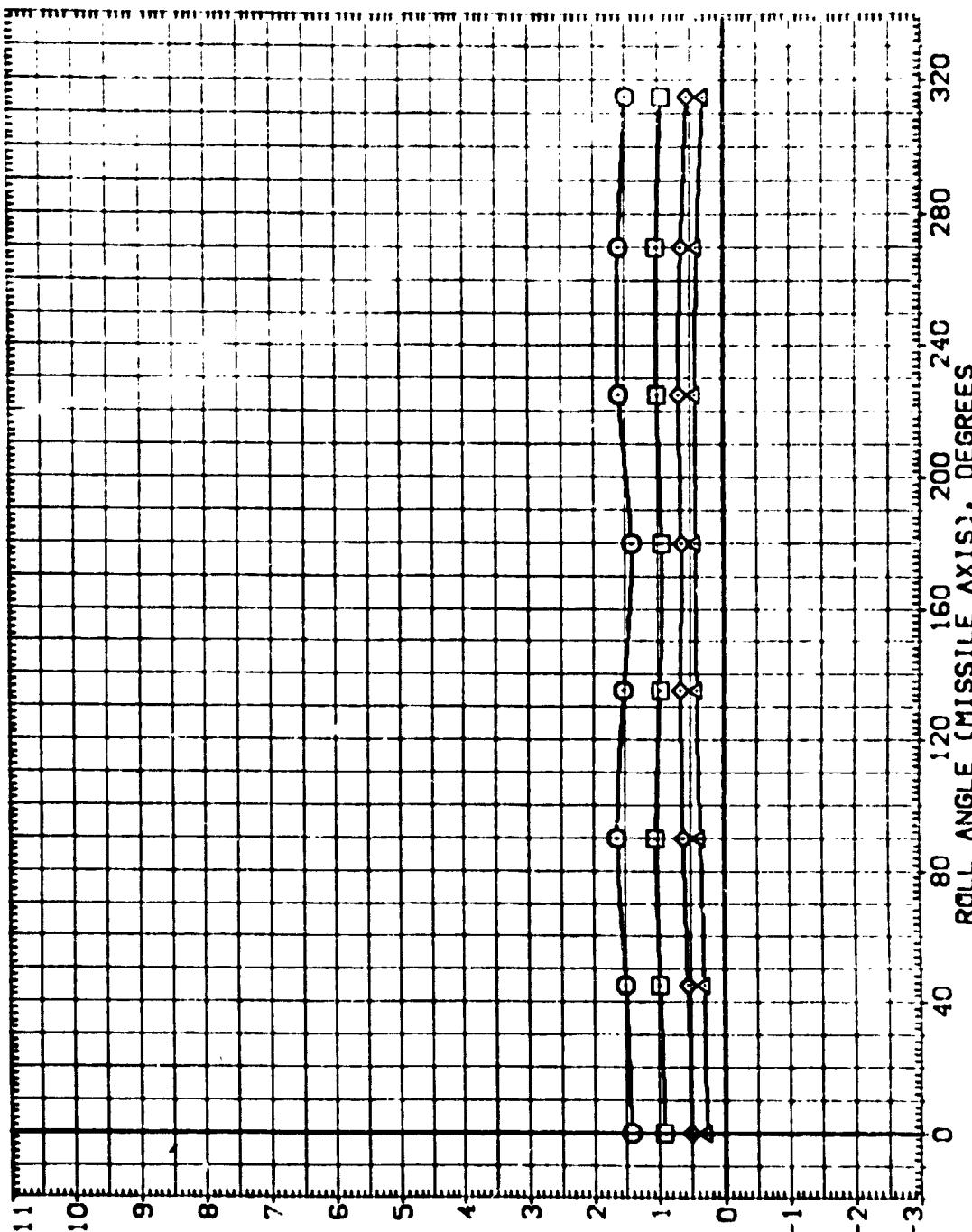
PAGE

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

P TRIM VALUES
10.400 10.160

ROLL ANGLE (DEGREES)	135.	160.	165.	170.
REFERENCE	594.1	330.	320.	140.
REF	330.	320.	320.	320.
REF	140.	140.	140.	140.
IN.				
IN. XT				
IN. YT				
IN. ZT				

SCALE

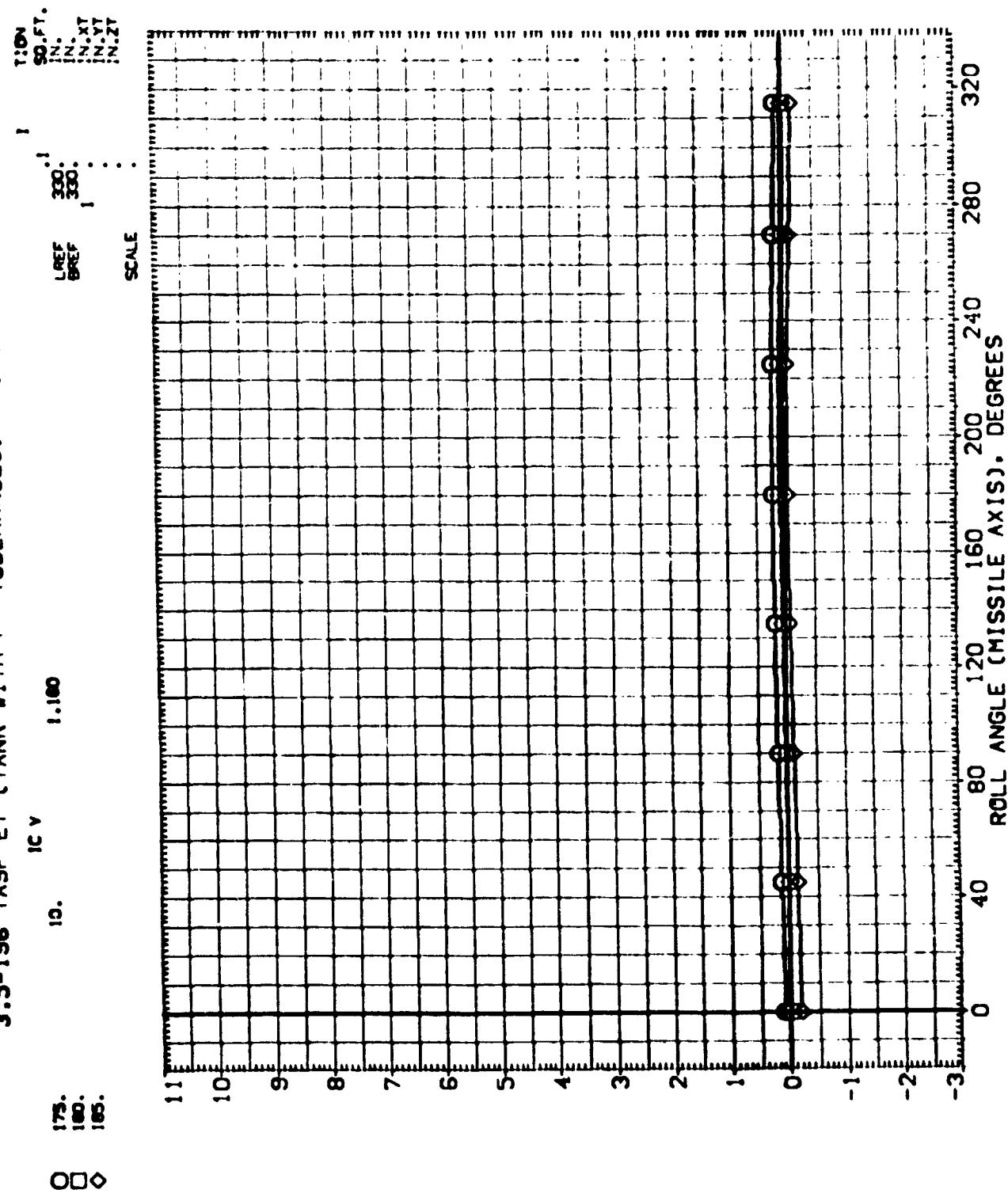


NORMAL-FORCE COEFFICIENT (MISSILE AXIS), CNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

3.5-196 TAGF ET (TANK WITH P TUBERANCES) (NEYMO1)

10. 10. 10. 10. 10.
173. 169. 165. 160. 156.
O O ◊



NORMAL-F C EFFICIENT (MISSILE AXIS). C

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

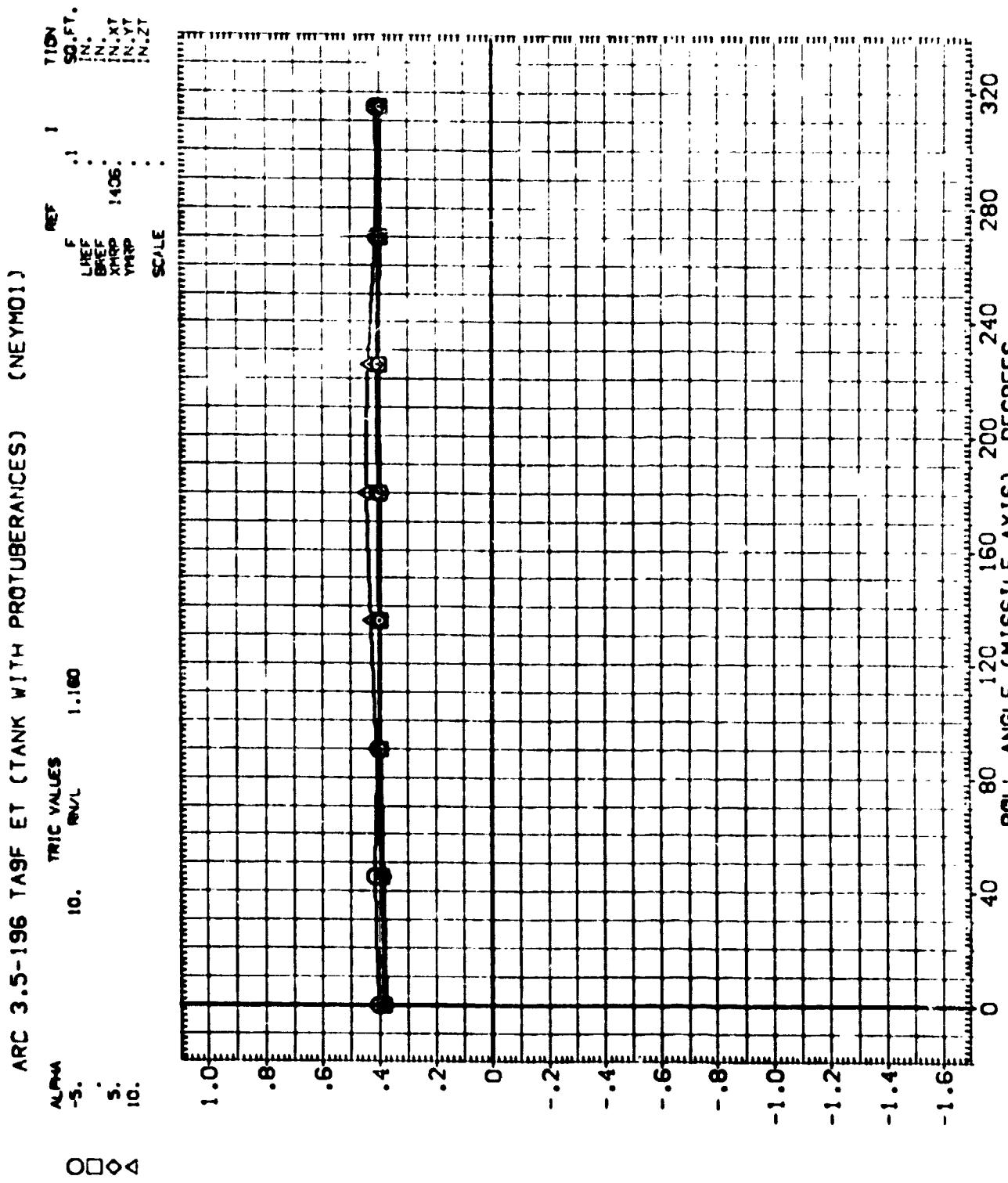


FIG. 9 COEFFICIENTS VS US ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH P TUBERANCES) (NEYMO1)

	TRIC VALUES	1.160
15.	P	10.400
20.	R _{AV/L}	1.160
25.		
30.		

○□◊◀

AXIAL FORCE COEFFICIENT (MISSILE AXIS). CA

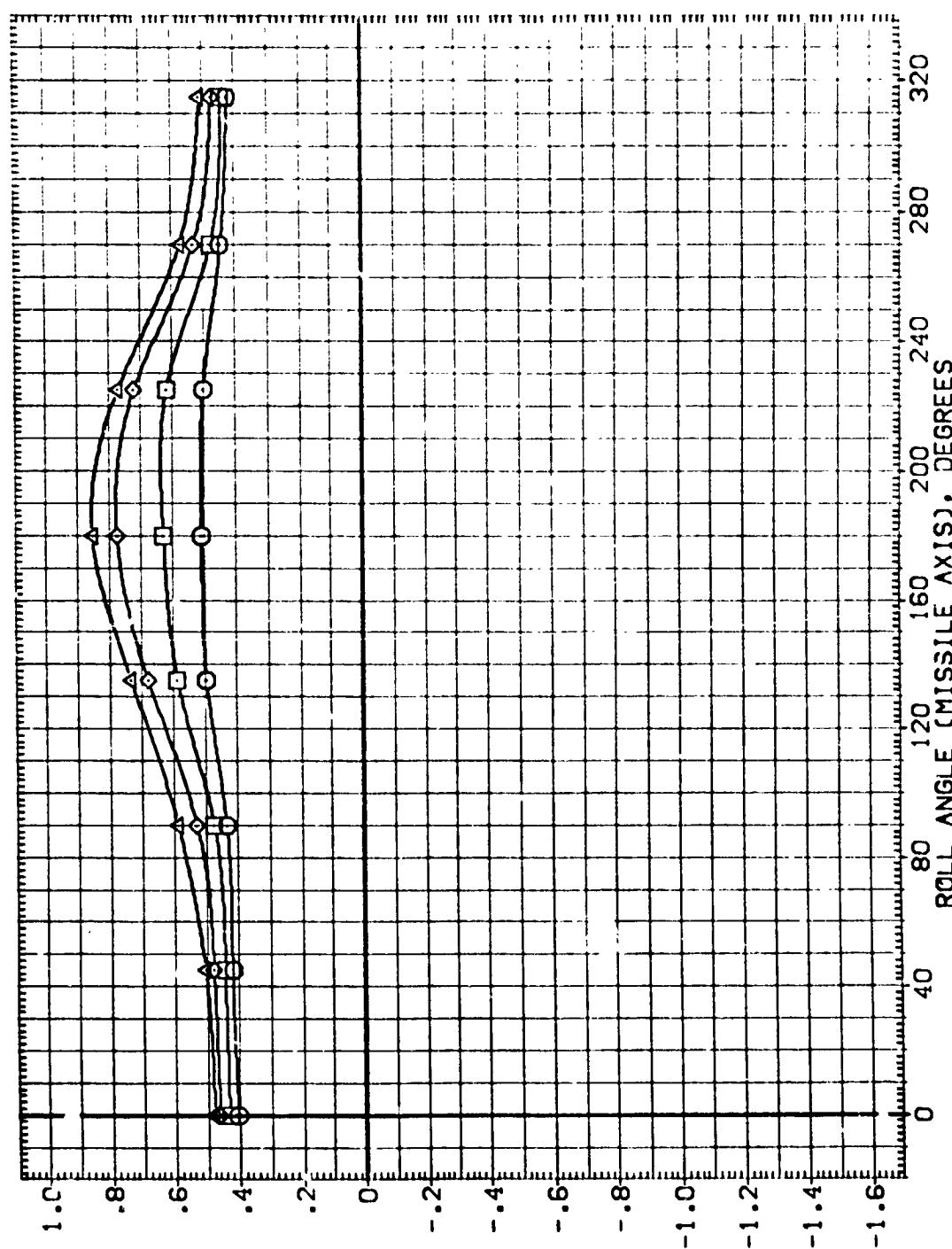


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

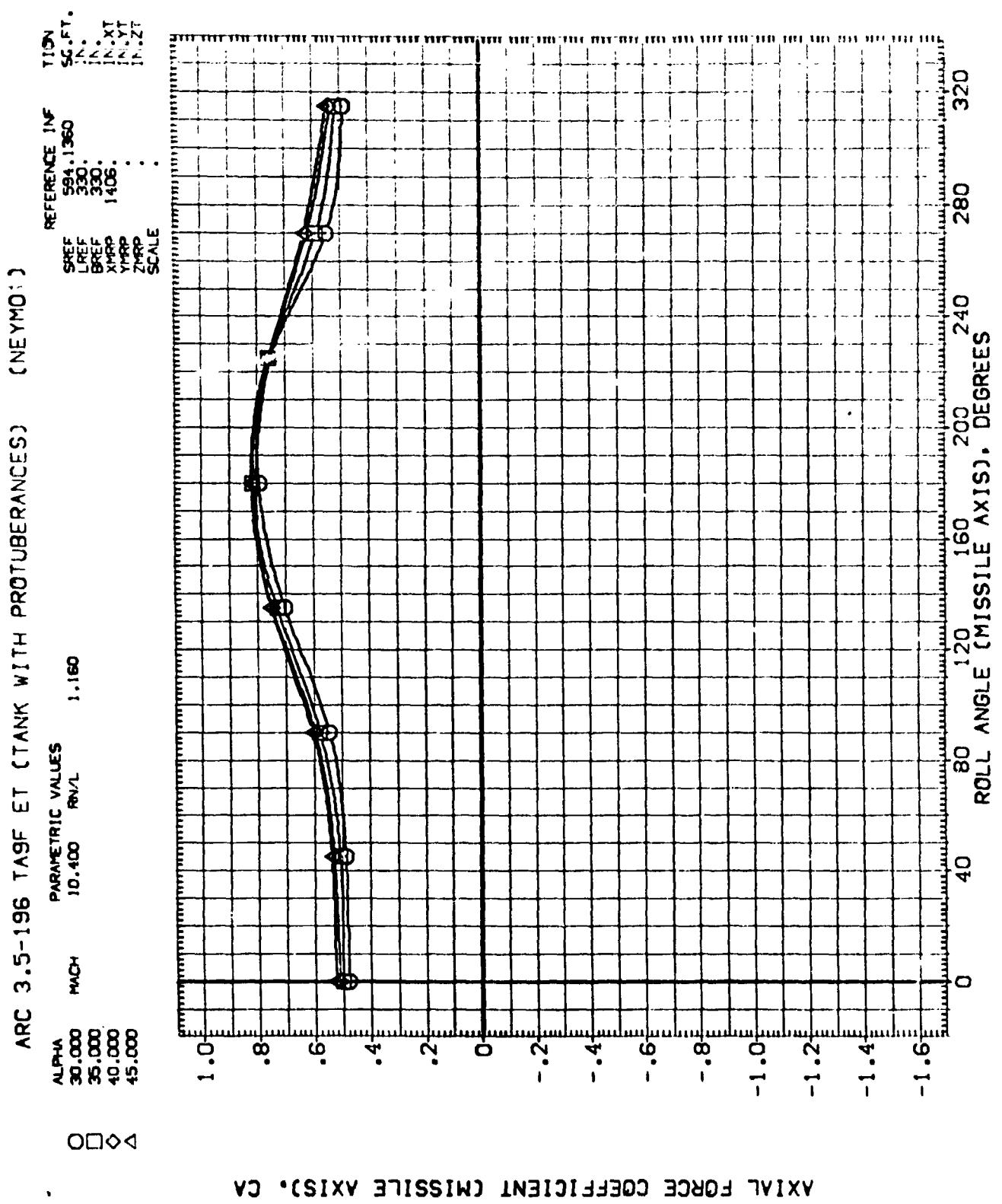
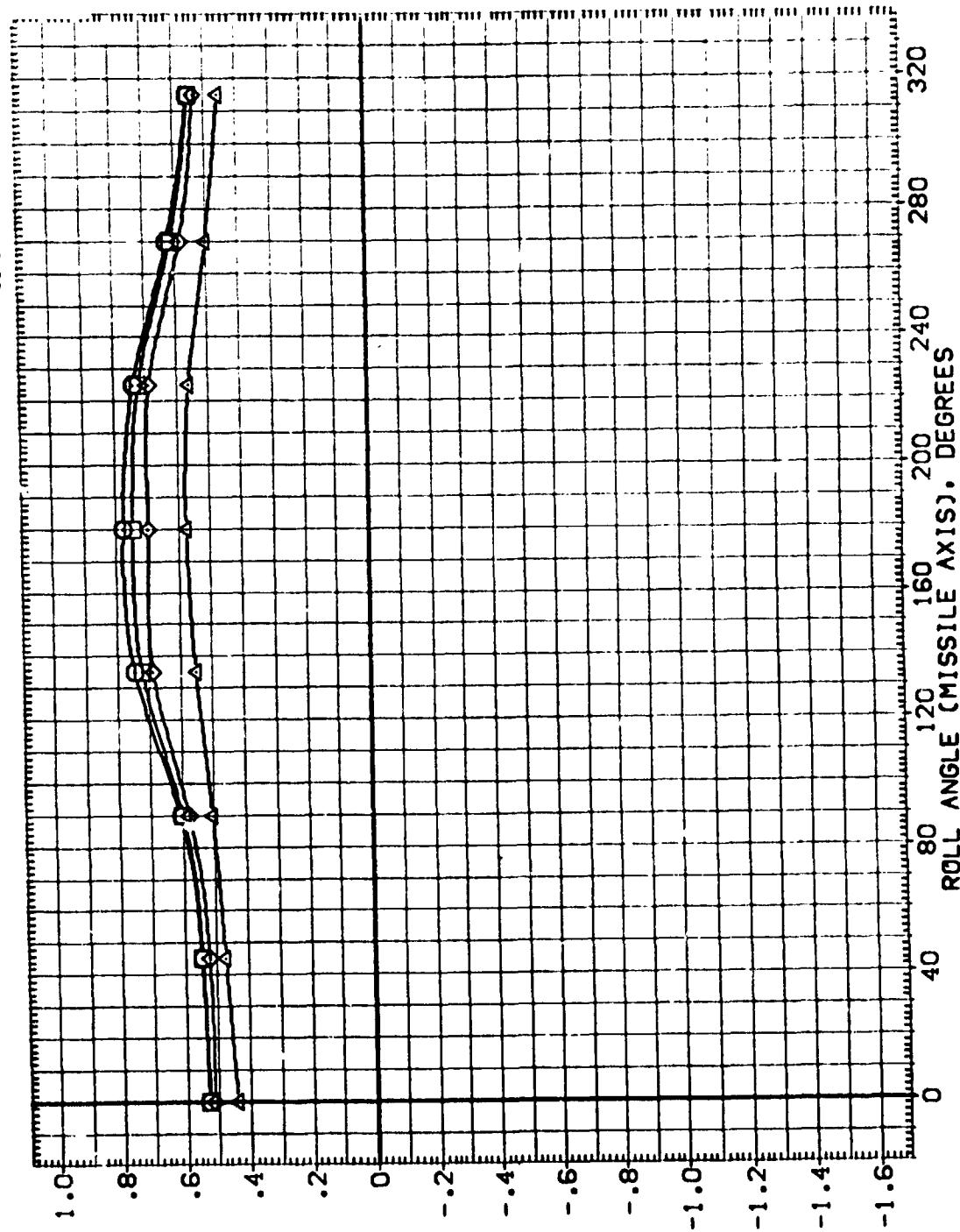


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VAL
10.400 RNL 1.160
50.
55.
60.
70.
O □ ◇ △



AXIAL FORCE COEFFICIENT (MISSILE AXIS). CA

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMOI)

ALPHA
75.
80.000
85.000
90.000

PARAMETRIC VALUES
10,400 RNL 1.160

REFERENCE IN
SREF 594.1360
LREF 330.
BREF 330.
XMPR 1406.
YMPR 2000.
ZMPR 1000.
SCALE

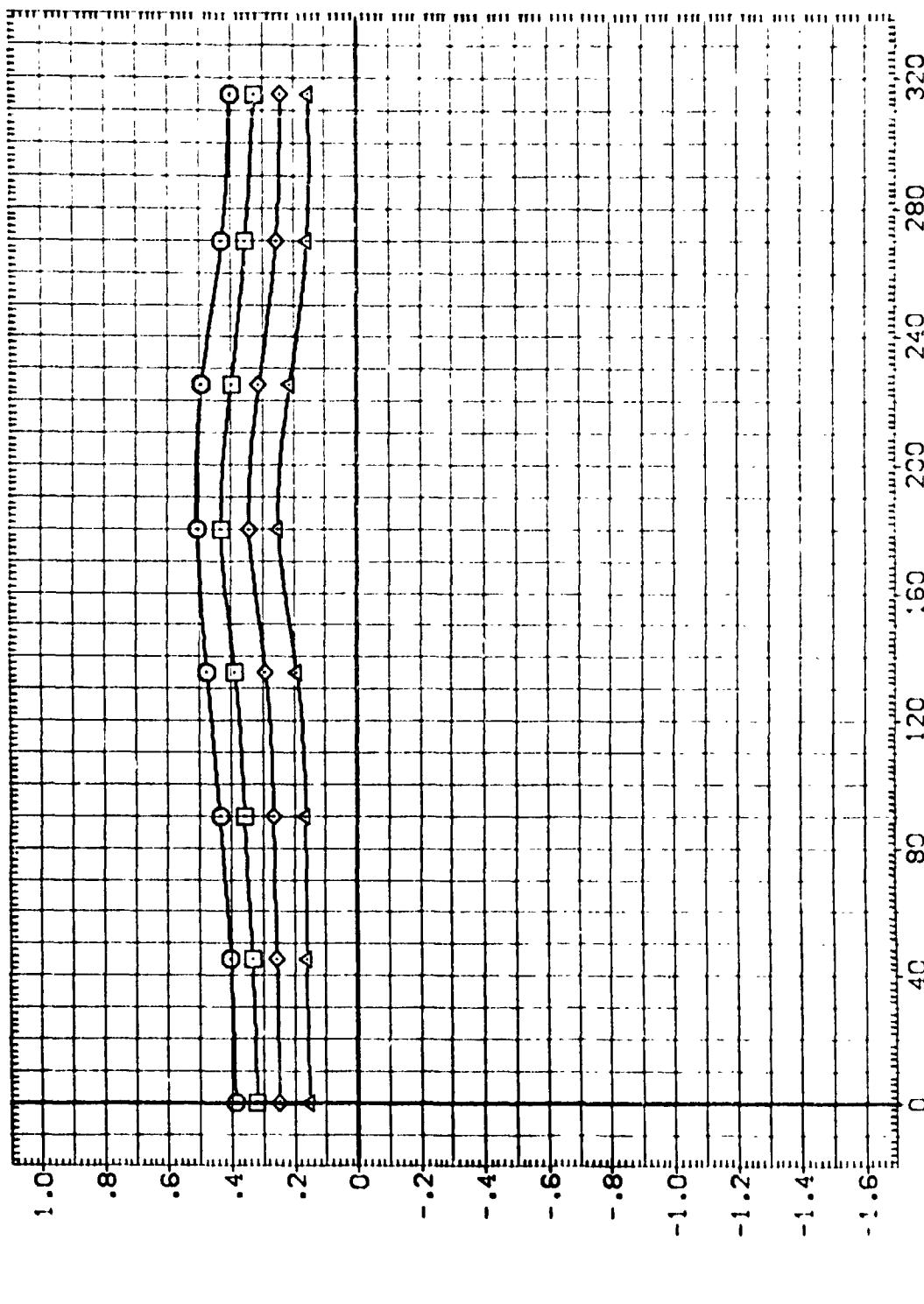


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	PARAMETRIC VALUES	RNL	1.160
.95.			
100.000			
125.000			
150.000			

REF. 594.1 SEC
LREF 330.
BREF 330.
XTRP 1406.
YTRP 2000.
ZTRP 110.000
SCALE .1

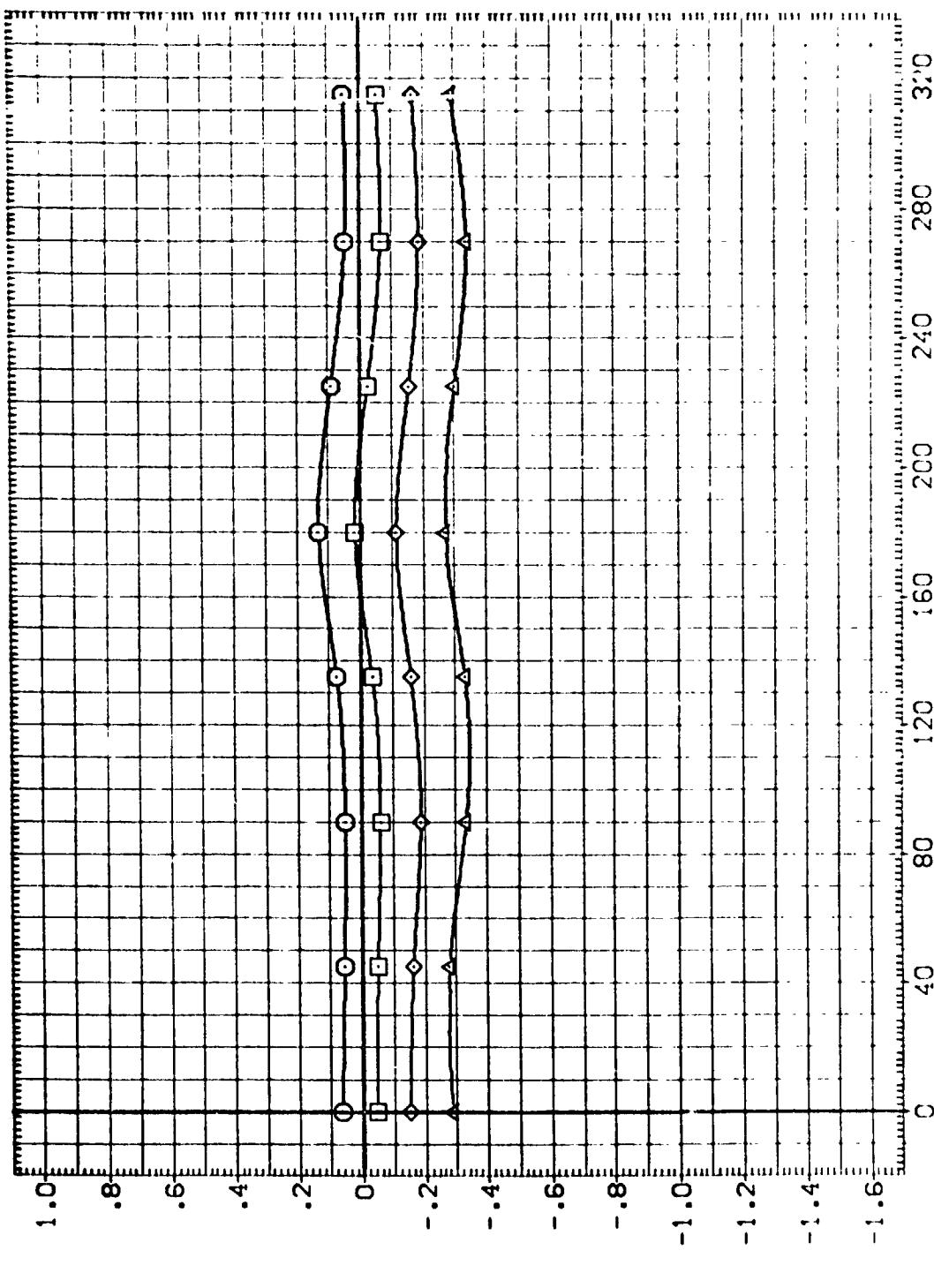


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) [NEYMO1]

ALPHA	MACH	PARAMETRIC VALUES
115.000	10.400	RNL 1.160
120.000		
125.000		
130.000		

REFERENCE INF 52.FT.
 SREF 594.1360
 LREF 330.2000
 BREF 330.2000
 XHPP 1406.
 YHPP ...
 ZHPP ...
 SCALE ...

○□◊△

AXIAL FORCE COEFFICIENT (MISSILE AXIS). CA

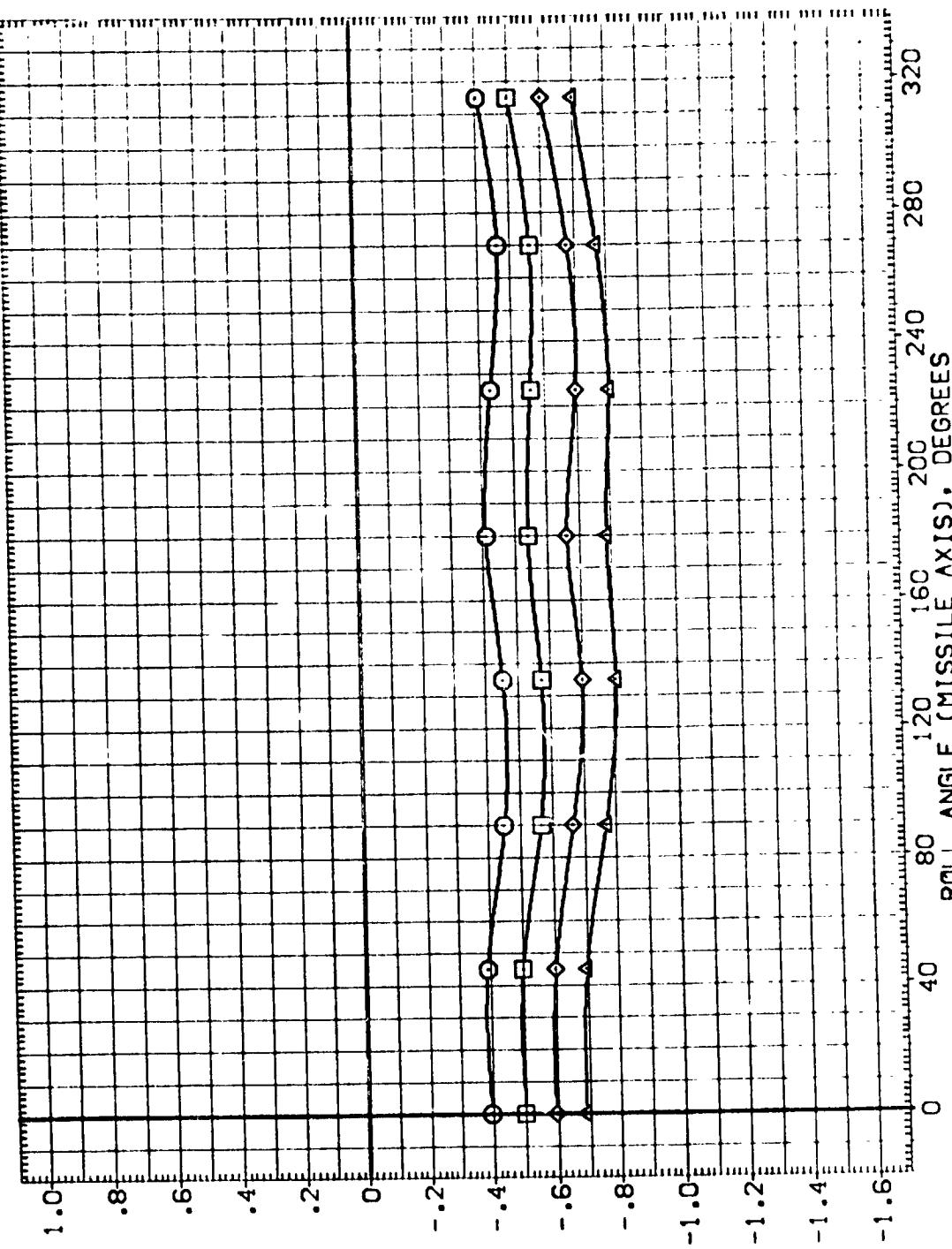


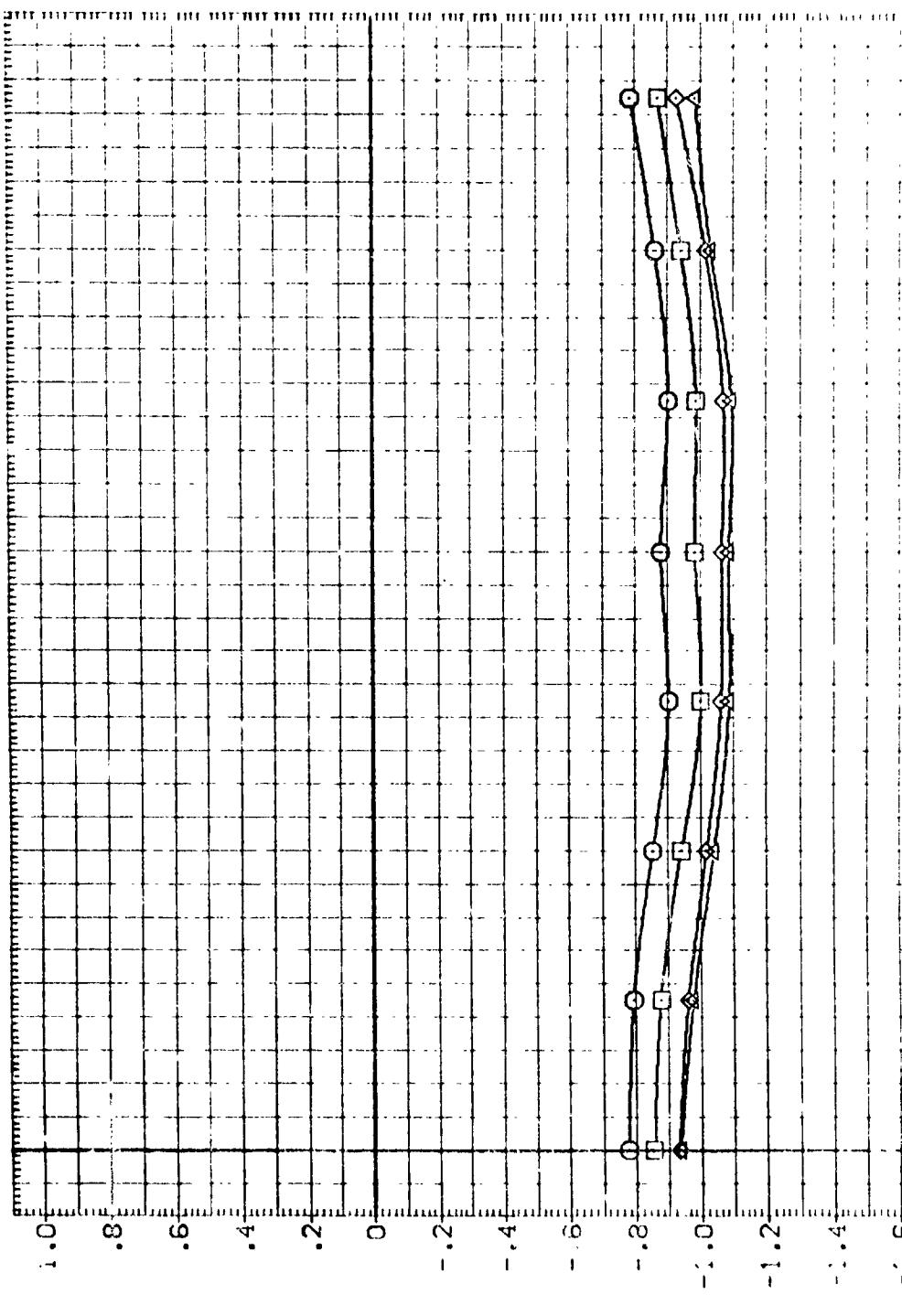
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

PAGE 7.

ARC 3.5-196 TAGE ET (TANK WITH PROTUBERANCES) (CNEYMO1)

PARAMETRIC VALUES
 ALPHA MACH 0.400 ROLL 1.160
 135.000 140.000 145.000 150.000

REFERENCE IN
 SO.FT.
 SREF 594.1360
 LREF 330.2000
 BREF 330.2000
 XMRP 1406.0000
 YMRP 10000
 ZMRP .0000
 SCALE .0000



AXIAL FORCE COEFFICIENT (MISSILE AXIS), CA

ANGLE 20 85 160 200 240 280 320
 0 45 90 135 180 225 270 315
 0 45 90 135 180 225 270 315

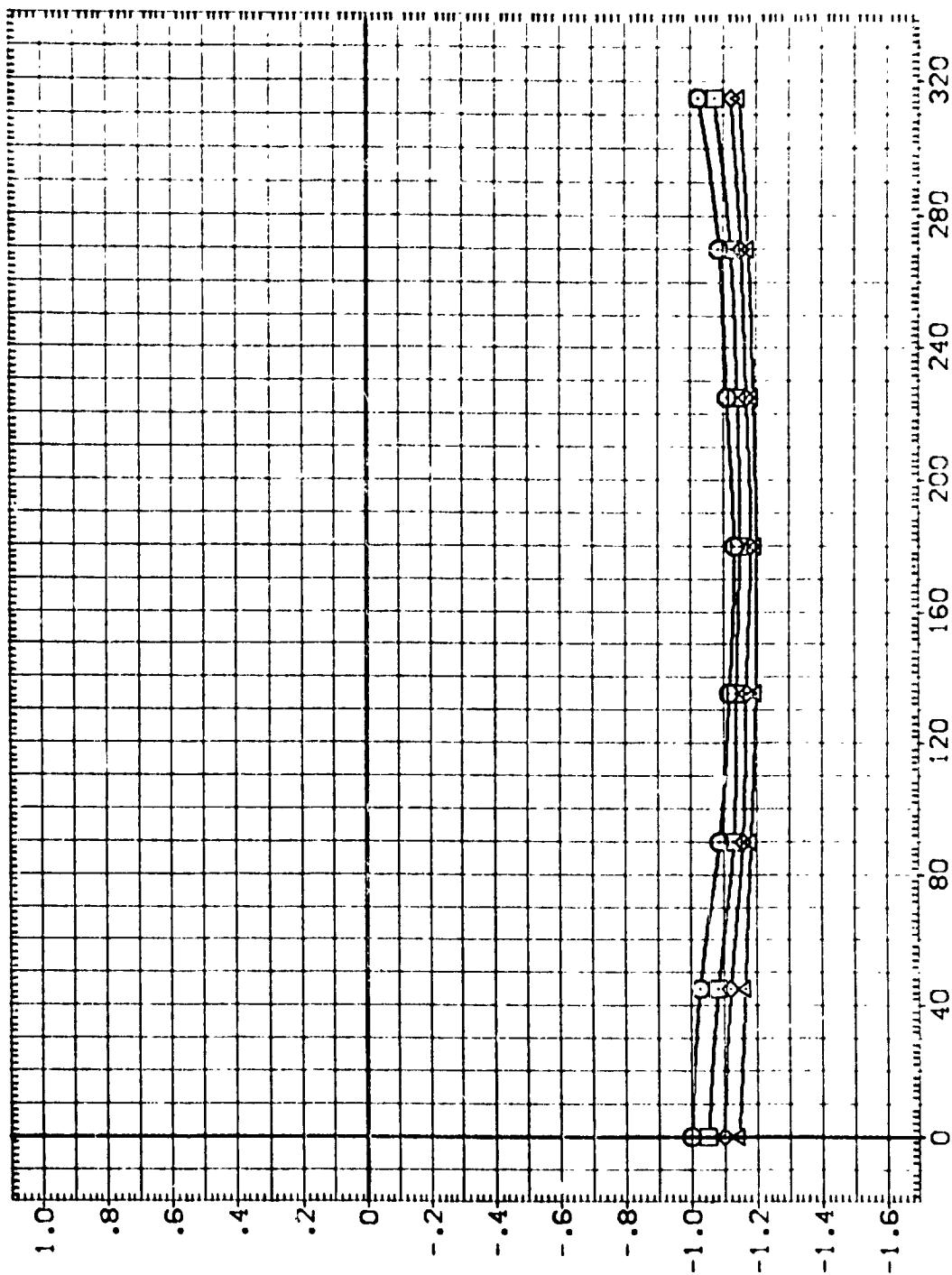
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

DAGF

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) [NEYMO1]

PARAMETRIC VALUES
 ALPHA 135.
 160.000 10.400 RNL 1.160
 165.000
 170.000

○ □ ◇ △



AXIAL FORCE COEFFICIENT (MISSILE AXIS), CA

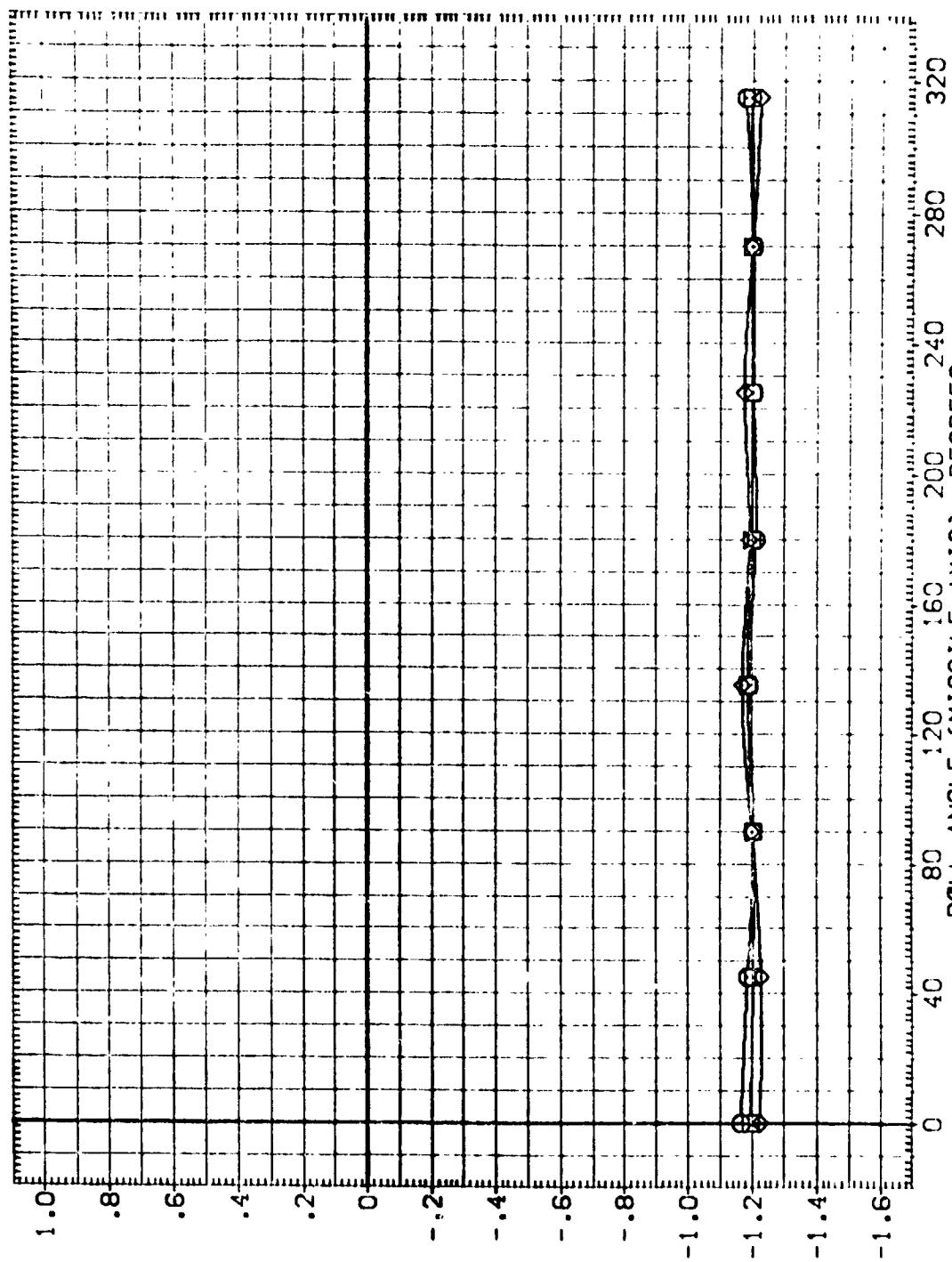
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO!)

PARAMETRIC VALUES

ALPHA	MACH	ROLL	1.160
175.000	10.400	10.400	
180.000			
185.000			

REFERENCE INFORMATION
SREF 594.1360
LREF 330.
BREF 330.
XMRP 1406.
YMRP
ZMRP
SCALE



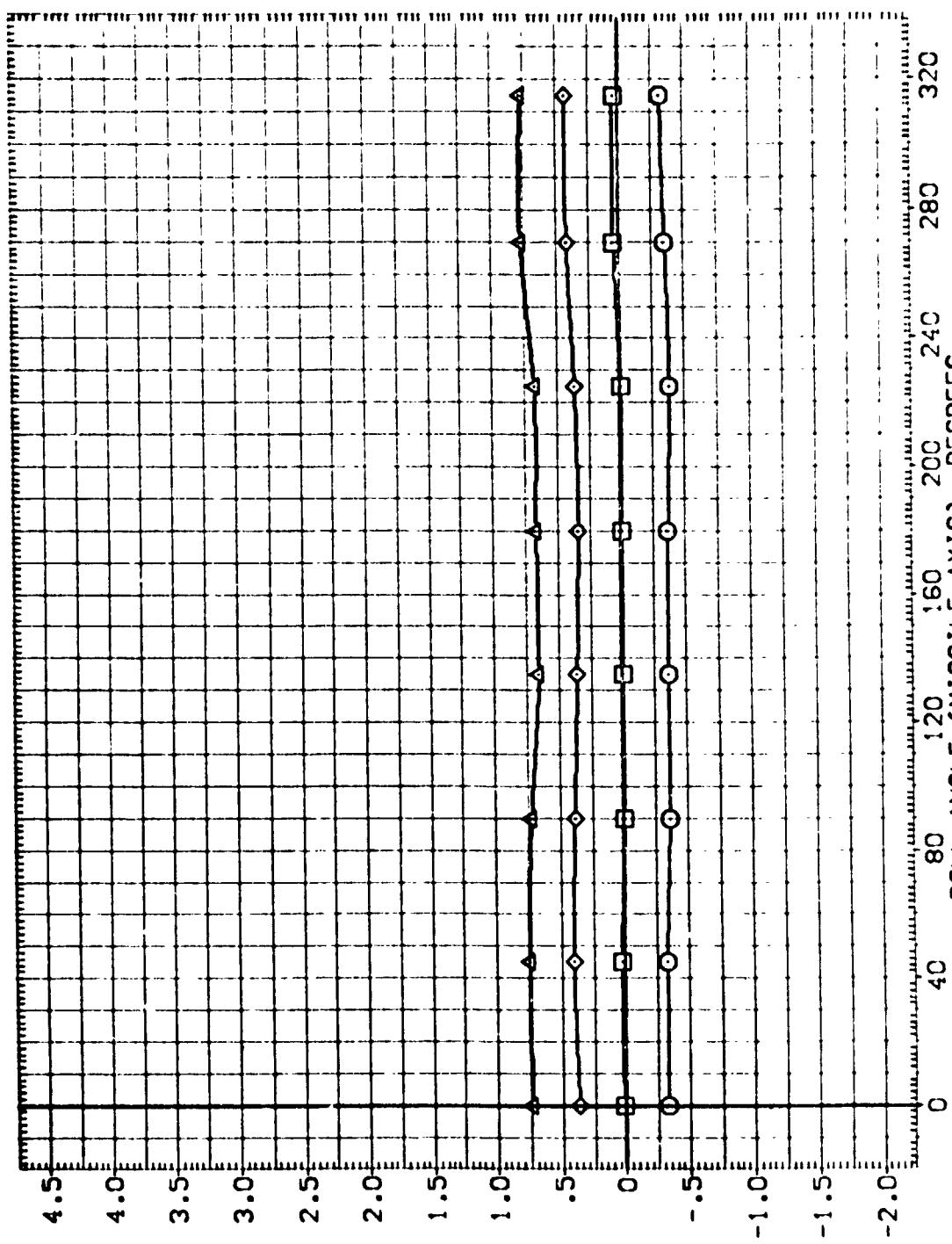
AXIAL FORCE COEFFICIENT (MISSILE AXIS), CA

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	POLARIC VALUES	ROLL ANG.
-5.		10.400	1.160
5.			
10.000			

□ ◇ ▲



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TARGF E1 CRANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
ALPHA 10.450 ROLL 1.180
15.000 40.000 25.000 30.000

REFERENCE INFORMATION
SREF 594.1360
LREF 330.
BREF 330.
XHPP 146.
YHPP 146.
ZHPP 146.
SCALE 1.0

O 10 △

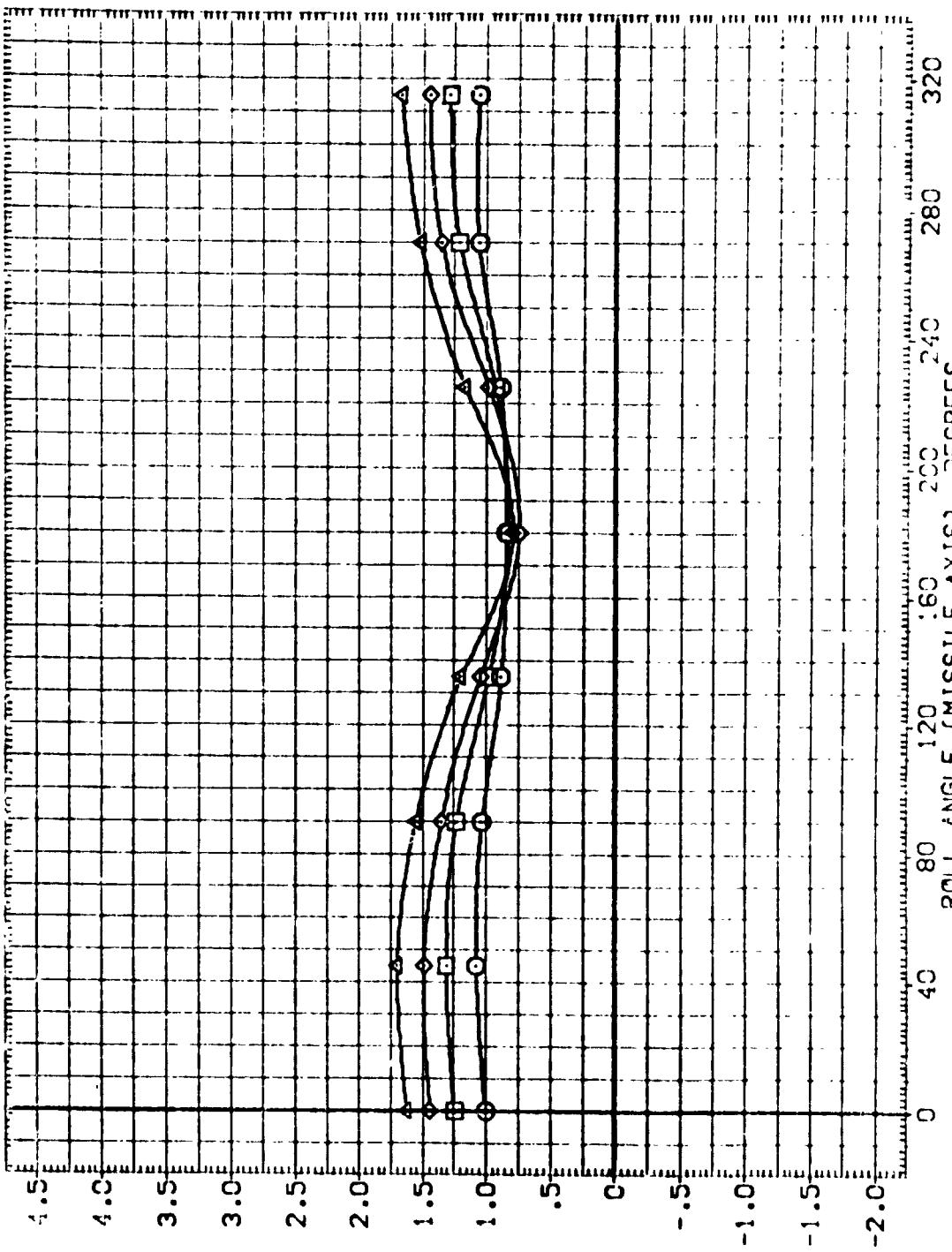


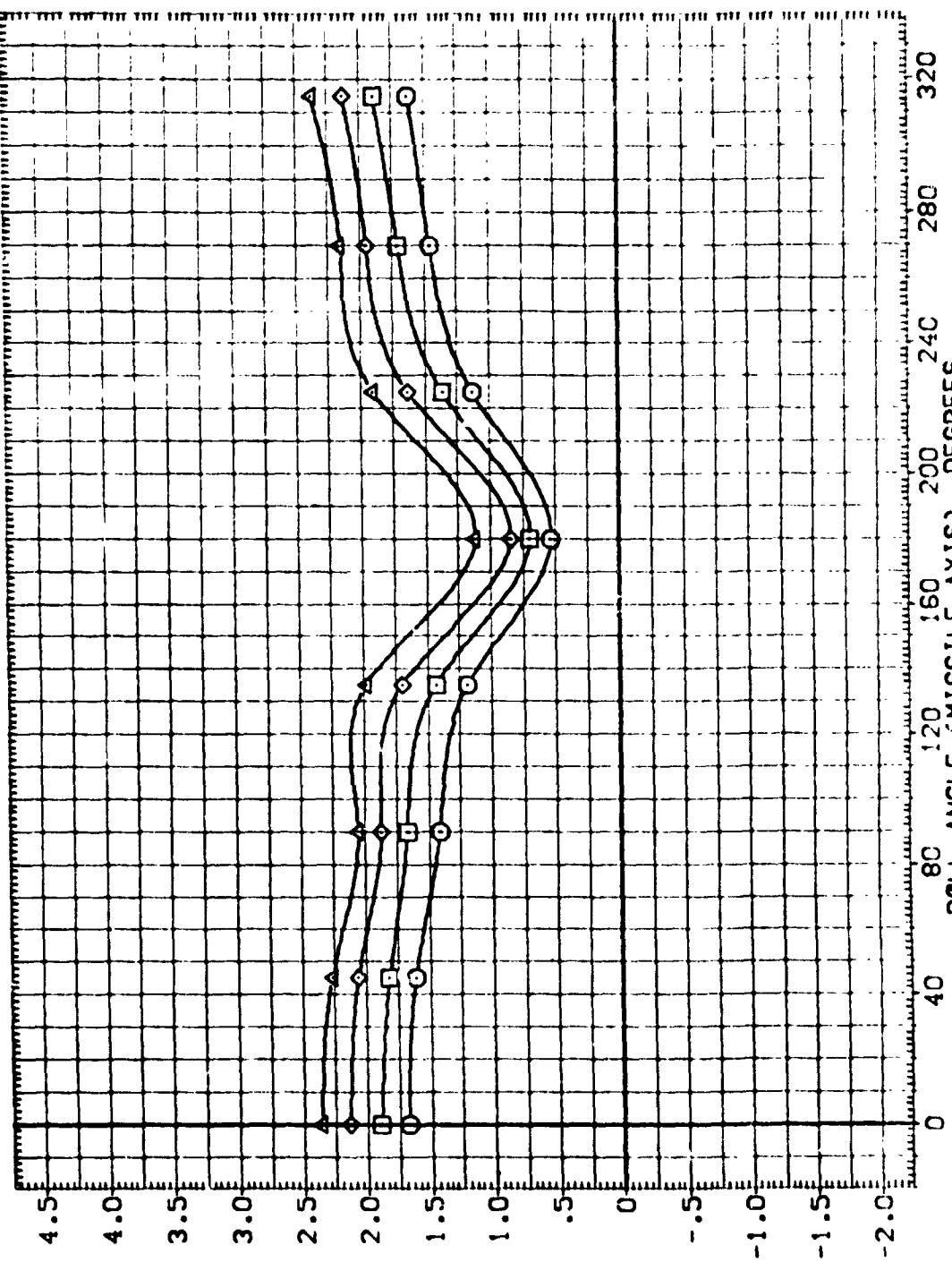
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

DATE 76

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMOI)

PARAMETRIC VALUES
 ALPHA_{20.} 10.400 R/H 1.160
 ALPHA_{30.}
 ALPHA_{40.}
 ALPHA_{45.}

REFERENCE INFORMATION
 LREF 594.1360 SQ.FT.
 SREF 330. IN.
 XREF 145. IN.X
 YREF IN.Y
 ZREF IN.Z



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMOI)

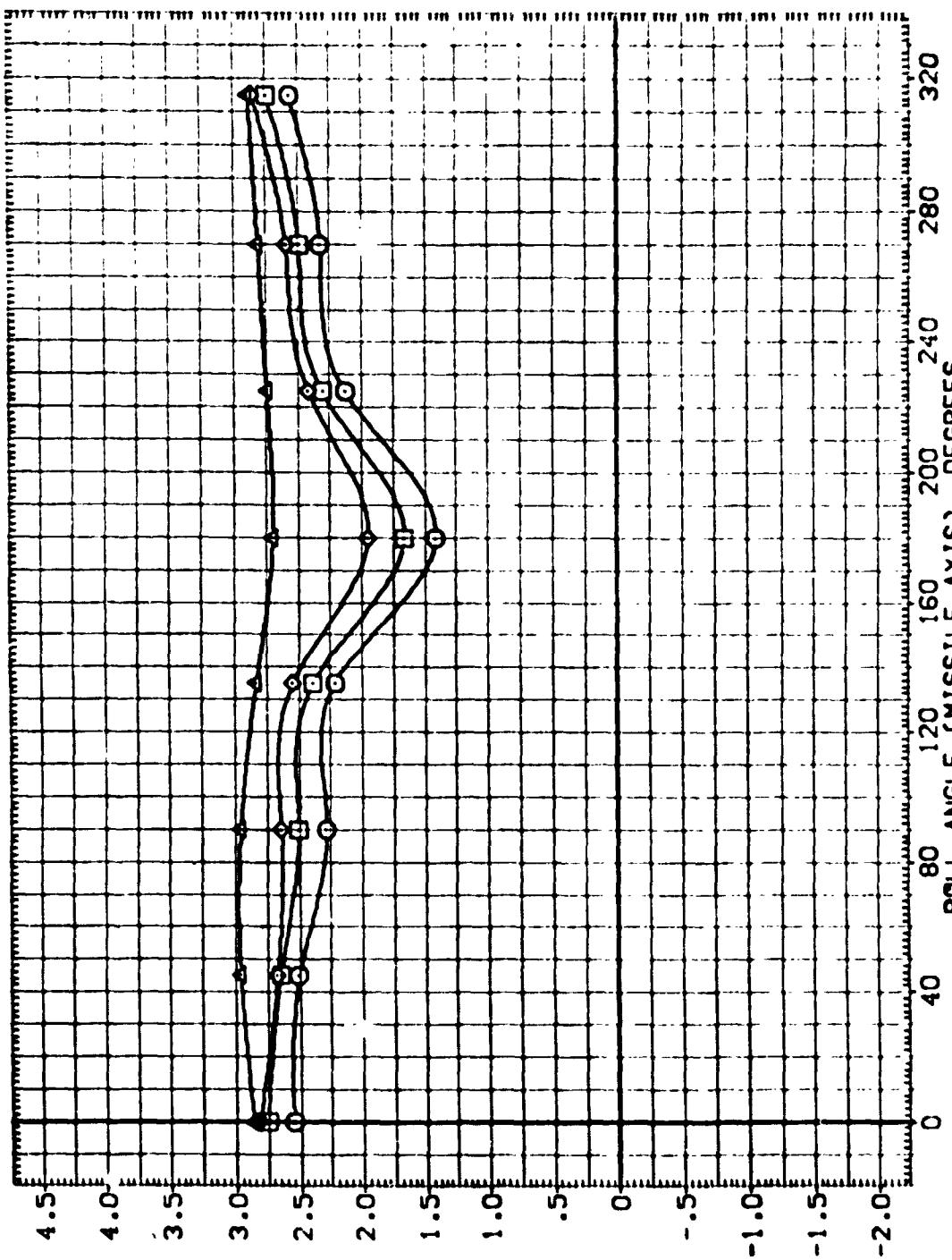
P. TRIC V

1.180

80.
85.
90.
95.
10.

0□♦◀

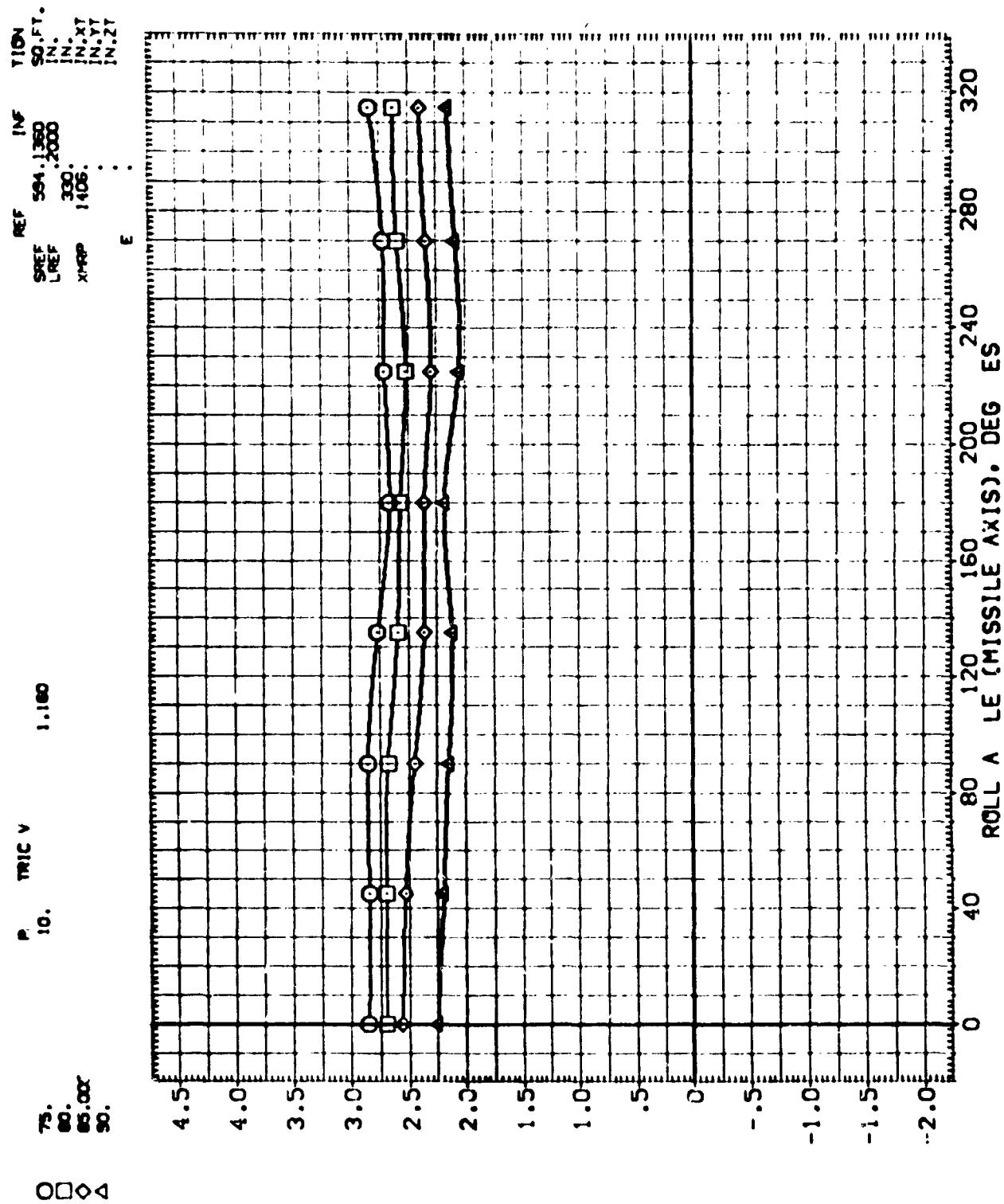
INF. ATION
SQ.FT.
N.
N.XT
N.YT
N.ZT
LREF
BREF
XHPP



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLHM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CL

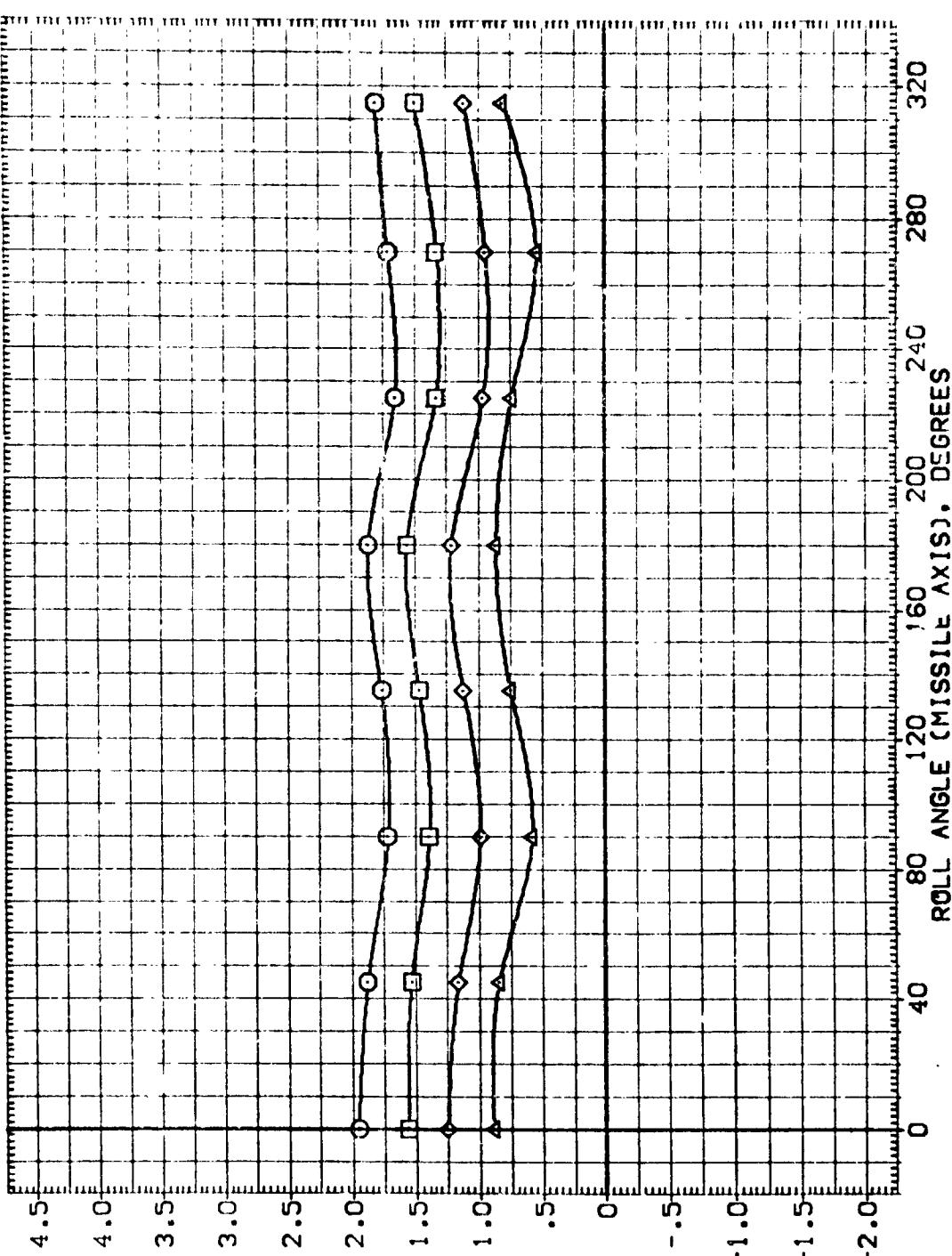
FIG. 9 COEFFICIENTS VERSUS ANGLE OF LL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA MACH $P_{10,400}$ RNU 1.160

95.			
100.000			
105.000			
110.000			

REF. 954.1
REF. 330.
REF. 330.
REF. 1406.
XMP
YMP
ZMP
SCALE



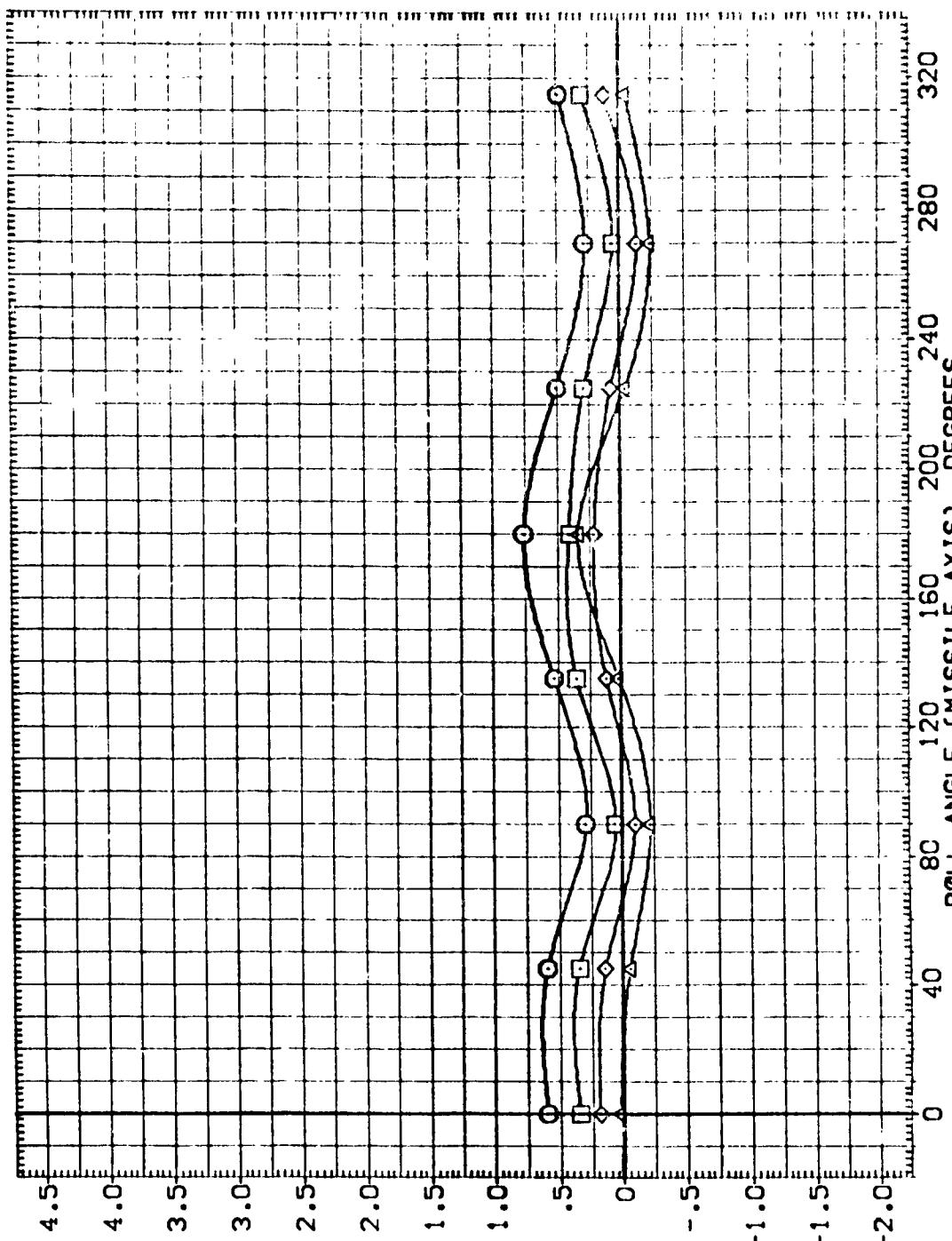
PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

P_{TRIC} VALUES
MACH 10.400 ROLL 1.160
ALPHA 115.000 120.000 125.000 130.000

REFERENCE INF.
SREF 594.1360
REF 330.
BREF 330.
XREF 1406.
YREF 1406.
ZREF 1406.
SCALE



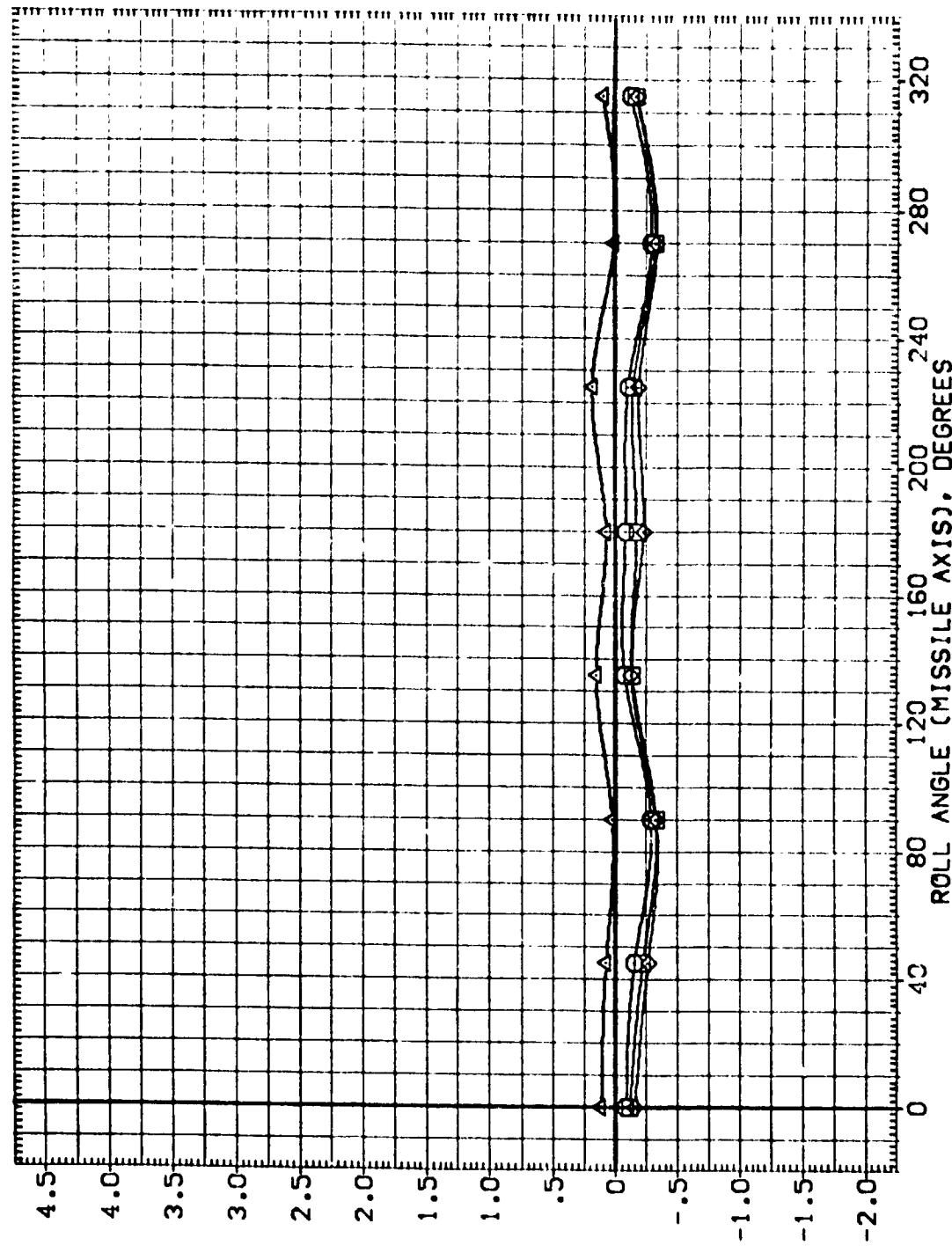
PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES	1.160
10.400 RFL	
135.	
140.000	
145.	
150.000	

REF. 594.1
LREF. 330.
BREF. 330.
XMRP. 145.
YMRP. 280.
ZMRP. 320.
SCALE .



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
10.400 MACH 1.160

ALPHA	MACH
155.000	160.000
165.000	170.000

○ ◇ △

REFERENCE INF.
SQ.FT.
SREF 594.1360
LREF 330.
BREF 330.
XMRP 146.
YMRP 746.
ZMRP 200.
SCALE .



PITCHING MOMENT COEFFICIENT (MISSILE AXIS). CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

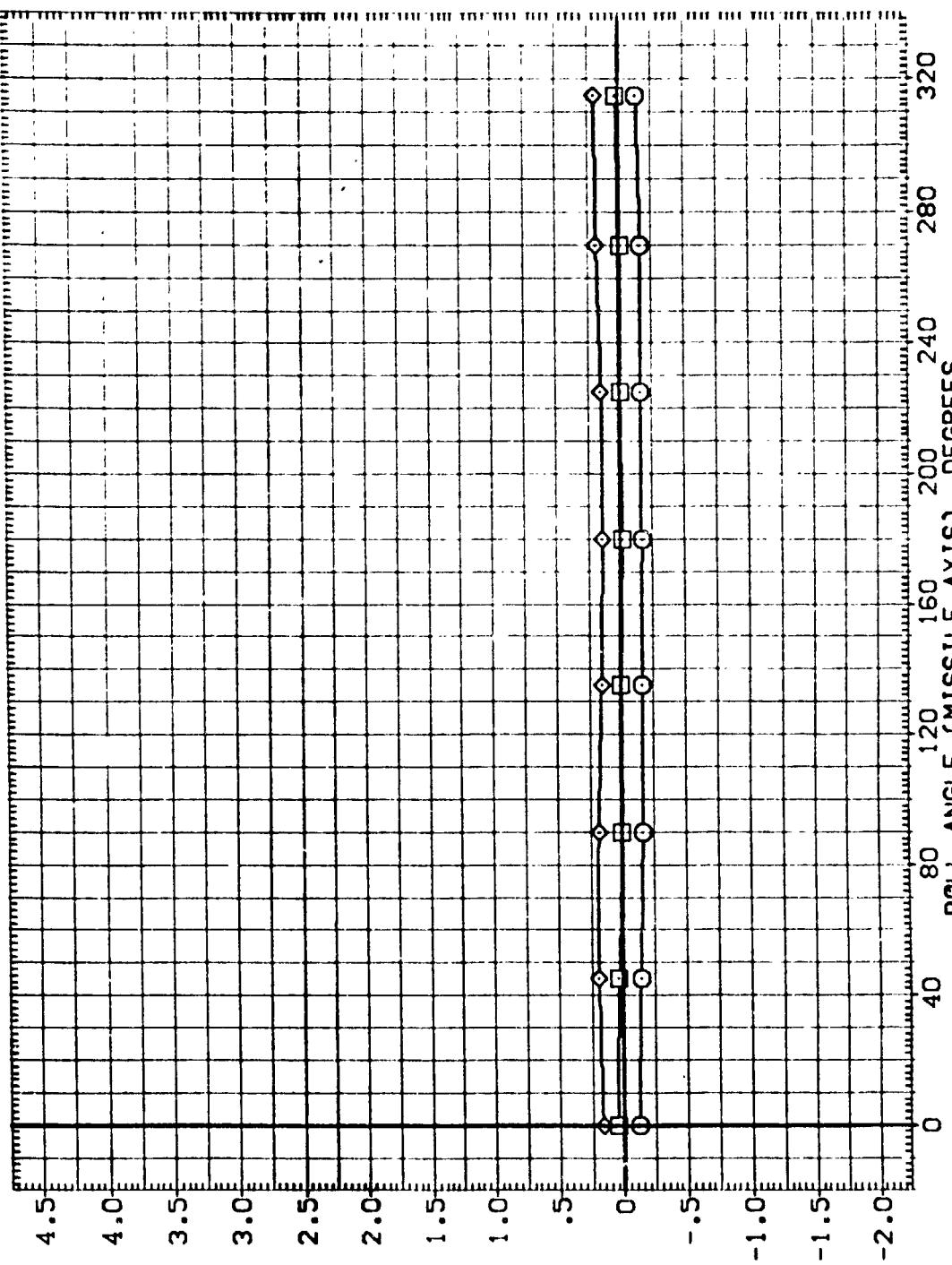
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA
175.000
180.000
185.000

P TRIC VALUES
10.400 181. 1.160

○□◊

REFERENCE INFORMATION
SREF 594.1360
LREF 330.
BREF 330.
XMRP 1406.
YMRP .0000
ZMRP .0000
SCALE .0060



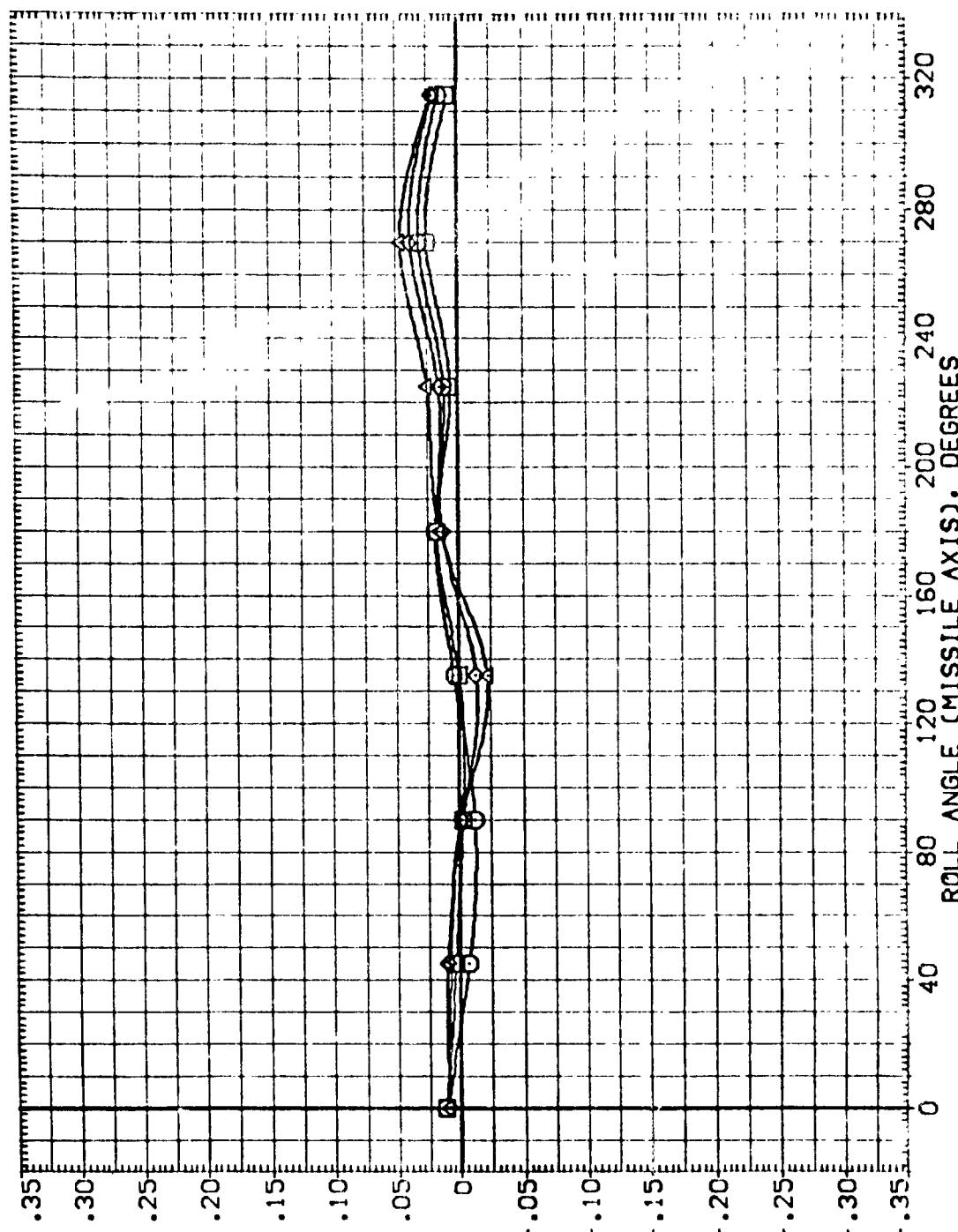
PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLMM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
 10.400 ANGL 1.160
 ALPHA MACH
 -.000 .000 5.000 10.000

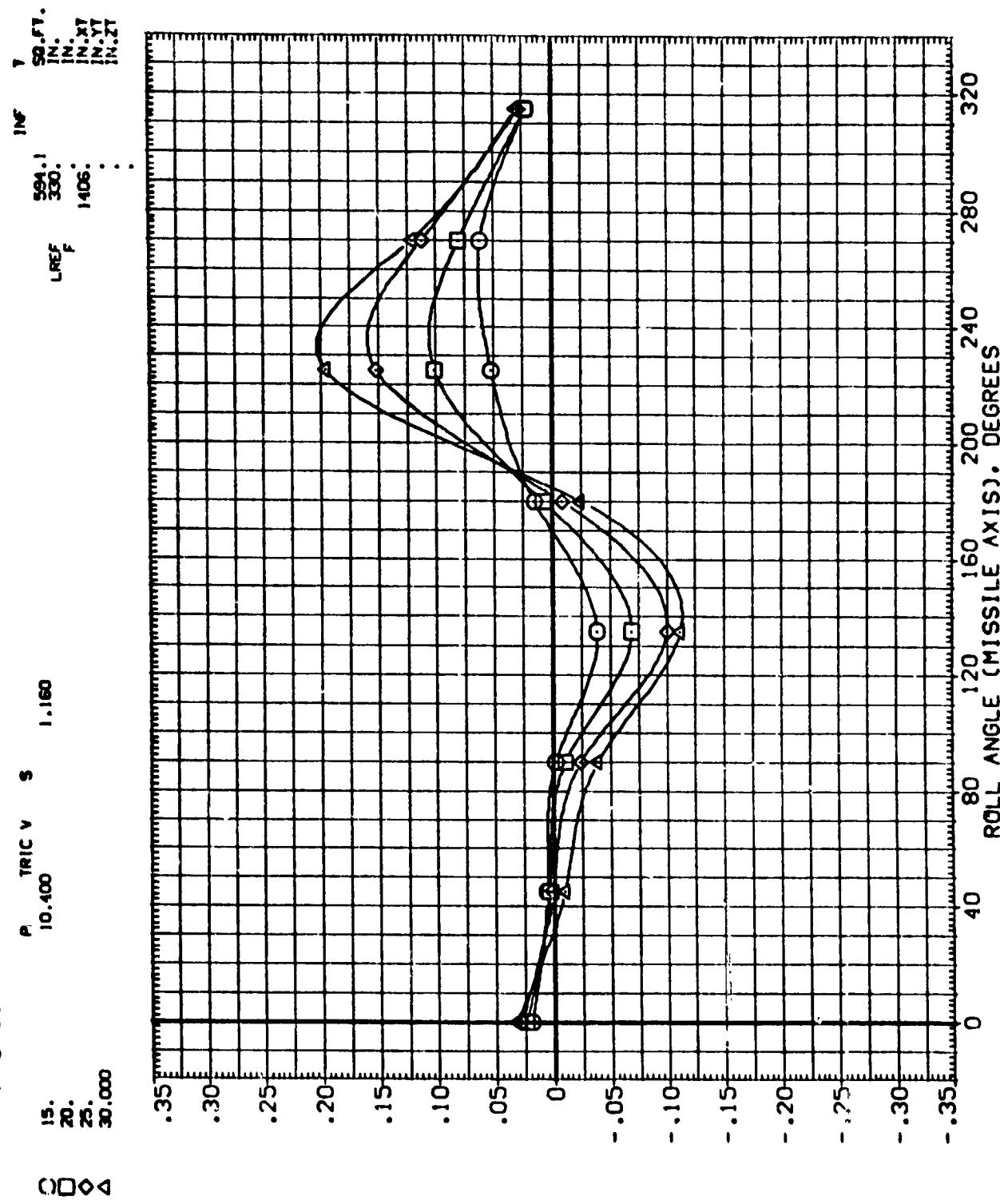
REFERENCE INFORMATION
 STUFF 594.1360 IN.
 LREF 330. IN.
 BREF 1406. IN.XT
 XMRP 1406. IN.YT
 ZMRP 1406. IN.ZT
 SCALE



SIDE-FORCE COEFFICIENT (MISSILE AXIS). CM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)



SIDE-FORCE COEFFICIENT (MISSILE AXIS). CM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

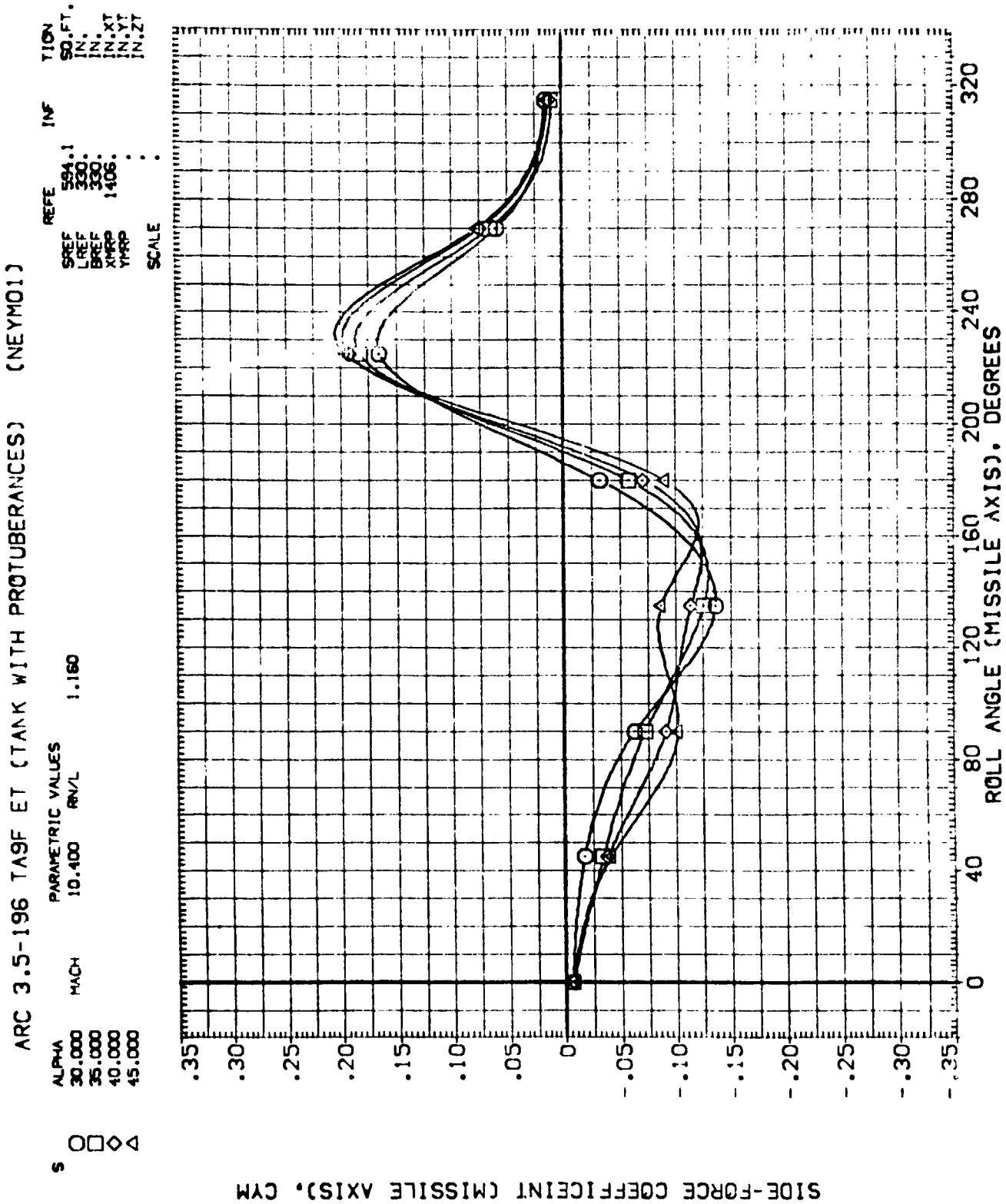


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

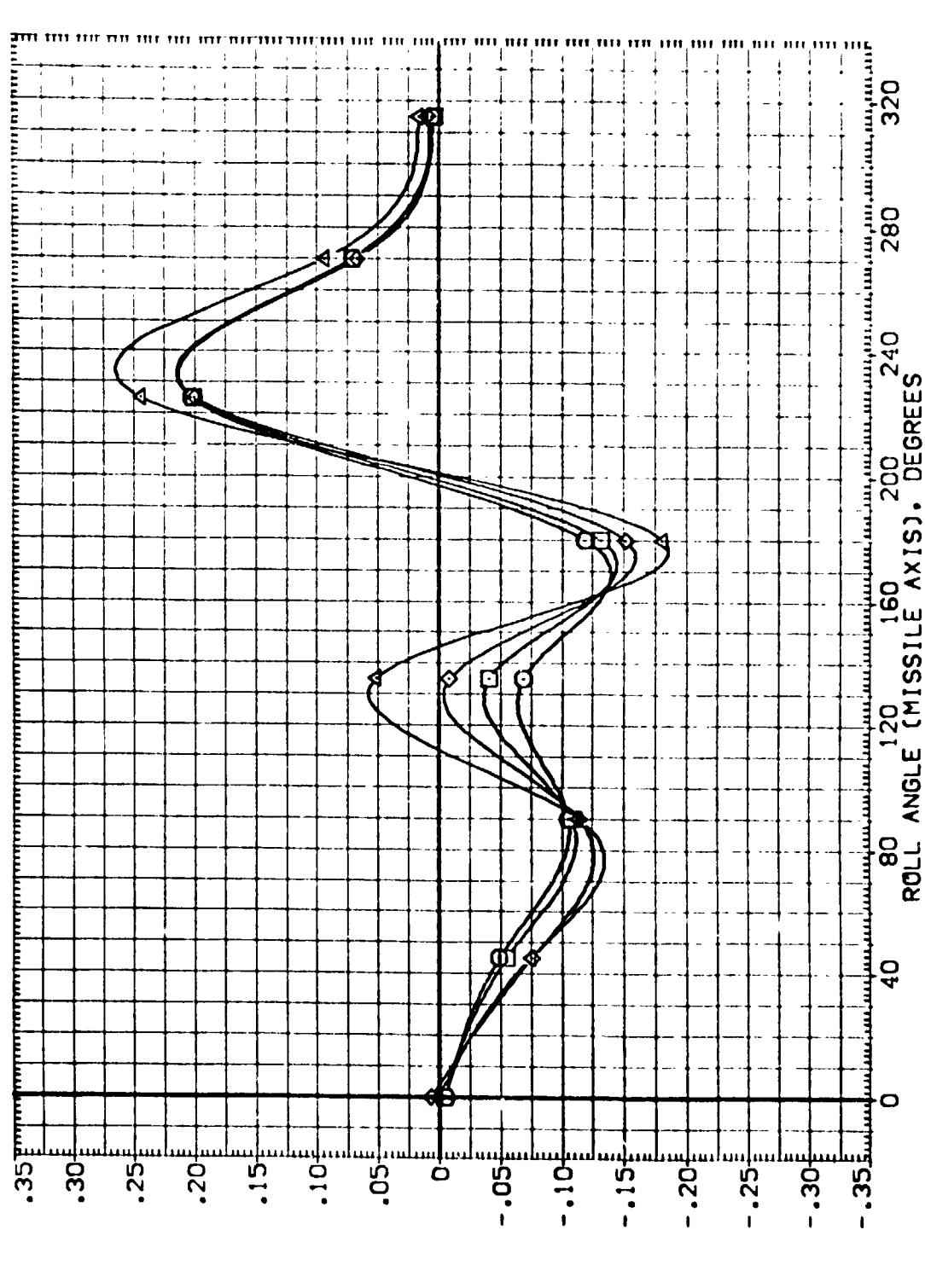
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES

10.400 RVAL 1.160

ALPHA
50.000
55.000
60.000
70.000

○ □ ◇ ▲



SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

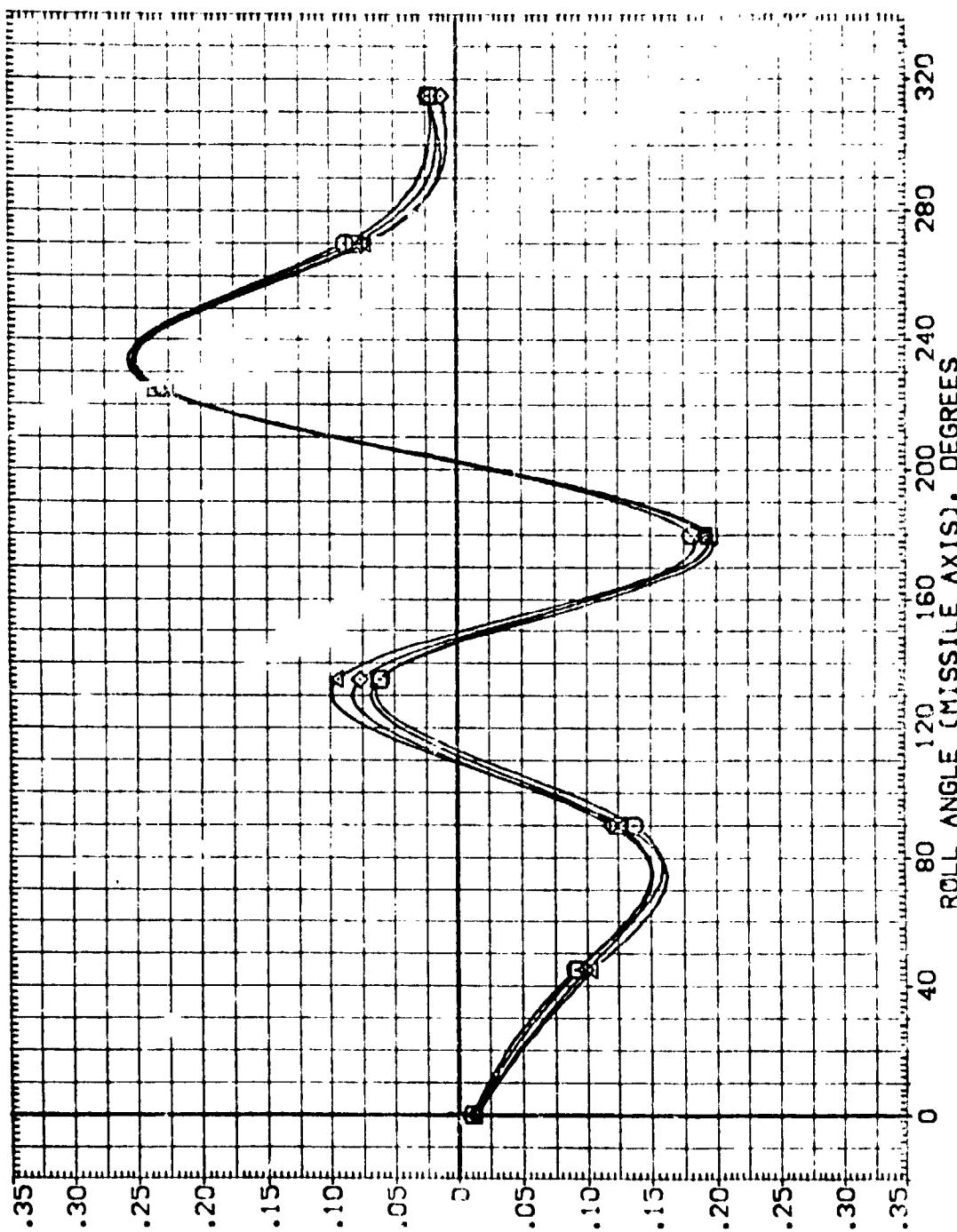
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	PARAMETRIC VALUES	R _{AVL}	C _Y _{AVL}
75.	80.000	10.400	1.160	
85.000				
90.000				

○ □ △

REFERENCE SURFACE
SREF 594.1
XREF 30.
YREF 30.
XHP 1406.
YHP 1406.
ZHP 1406.
SCALE



SIDE-FORCE COEFFICIENT (MISSILE AXIS). CM

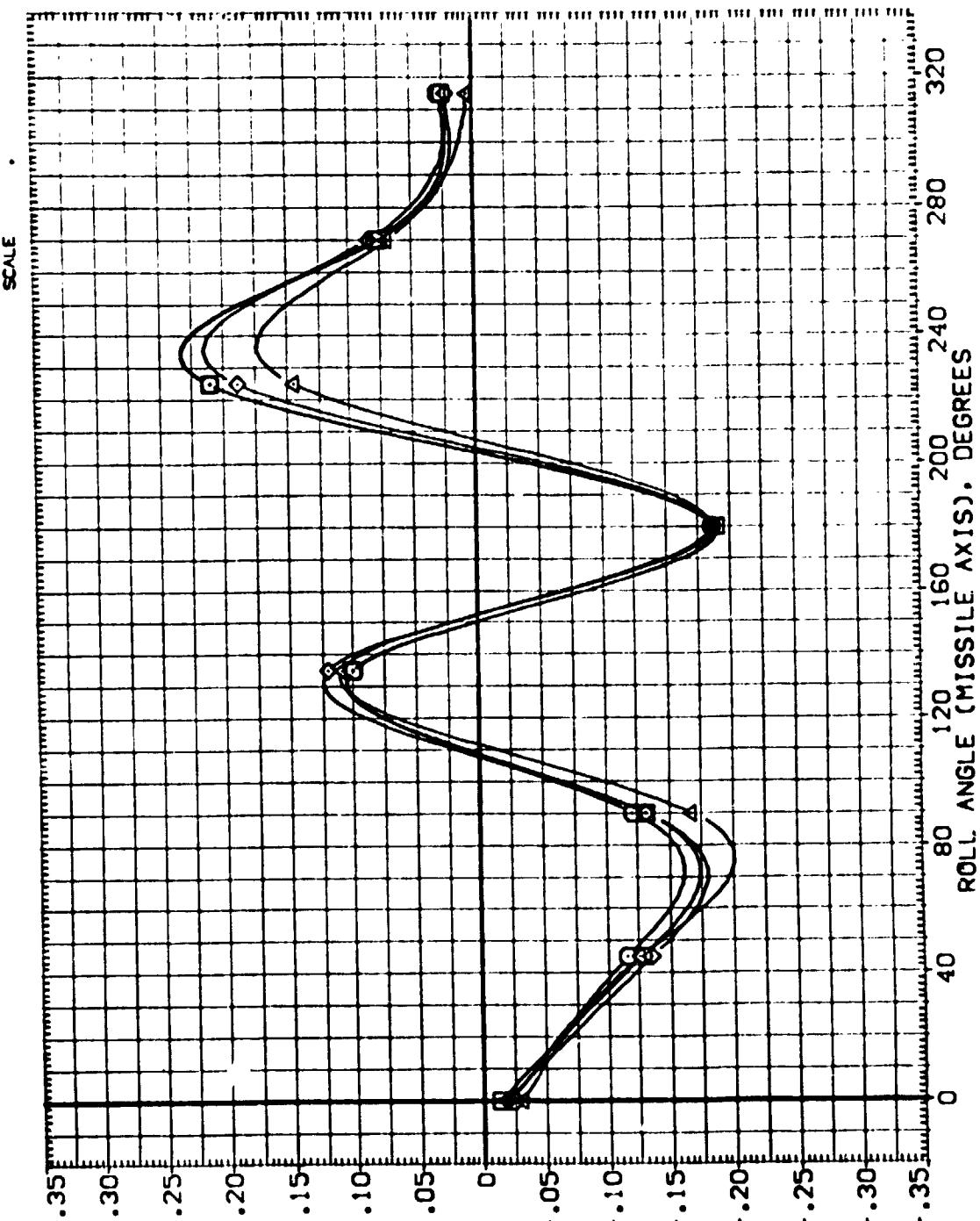
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	P _A TRIC VALUES	R _{ANL}	R _{ANL}
.95.	10.400	330.	1.160
100.		330.	
105.		1406.	
110.			

○□◊△

REFERENCE INFORMATION
SREF 594.1
LREF 330.
BREF 1406.
IN. IN. XT
IN. YT
IN. ZT



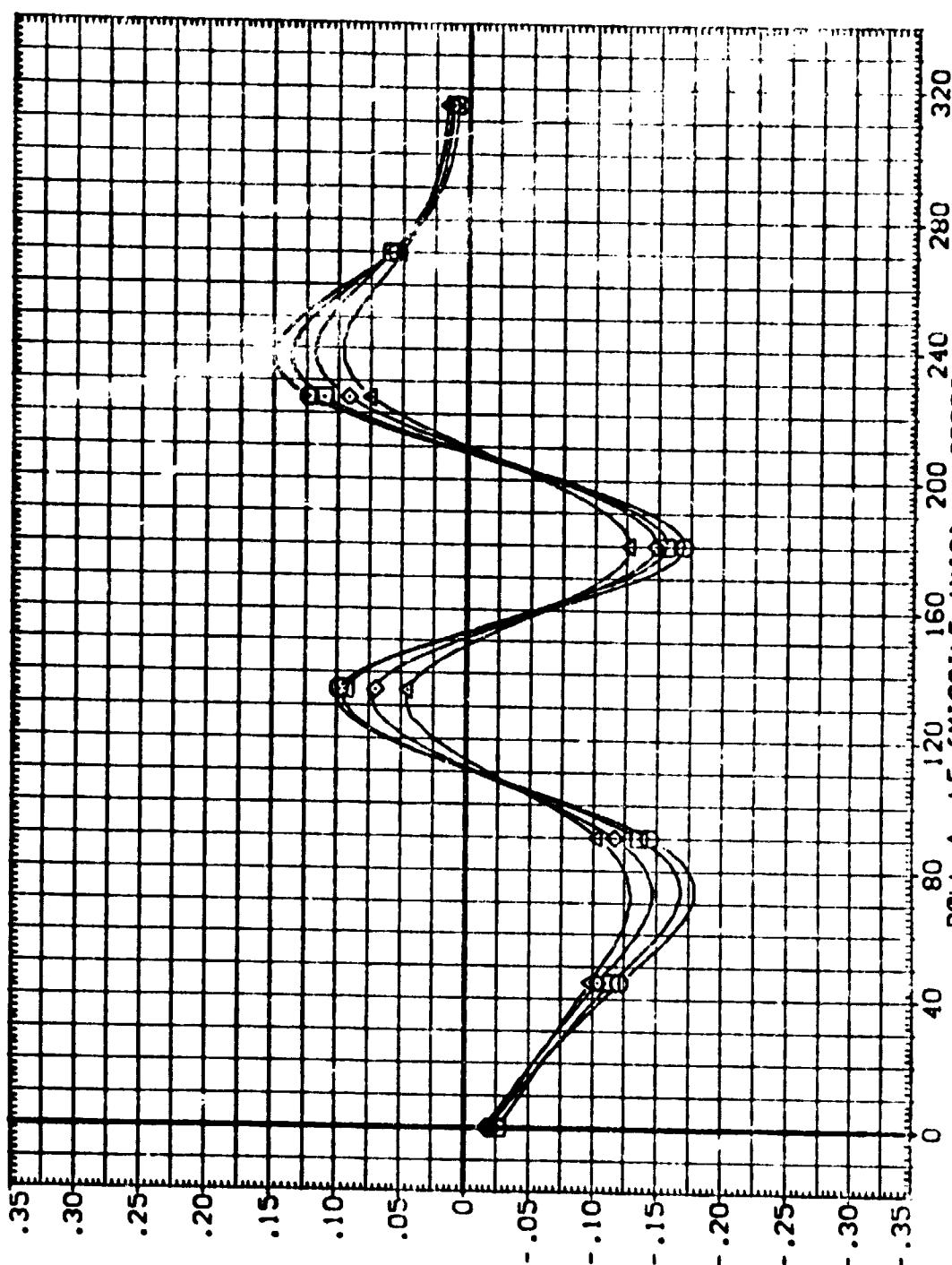
SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TASF ET (TANK WITH PROTUBERANCES) (YM01)

115. 10.400 TRIC V S .150.
120. 1406.
125. 1406.
130. 1406.
135. 1406.
140. 1406.
145. 1406.
150. 1406.
155. 1406.
160. 1406.
165. 1406.
170. 1406.
175. 1406.
180. 1406.
185. 1406.
190. 1406.
195. 1406.
200. 1406.
205. 1406.
210. 1406.
215. 1406.
220. 1406.
225. 1406.
230. 1406.
235. 1406.
240. 1406.
245. 1406.
250. 1406.
255. 1406.
260. 1406.
265. 1406.
270. 1406.
275. 1406.
280. 1406.
285. 1406.
290. 1406.
295. 1406.
300. 1406.
305. 1406.
310. 1406.
315. 1406.
320. 1406.

○□△▲



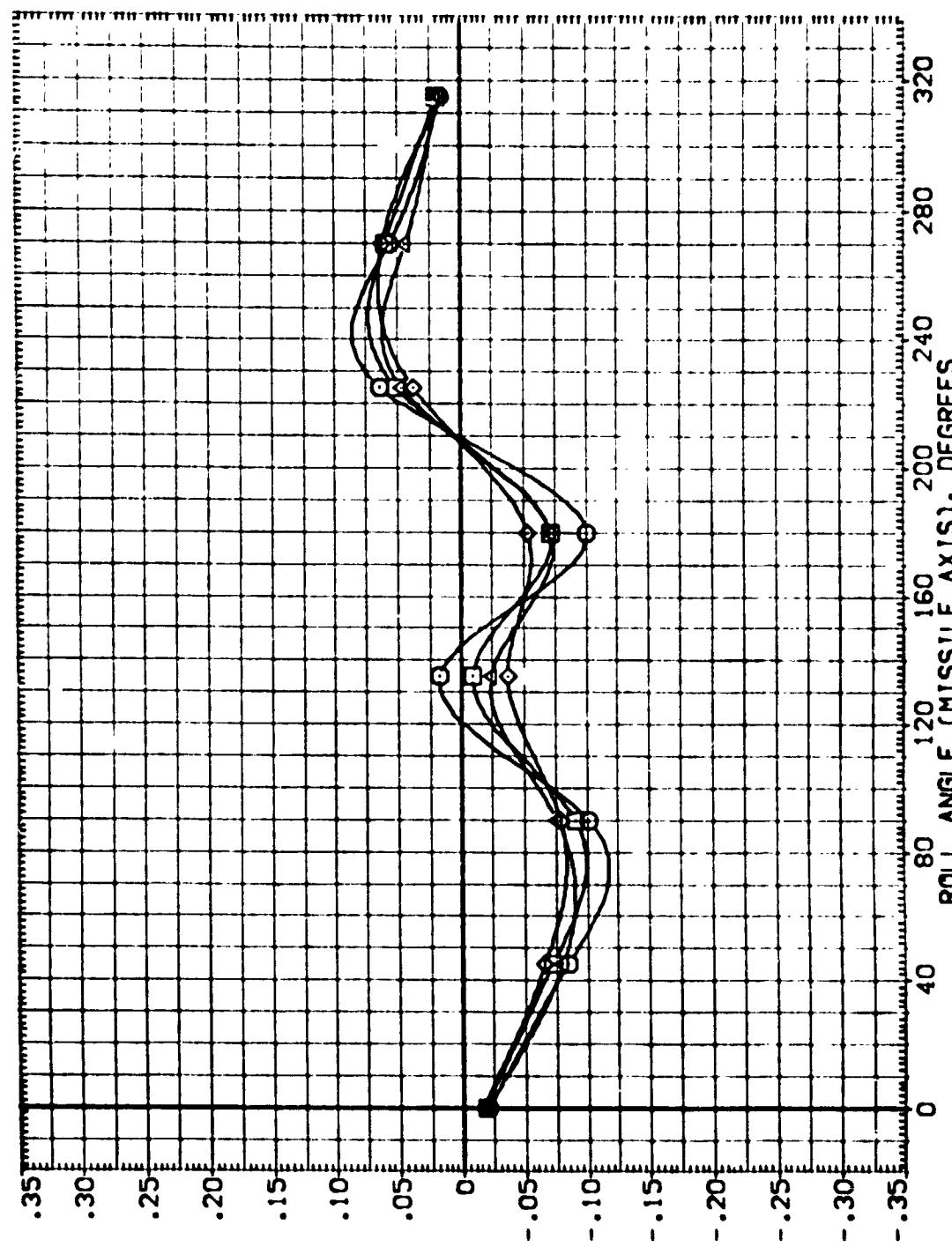
SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMOI)

METRIC V S 1.180
135.
140.
145.
150.
OO♦△

110N.
90.FT.
N.
N.XT
N.YT
N.ZT



SIDE-FORCE COEFFICIENT (MISSILE AXIS), CYM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

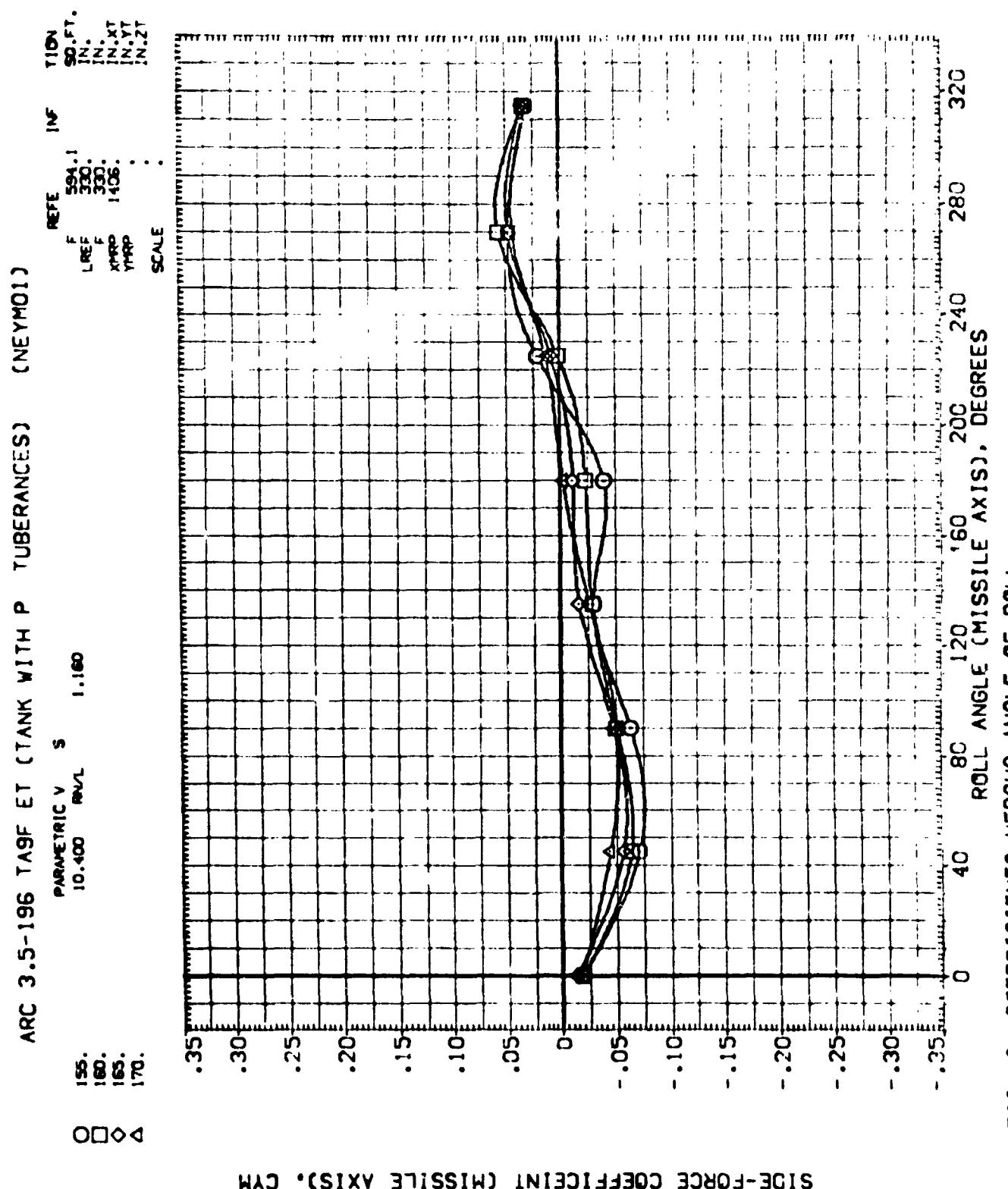


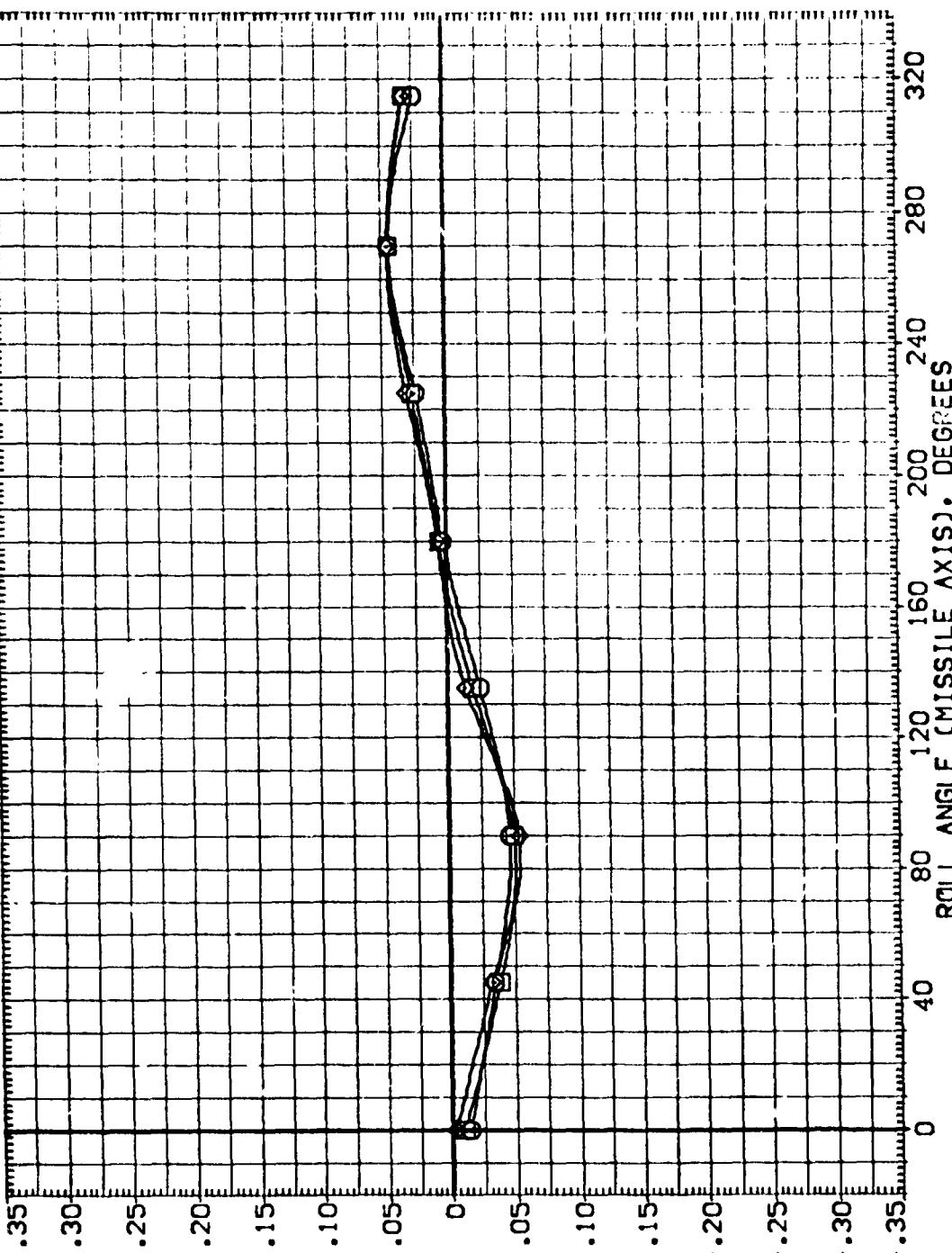
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (LINK WITH PROTUBERANCES) [NEYMO1]

ALPHA^P TRIC VALUES 1.160
 175. 10.400 ROLL
 180. 1.160
 185.000

○ ◇

REFERENCE INF.
 SREF. 594.1300 SD.FT.
 LREF. 330. N.
 BREF. 330. N.XT
 XMP. 1406. N.YT
 YMP. 1406. N.ZT
 ZMP. 1406. N.ZT
 SCALE.



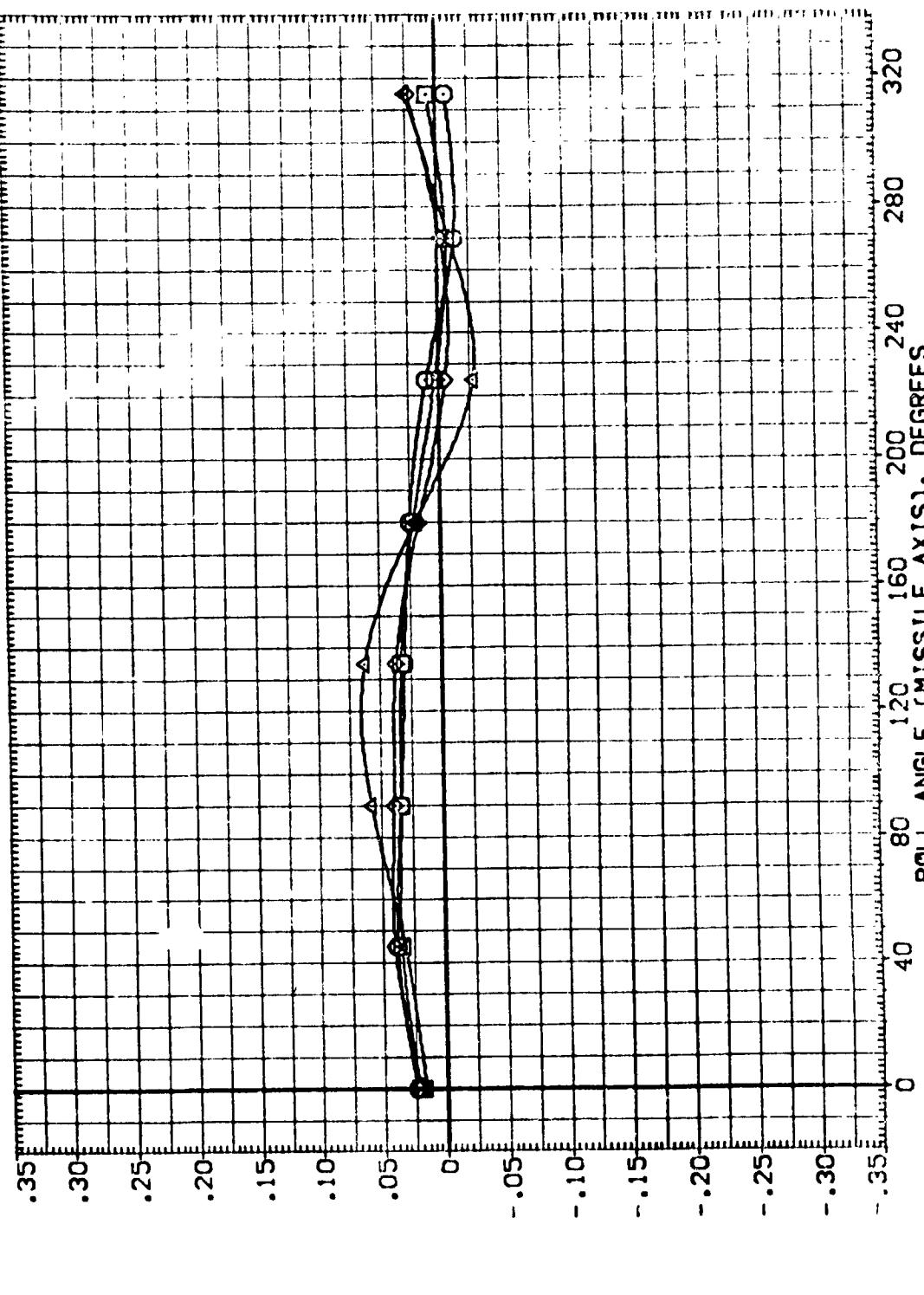
SIDE-FORCE COEFFICIENT (MISSILE AXIS). CYM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAG ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
ALPHA -5.
MACH 10.400 ROLL 1.160
5.000
10.000

REFERENCE INFORMATION
SREF 594.1
LREF 330.
BREF 330.
XMRP 1406.
YMRP
ZMRP
SCALE



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

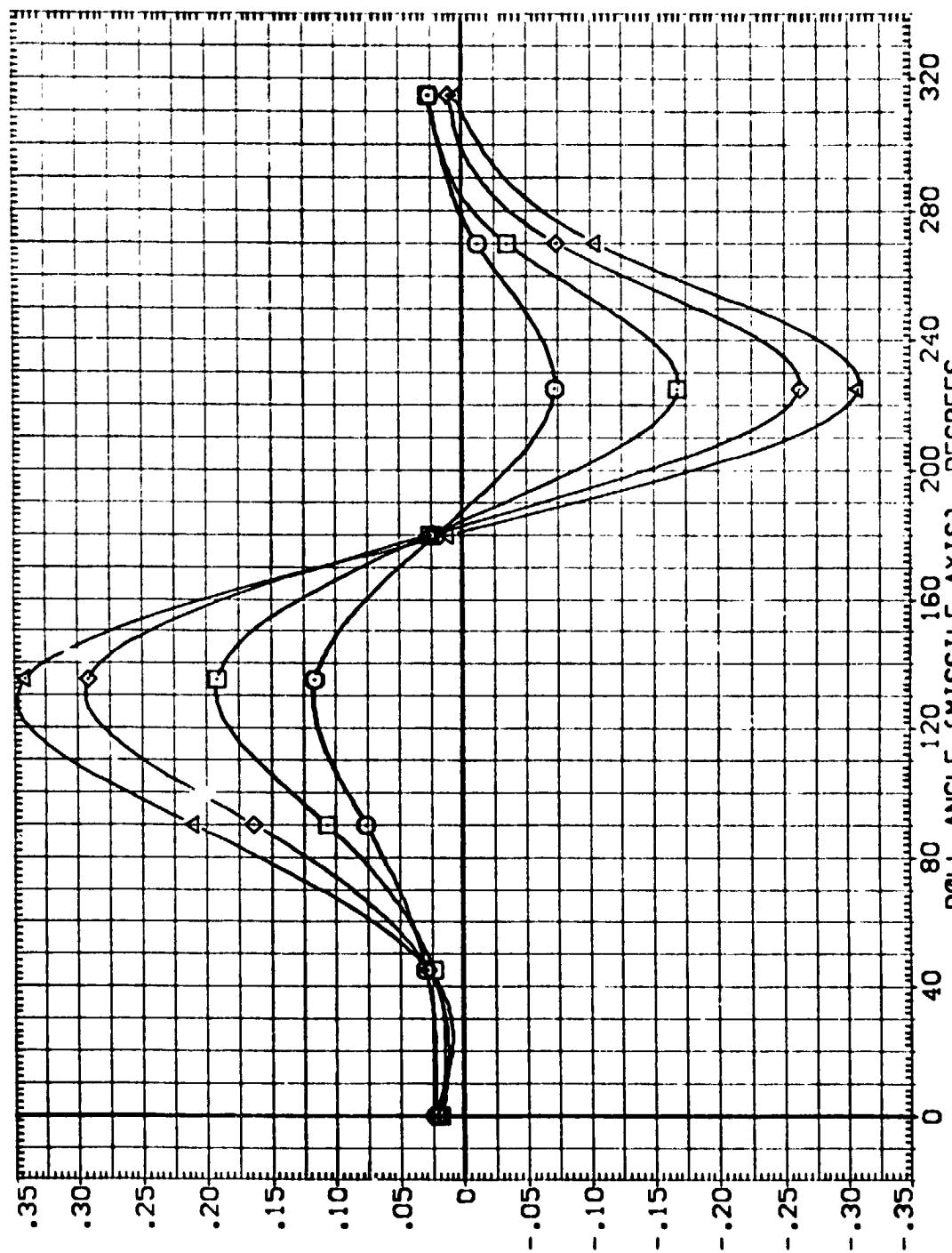
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

P_T TRIC VALUES 1.160
ALPHA
15.
20.
25.
30.000

REF NCE INF
LREF 594.1
300.
330.
1406.
XMRP
YMRP
ZMRP
SCALE

○ □ ◇ △



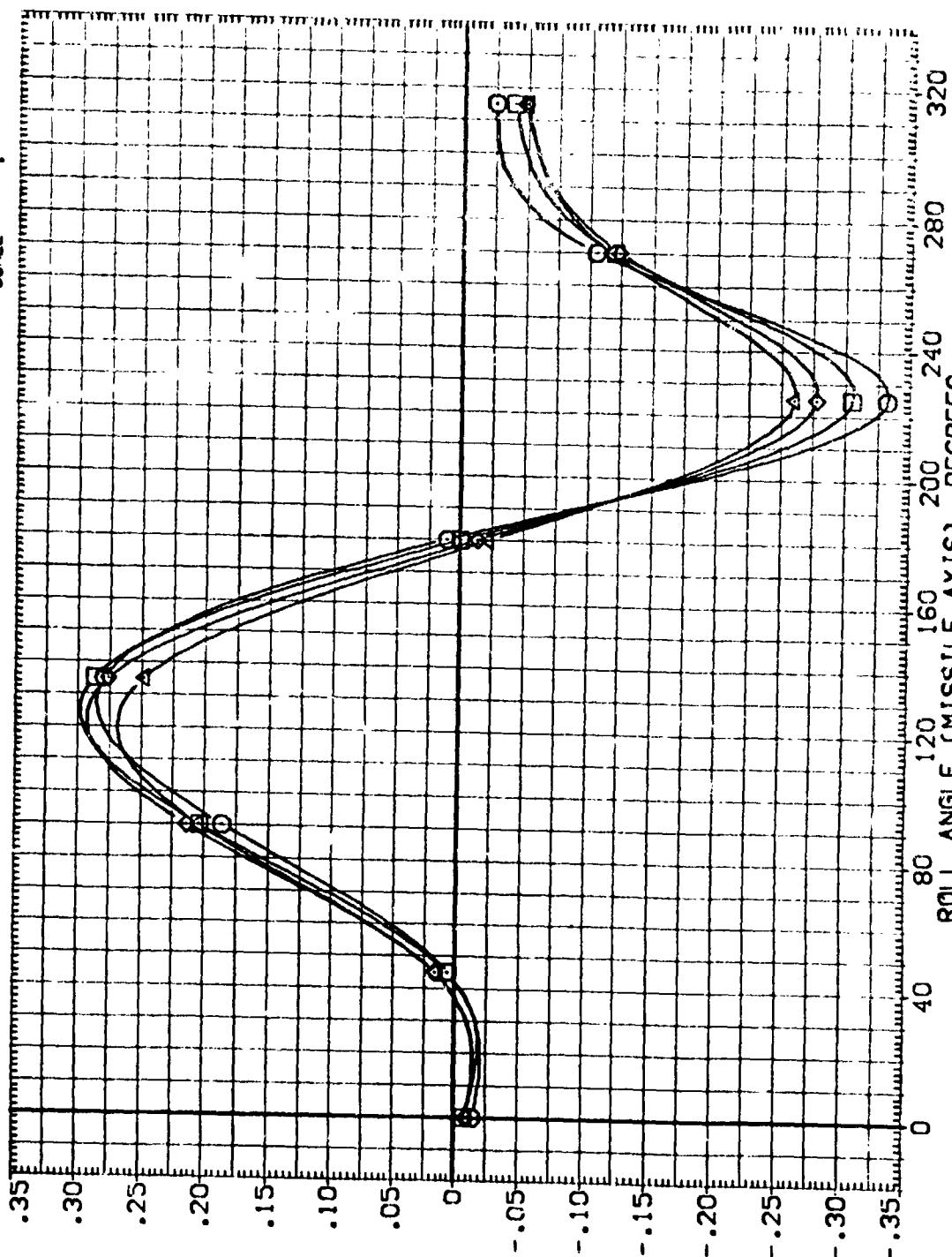
YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES	
ALPHA 30. 35. 40.000 45.000	MACH 10.400 11.60
RM/L	

REFERENCE INF
50. FT.
LREF 330.
BREF 200.
XRP 140.
YRP 15.
ZRP 27.
SCALE



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

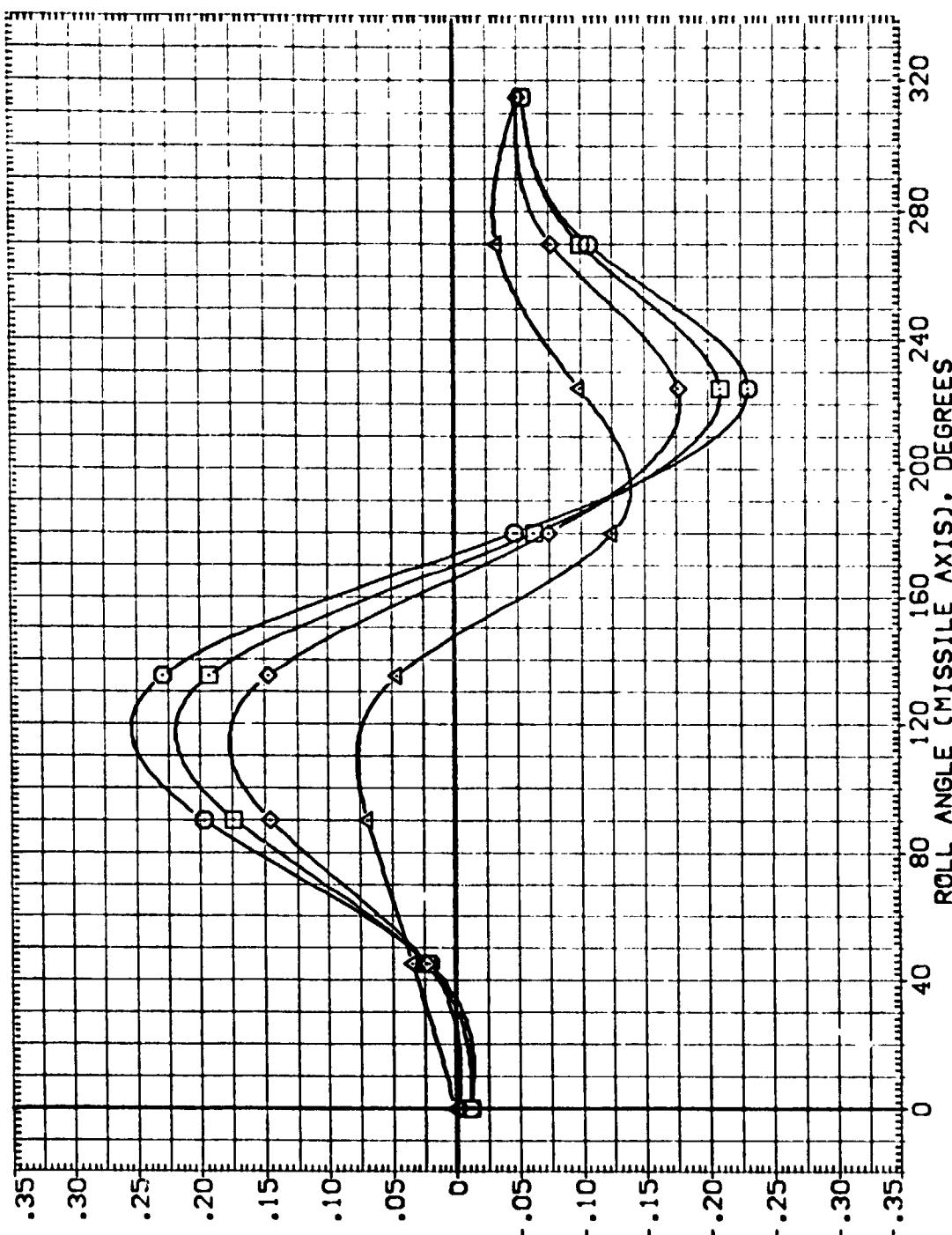
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 1.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA
50.
55.
60.000
70.000

P_T TRIC VALUES
10.400 RNL 1.160

REFERENCE INFORMATION
SREF 594.1360 SQ.FT.
LREF 330. IN.
BREF 330. IN.
XMRP 146. IN.XT
YMRP 60. IN.YT
ZMRP 70. IN.ZT
SCALE



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

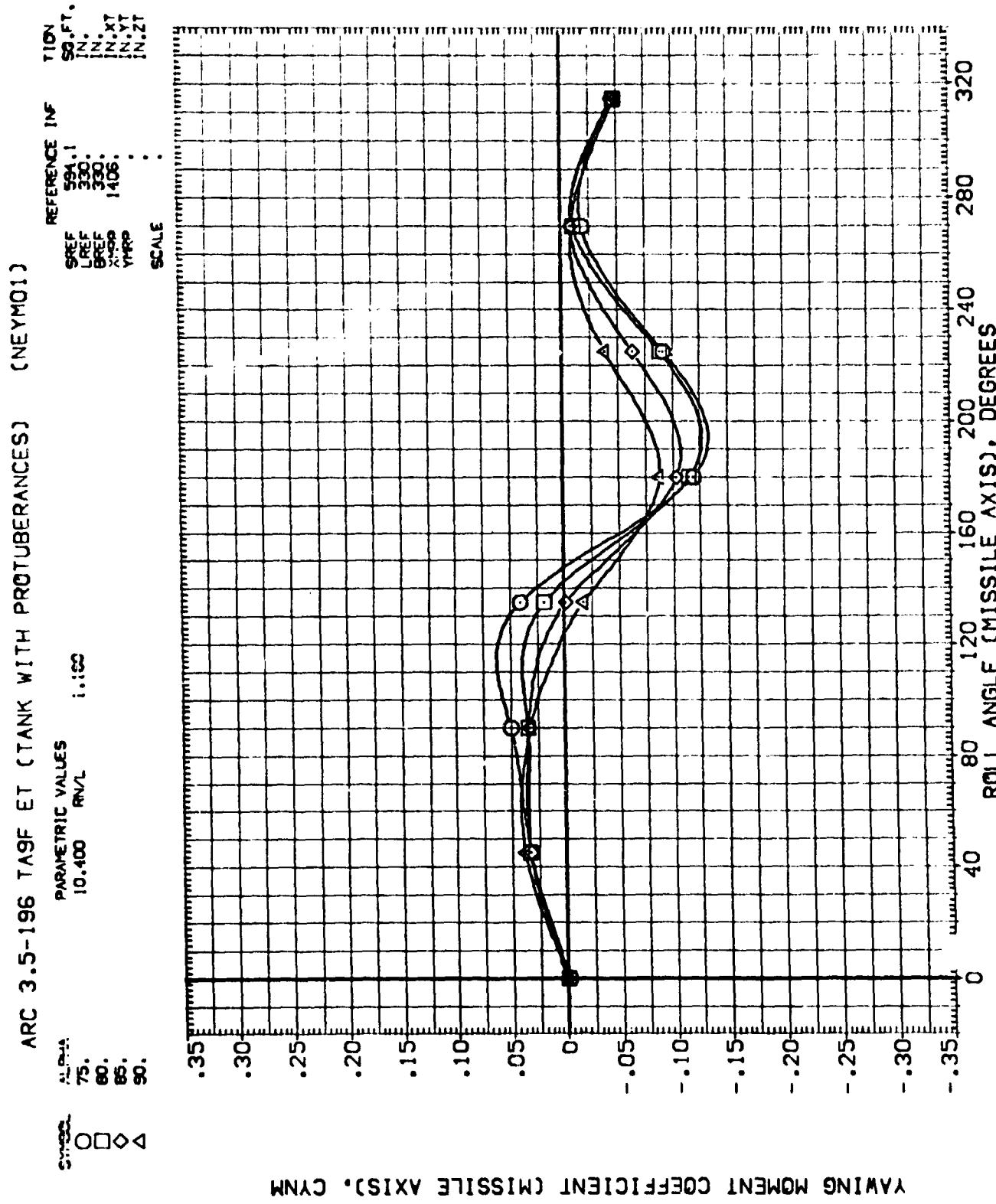


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	P _T TRIC VALUES	RNL
95.	100.	10.400	1.160
105.000			
110.000			

○ □ ◇ △

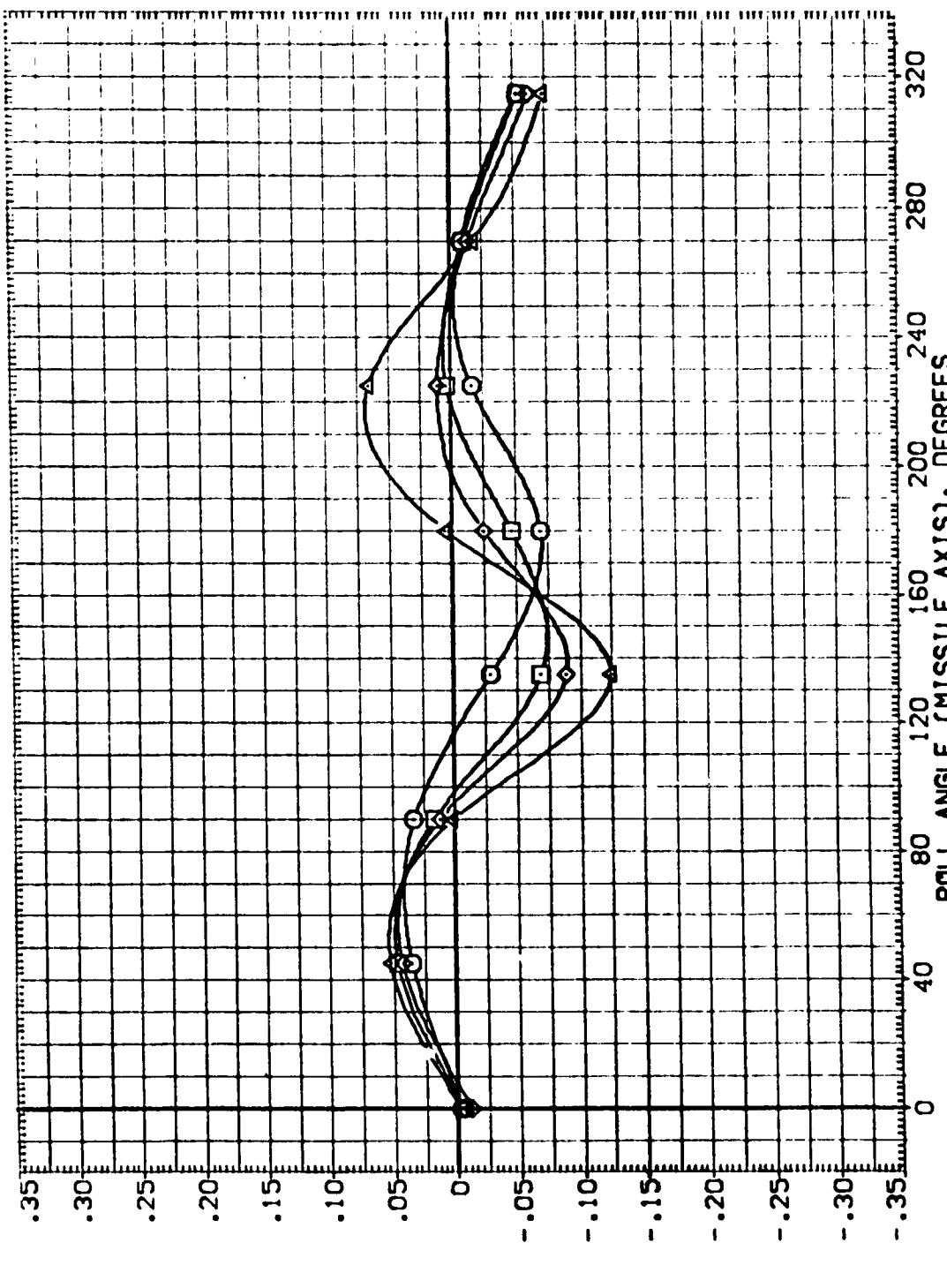
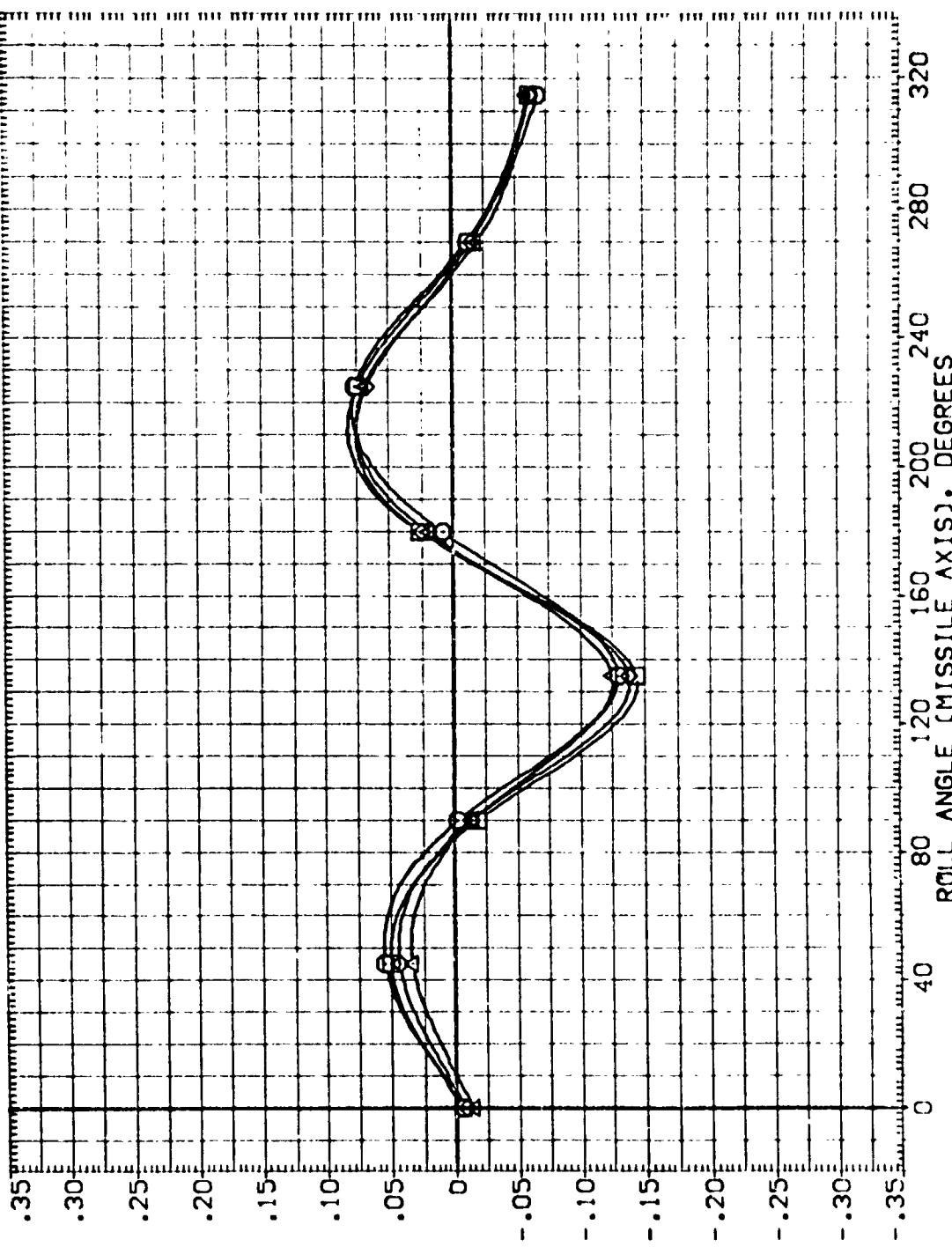


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
 ALPHA 115.000 MACH 1.160
 120.000 10.400 ROLL 1.160
 125.000
 130.000

REFERENCE IN
 SREF 594.1360 IN.
 LREF 330.2000 IN.
 BREF 330.2000 IN.
 XMRP 146.0000 IN.X
 YMRP .0000 IN.Y
 ZMRP .0000 IN.Z
 SCALE .0360



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

PAGE :0:

ARC 3.5-1.0 AIR CRANK WITH PROTUBERANCES (NEYMO:)

ALPHA MACH 10.25 ROLL 1.160

15.000 140.000 145.000 150.000

S Q C

REFERENCE IN
SO. FT.
SREF 594.1360
LREF 330.
BREF 330.
XMRP 1408.
YMRP 2408.
ZMRP 2408.
SCALE

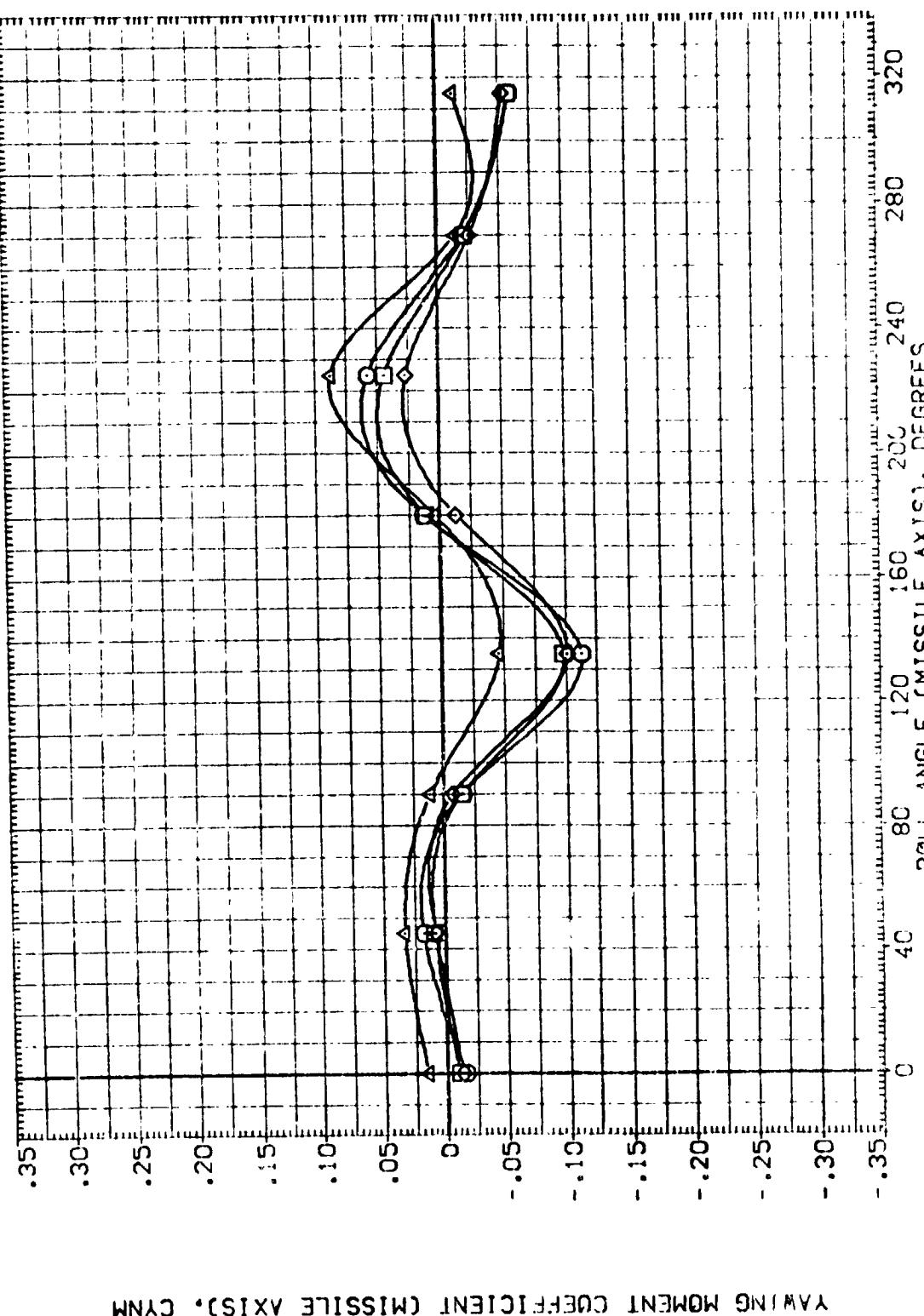


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES

ALPHA	MACH	10.400	RNL	1.160
155.000				
160.000				
165.000				
170.000				

REFE
LREF
BREF
X₁₂₀
Y₁₂₀
Z₁₂₀
SCALE

REFE
LREF
BREF
X₁₂₀
Y₁₂₀
Z₁₂₀
SCALE

○ □ ◇ ▲

yawing moment coefficient (missile axis). cym

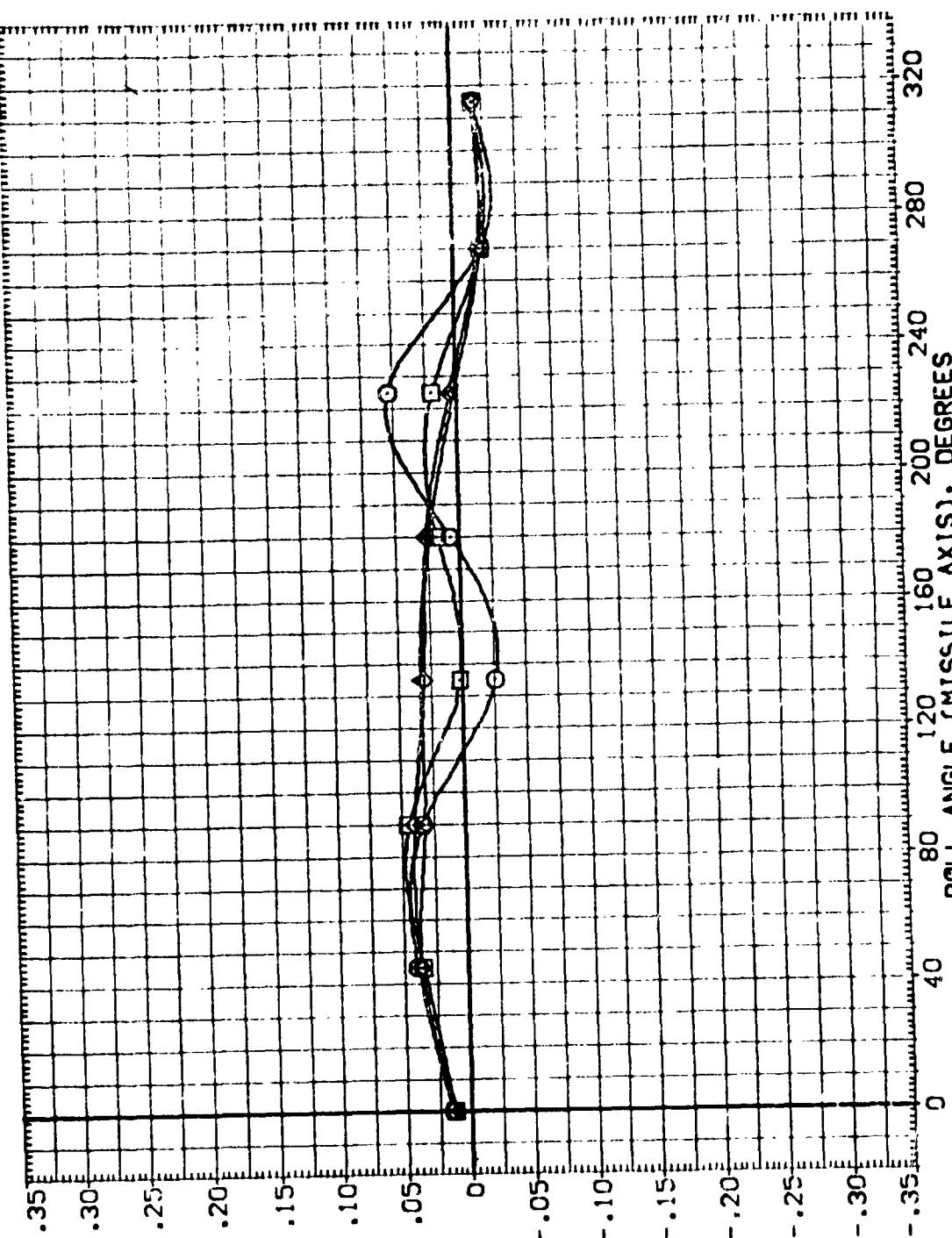
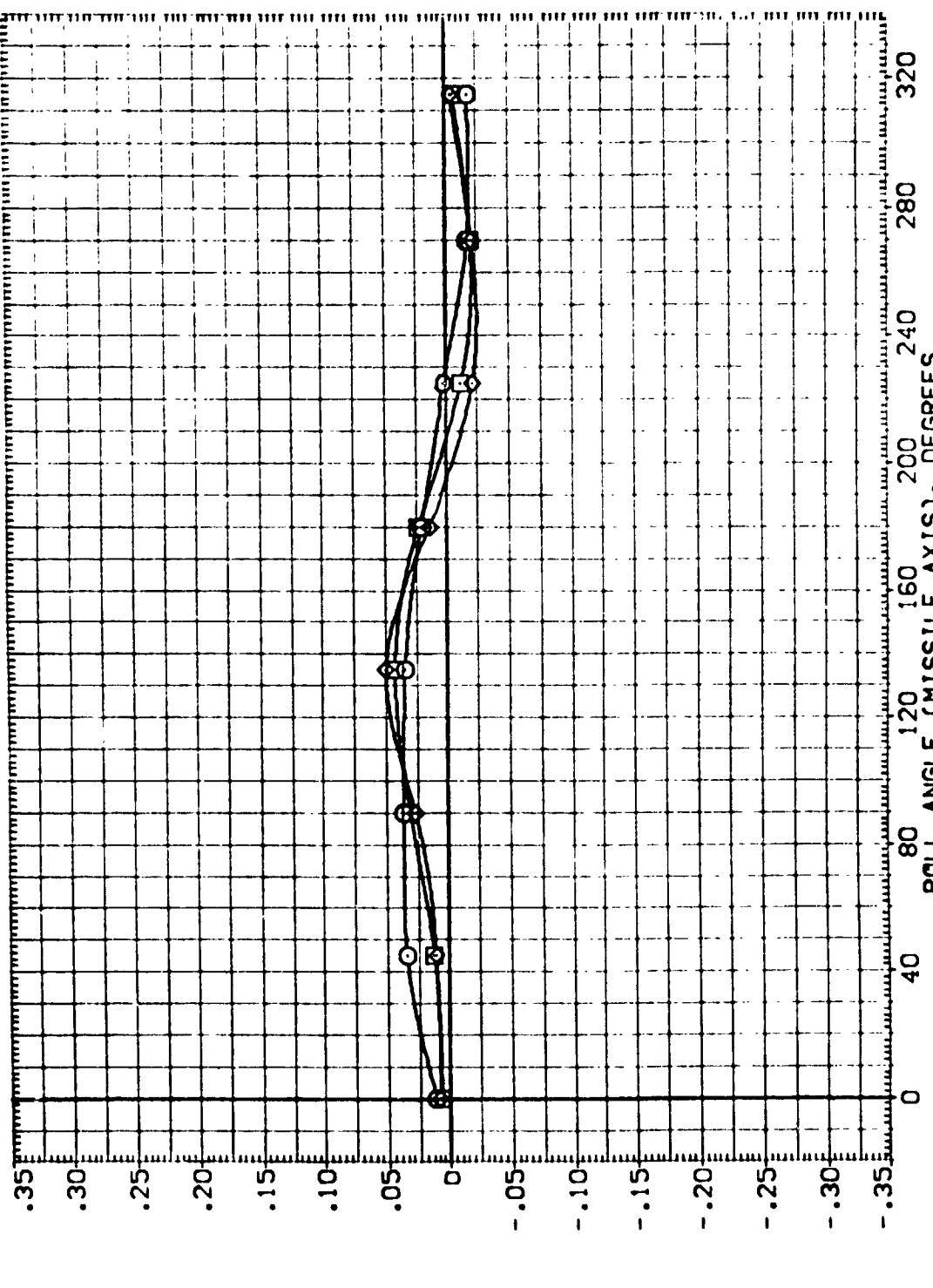


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PROTRUSION
VALUES
10.400 IN/L 1.180
175.
180.
185.
190.
195.
200.
205.

PROTRUSION
VALUES
10.400 IN/L 1.180
175.
180.
185.
190.
195.
200.
205.



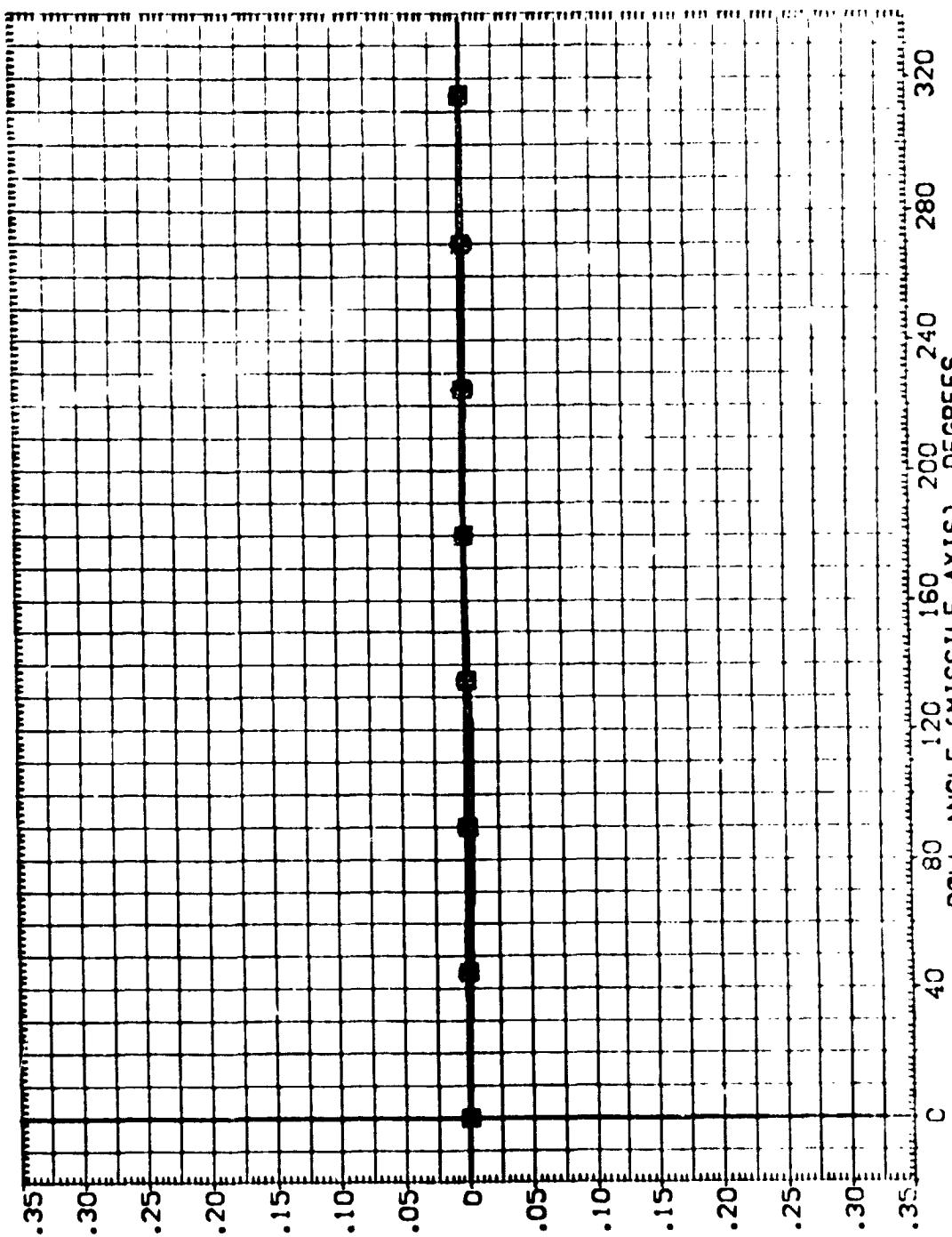
YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

P TRIC VALUES
10.400 1100 1.160
0 □ ◇ ▲

REFERENCE :
SREF 594.1
LREF 330.
BREF 330.
XMRP 1406.
YMRP 1406.
IN.XT
IN.YT
IN.ZT
SCALE



ROLLING MOMENT COEFFICIENT (MISSILE AXIS), C

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

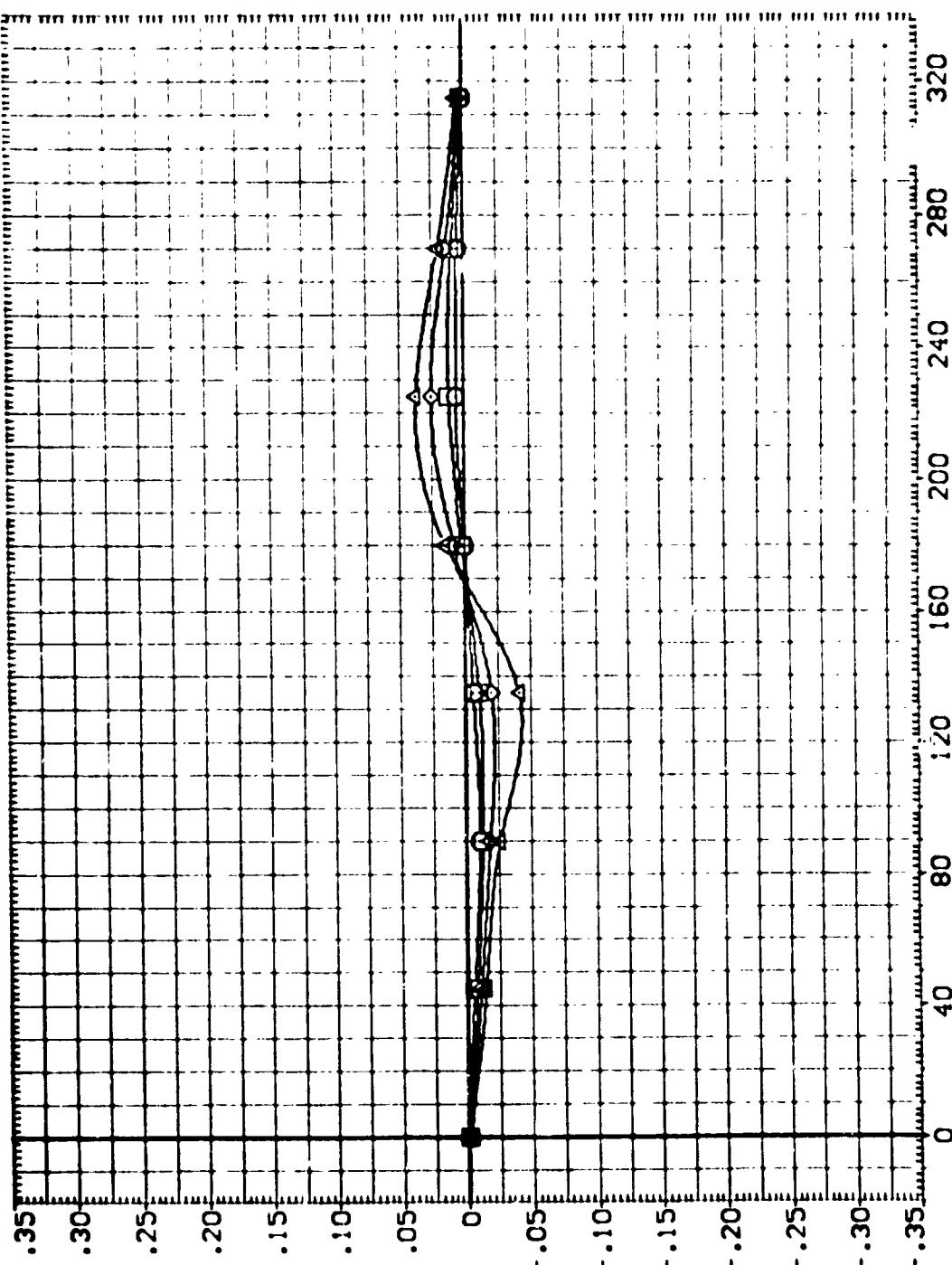
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

TRIC V S 1.160
10.400 ROLL 1.160
20.
25.000
30.

REF 330.
LREF 330.
BREF 146.
XMP 146.
YMP 146.
NXT N.YT
N.ZT

REF INF TION
SREF 330.
LREF 330.
BREF 146.
XMP 146.
YMP 146.
N.YT
N.ZT

SCALE .0063



ROLLING MOMENT COEFFICIENT (MISSILE AXIS). C

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMOI)

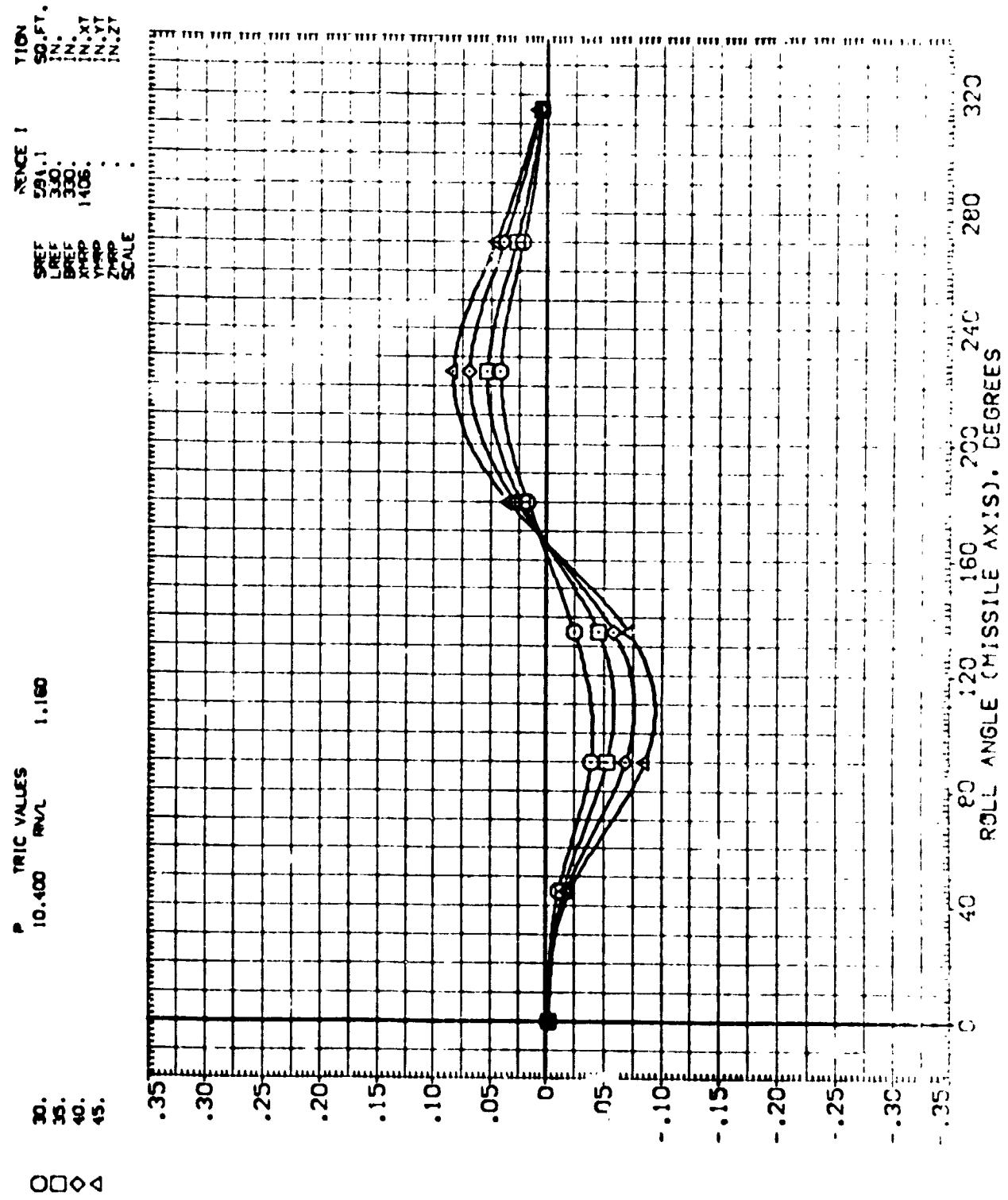


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	PARAMETRIC VALUES
50.000	10.400	RNL
55.000		
60.000		
70.000		

○ □ ◇ △

ROLLING MOMENT COEFFICIENT (MISSILE AXIS). CBL

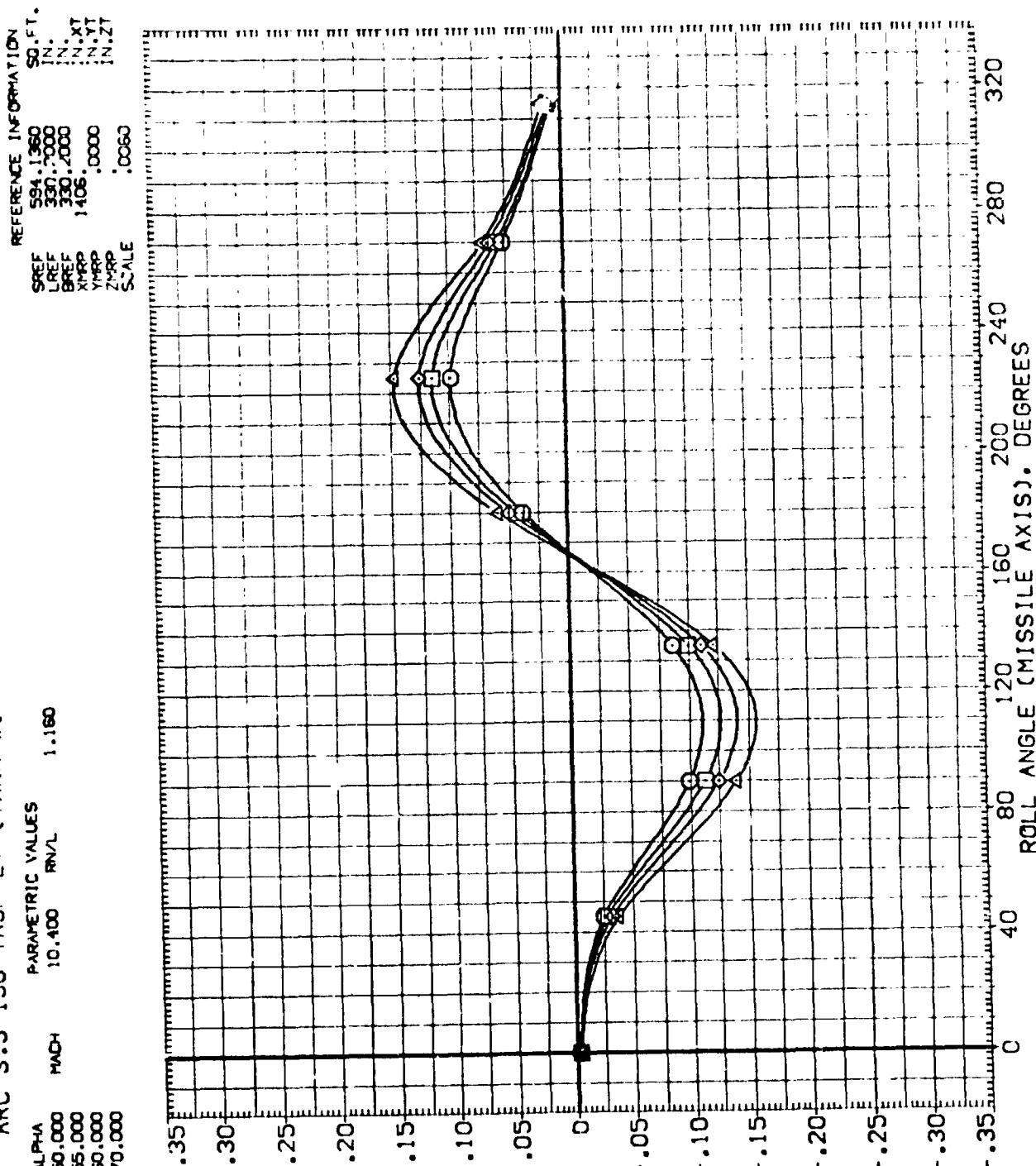


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

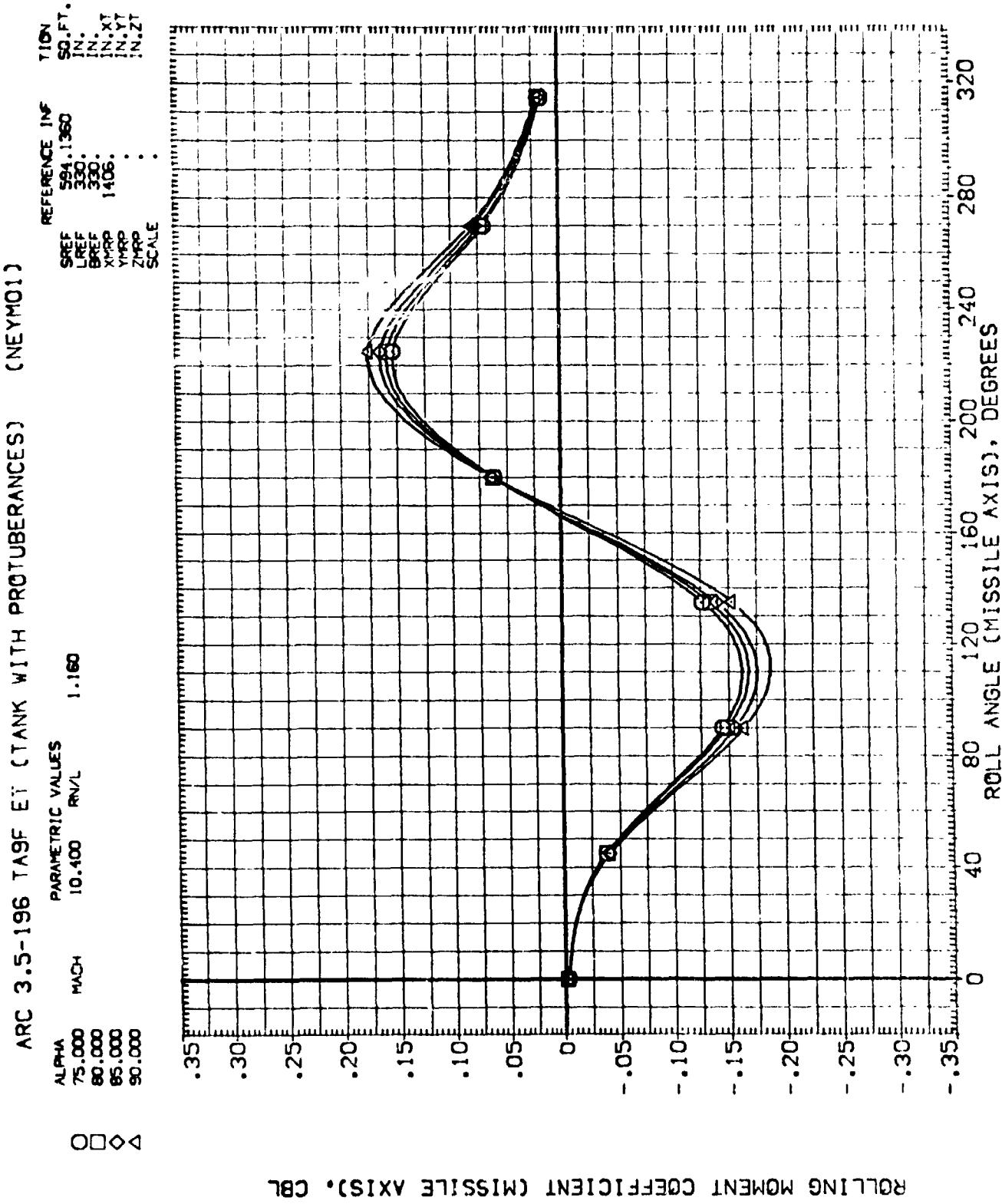


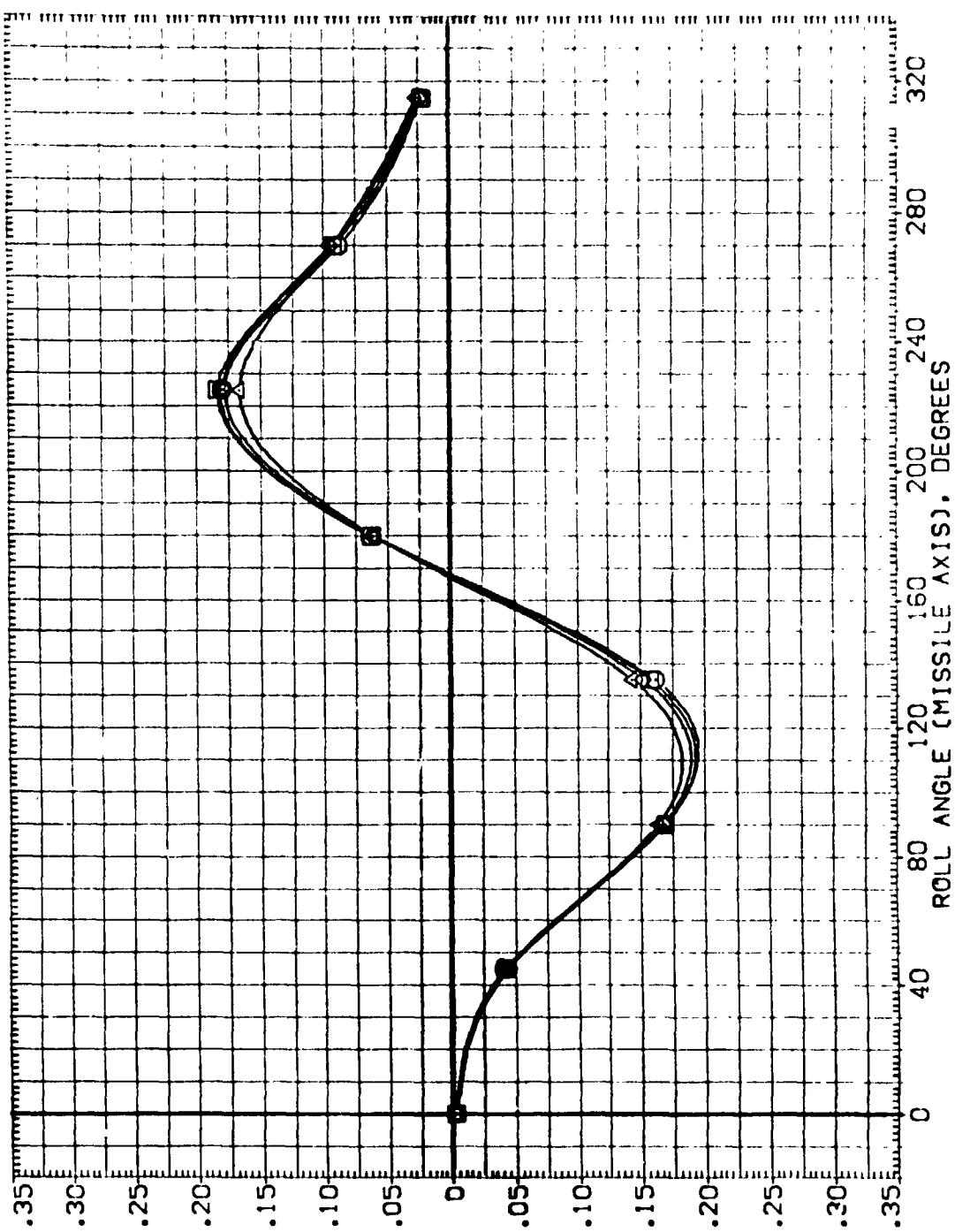
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
10.400 RNL 1.160
ALPHA
95.000
100.000
105.000
110.000

O □ ◇ △

REFERENCE INFORMATION
SREF 594.1360
LREF 330.2000
BREF 330.2000
XMRP 1405.0000
YMRP .0000
ZMRP .0000
SCALE



ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

ALPHA	MACH	RN/L	PARAMETRIC VALUES
115.000			1.160
120.000			10.400
125.000			
130.000			

□ ◇ △

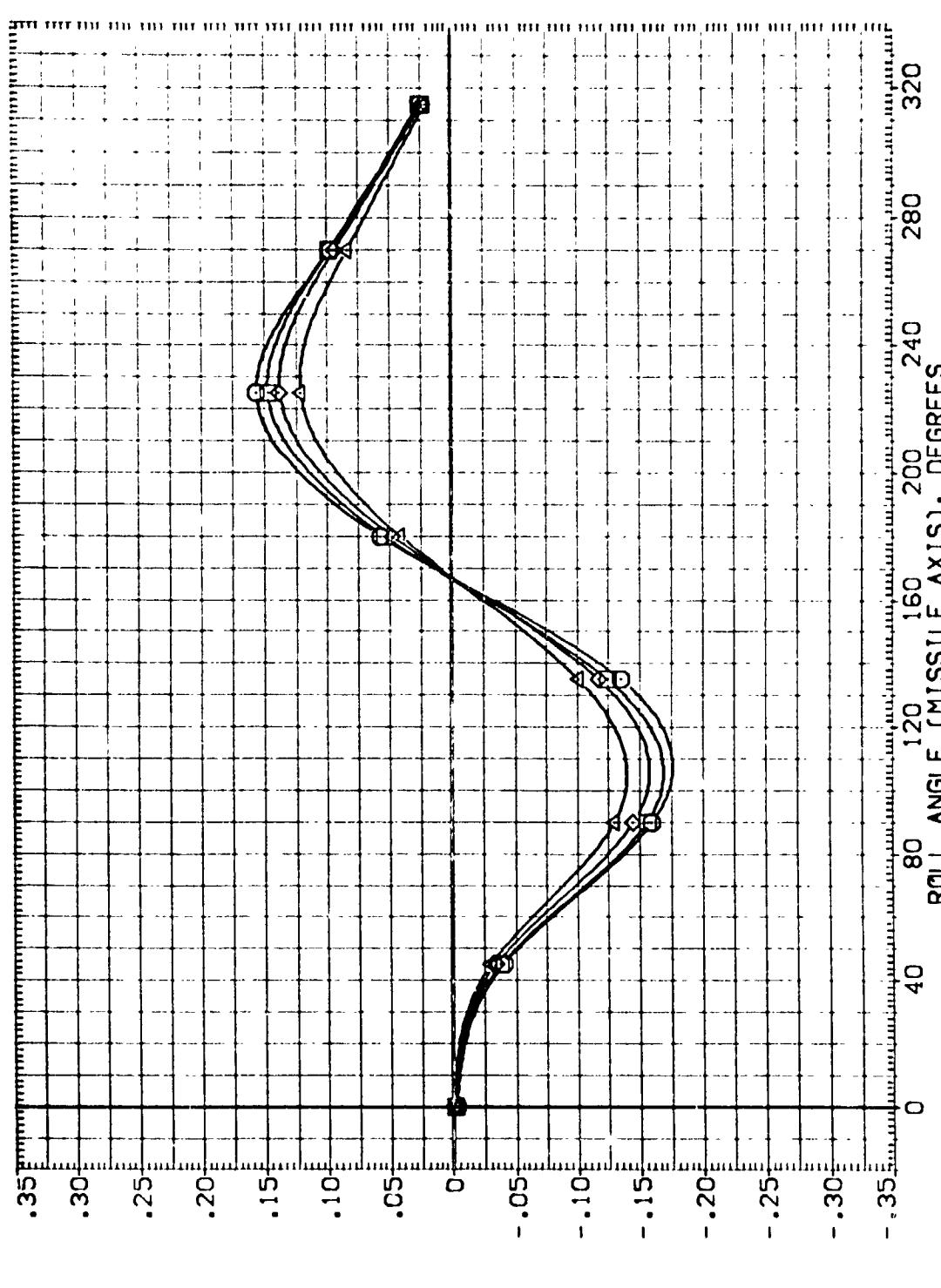


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

PAGE 111

ARC 3.5-195 TANK ON TANK WITH PROTUBERANCES (NEYMO:)

PARAMETRIC VALUES

ALPHA	.15.000	.20.000	.25.000	.30.000
R _{ML}	135.000	140.000	145.000	150.000
R _{ML}	1.160	1.200	1.240	1.280

REFERENCE INFORMATION

SREF	594.1360	SO.FT.
LREF	330.2000	IN.
BREF	330.2000	IN.
X-MRF	1406.0000	IN.XT
Y-MRF	.0000	IN.YT
Z-MRF	.0000	IN.ZT
SCALE	.0060	

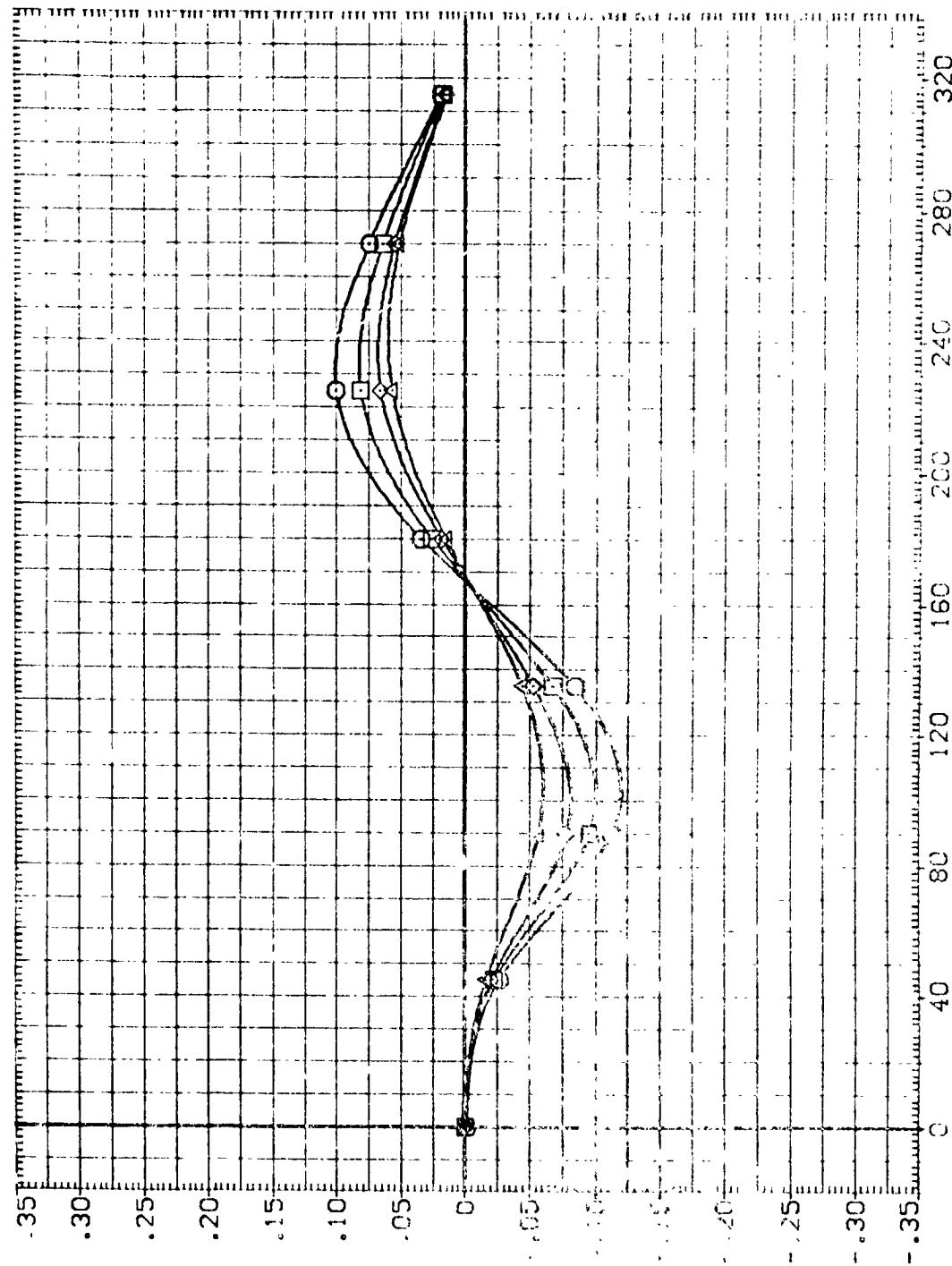


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
 ALPHA 155.000 MACH 10.400 ROLL 1.160
 160.000
 165.000
 170.000

○ □ ◇ △

REFERENCE INFORMATION
 SREF 594.1360 SO.FT.
 LREF 330.2000 IN.
 BREF 330.2000 IN.
 XRP 1468.0000 IN.XT
 YRP .0000 IN.YT
 ZRP .0000 IN.ZT
 SCALE .0050

ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

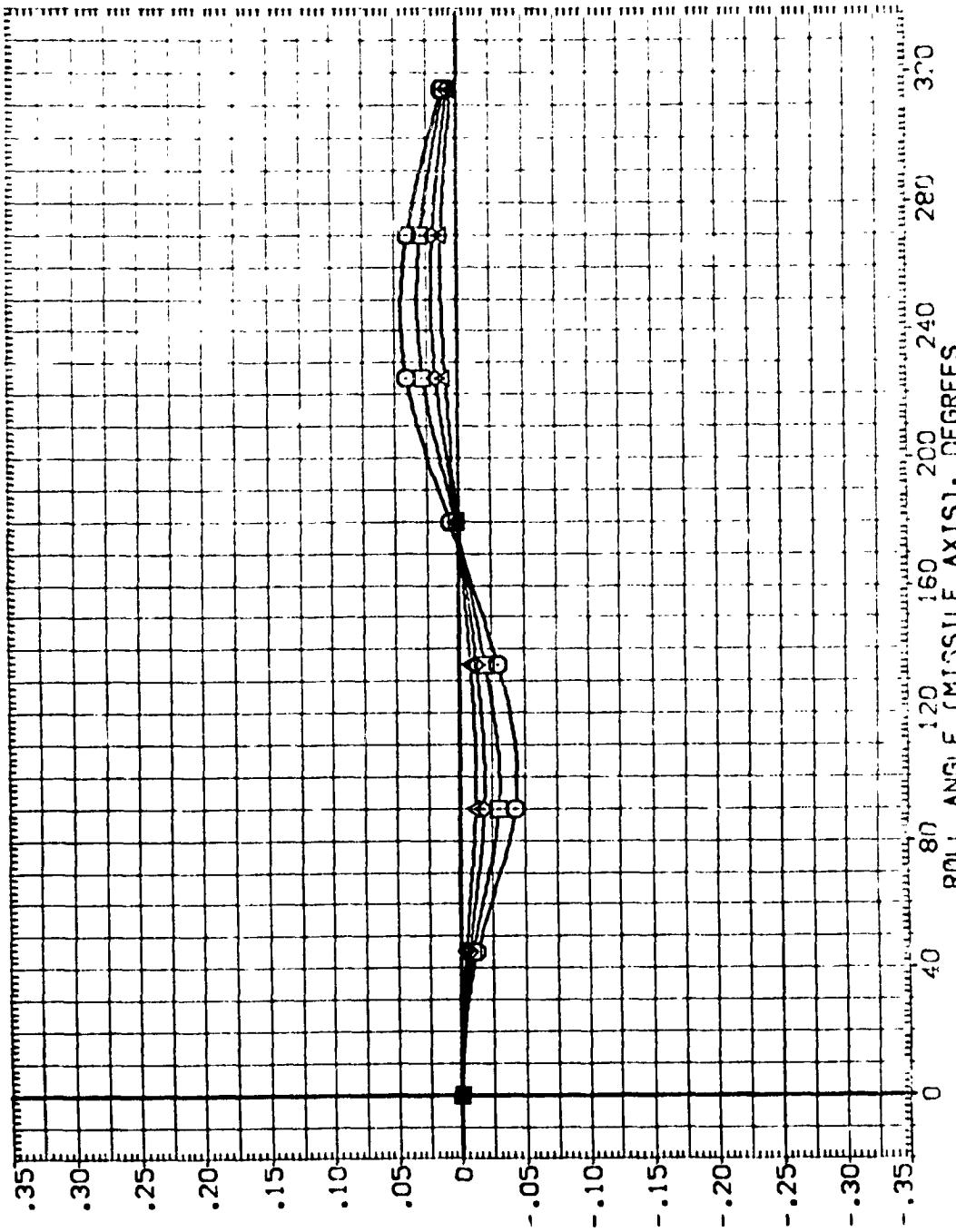


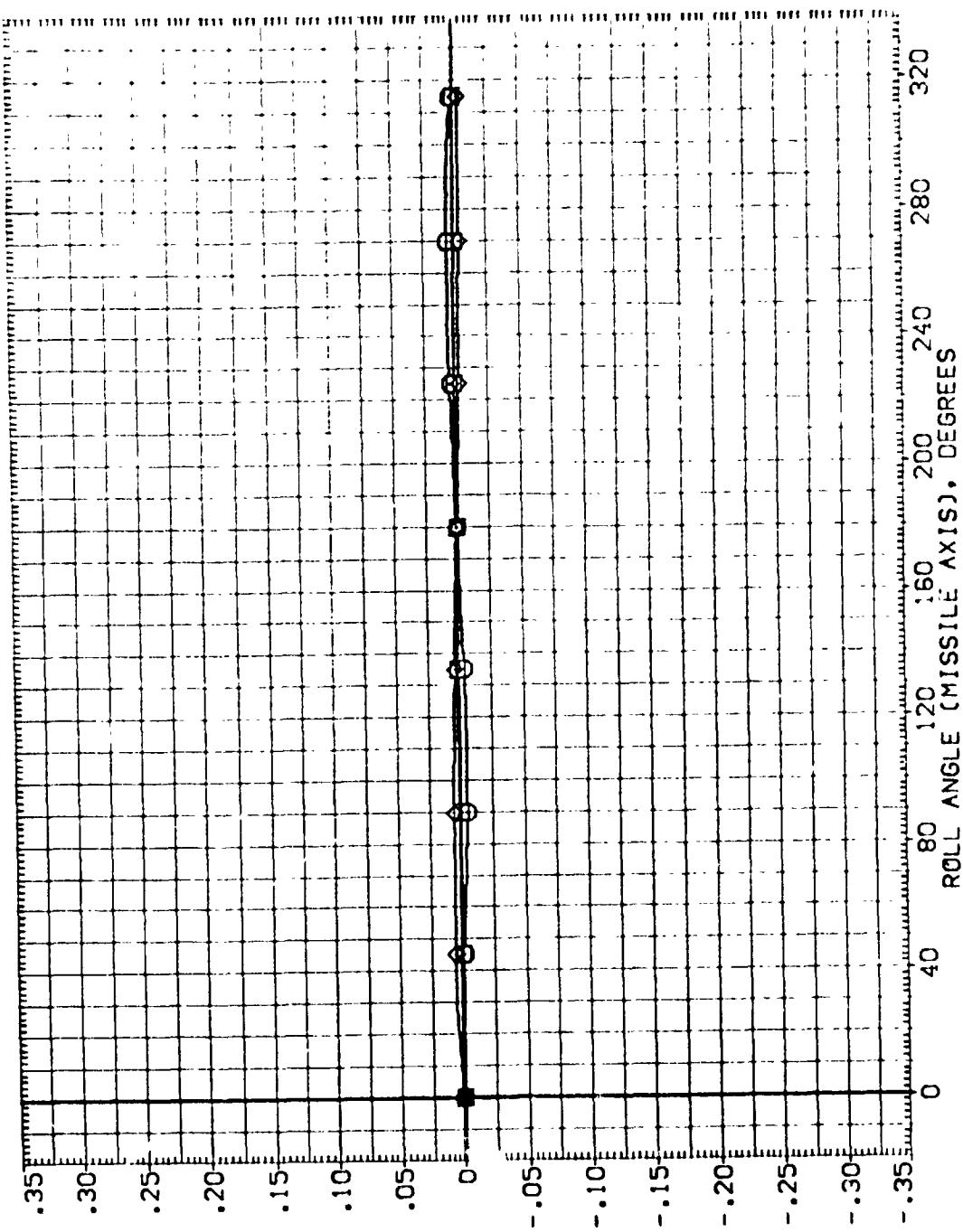
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES	10.100	RNL	1.160
ALPHA			
175.000	MACH		
180.000			
185.000			

○□◊

REFERENCE INFORMATION
 SREF 594.1350 SC. ST.
 LREF 330.2000
 BREF 330.2000
 XMP 1406.0000 XY
 YMP .0000 ZY
 ZMP .0000 SC.
 SCALE .0060



ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
MACH 10.400 RPL 1.160

ALPHA	.000
	.500
	1.000

REFERENCE IN
SQ.FT.
LREF 594.1360
BREF 330.
XHPP 1406.
YHPP 2000.
ZHPP 1000.

SCALE

IN.
IN.XT
IN.YT
IN.ZT

CENTER OF PRESSURE L ATTION, XCP/L

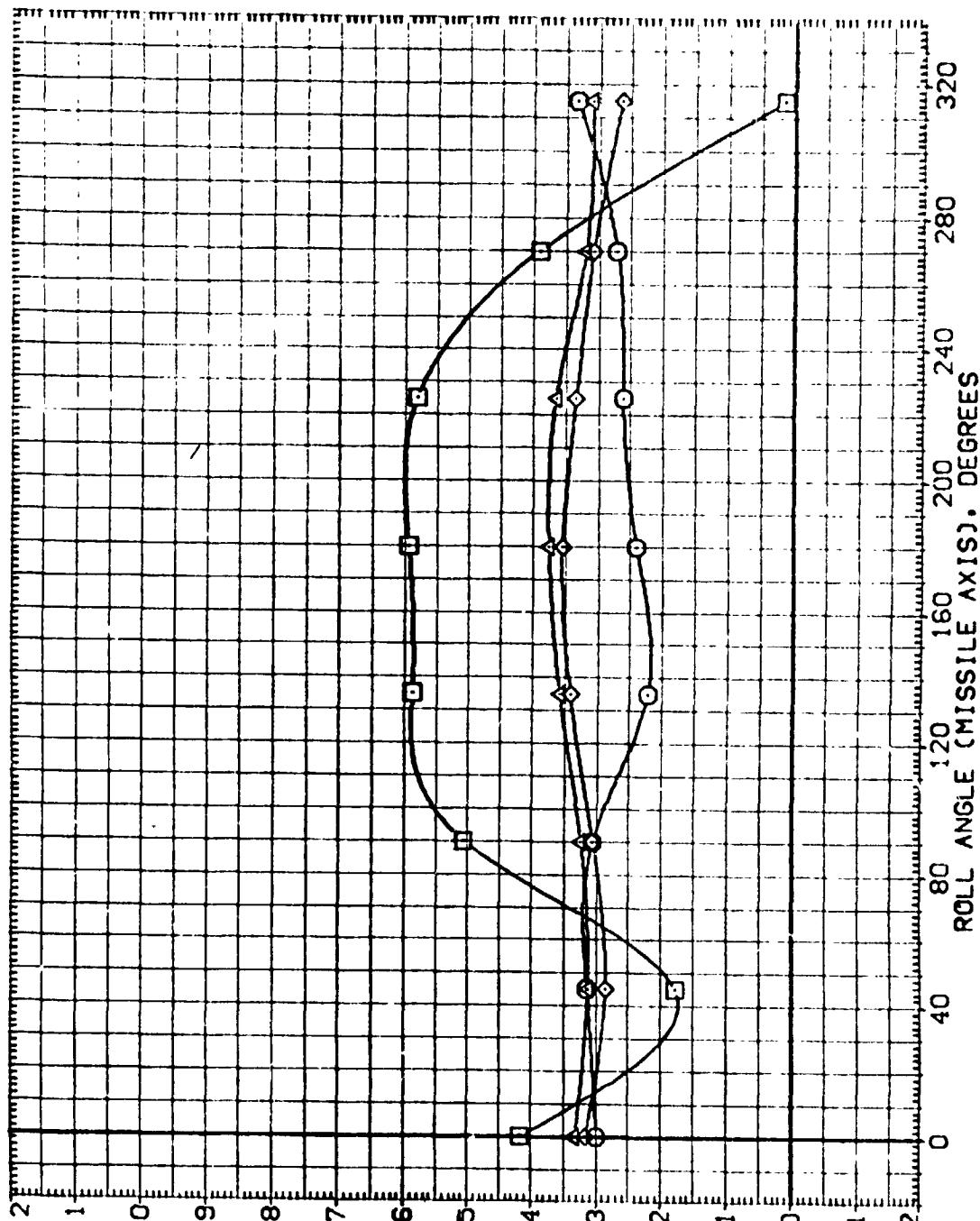


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

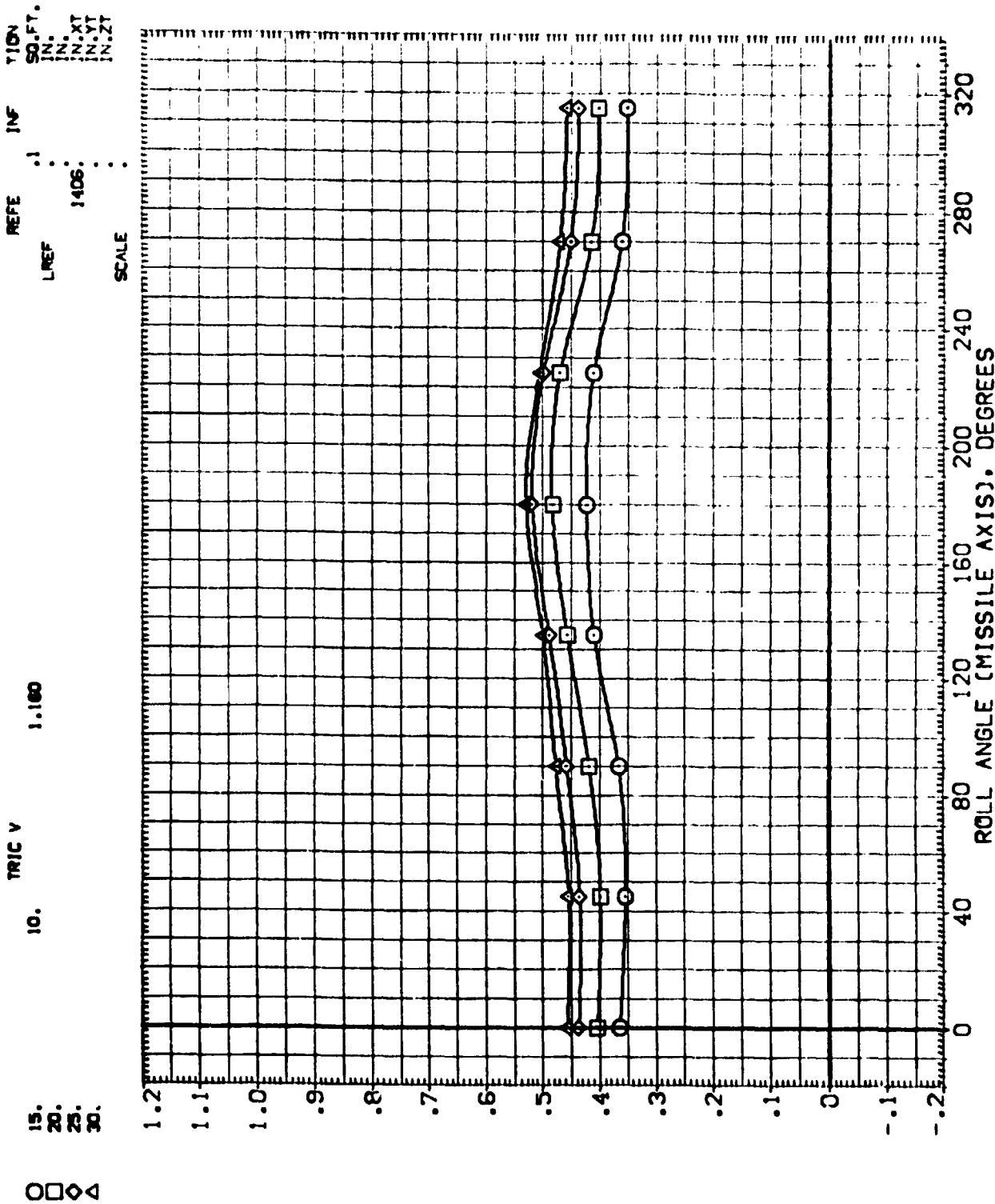


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

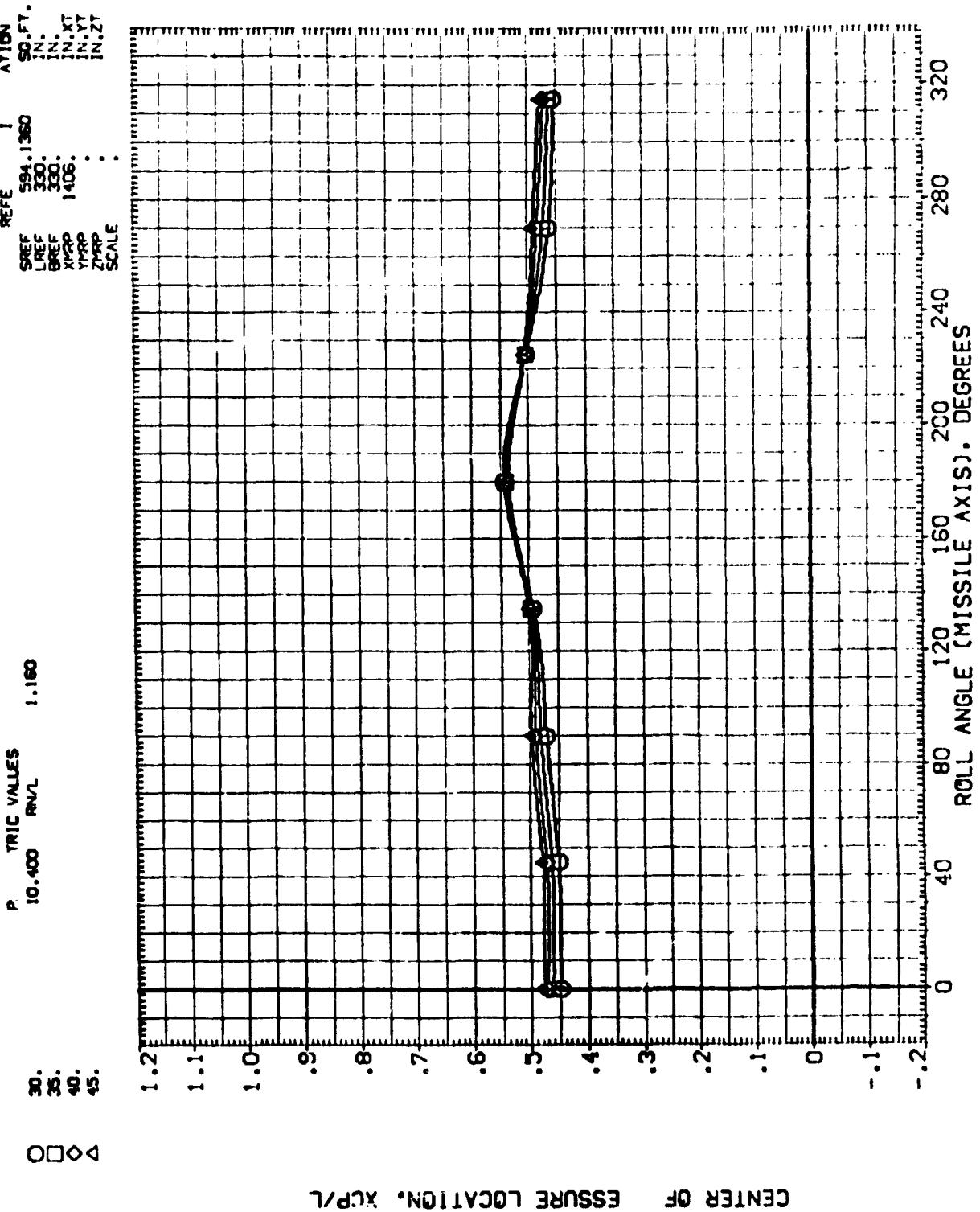
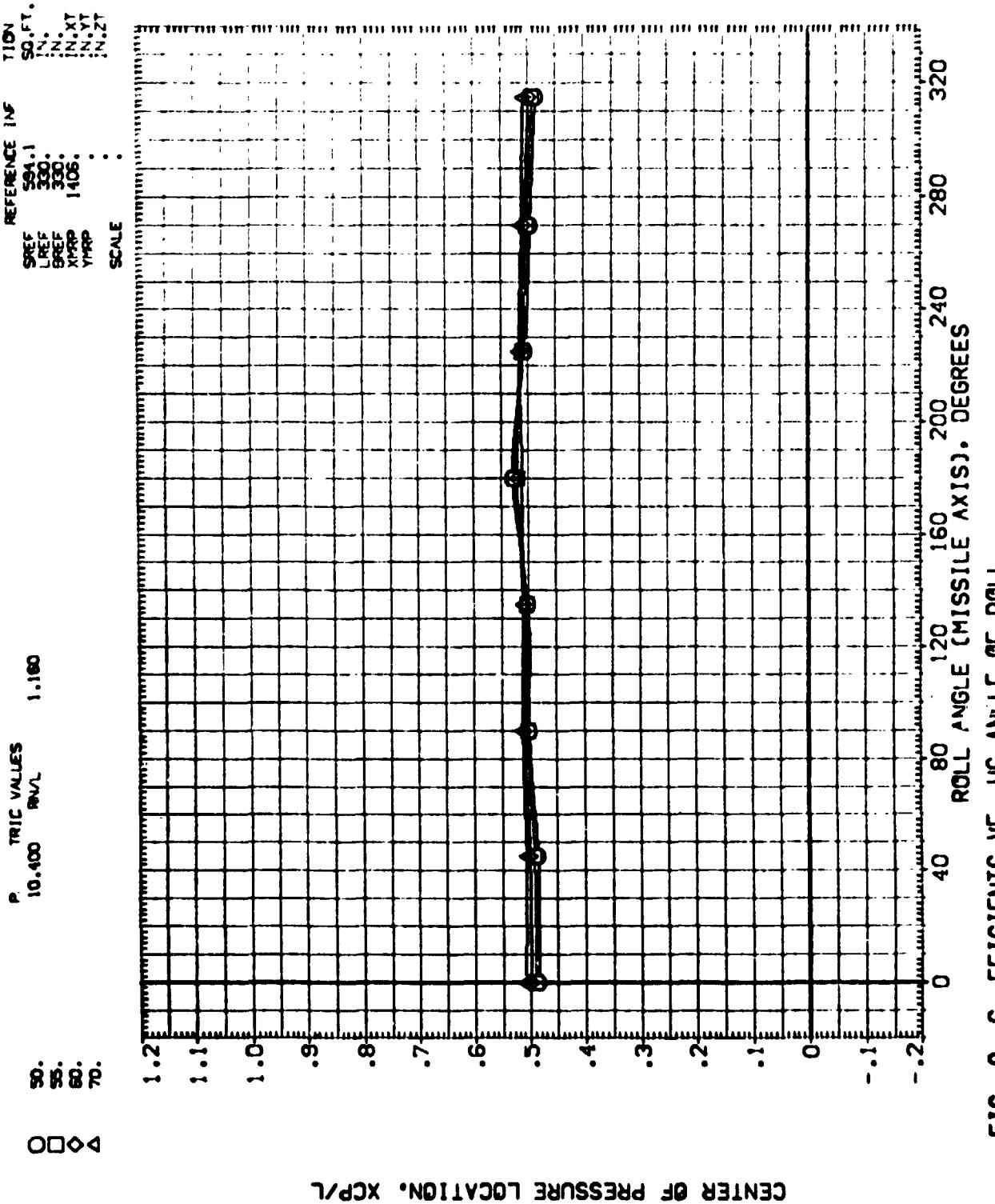


FIG. 9 COEFFICIENTS VERSUS A LE OF ROLL



A 3.5-1 TAGF ET TANK WITH
TUBERANCES (NEYMOI)

10. IC V S 1.100
Fig. 8

OOO△

CENTER ESSURE LOCATION. XCP/L

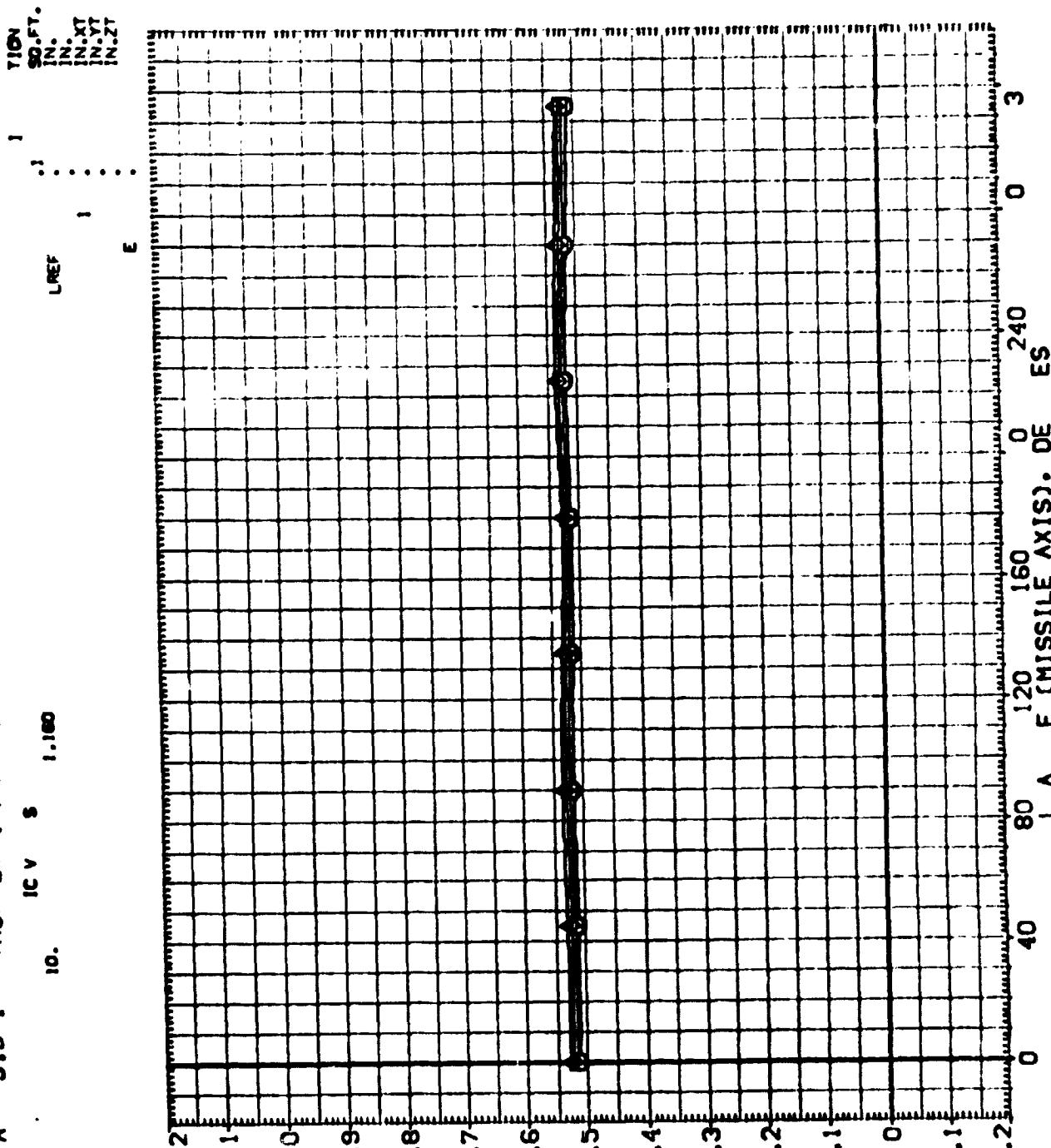


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

PAGE 119

A 3.5-196 TAGF ET (TANK WITH P TURANCES) (NEYMOI)

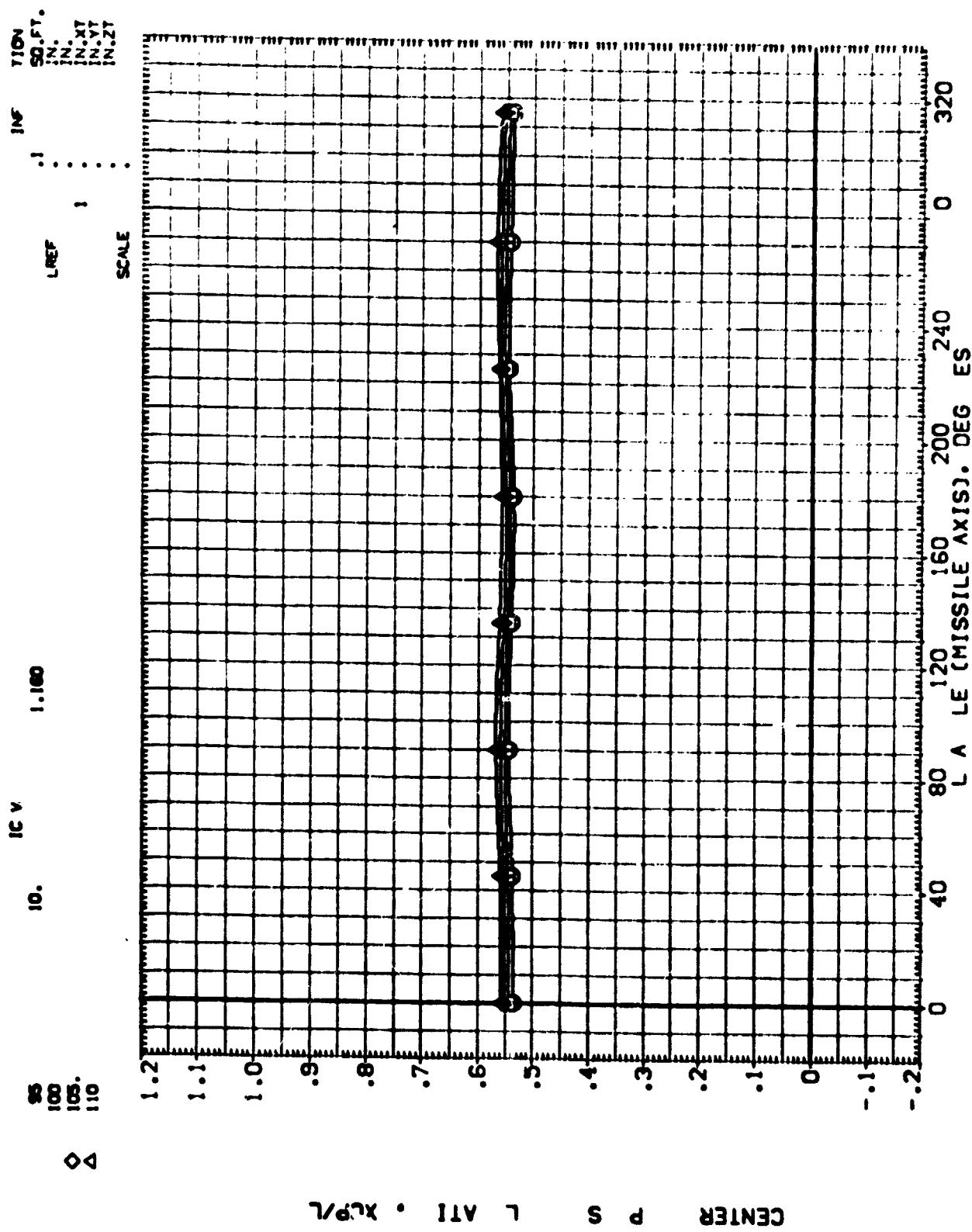


FIG. 9 COEFFICIENTS VS. ANGLE OF LL

PAGE 120

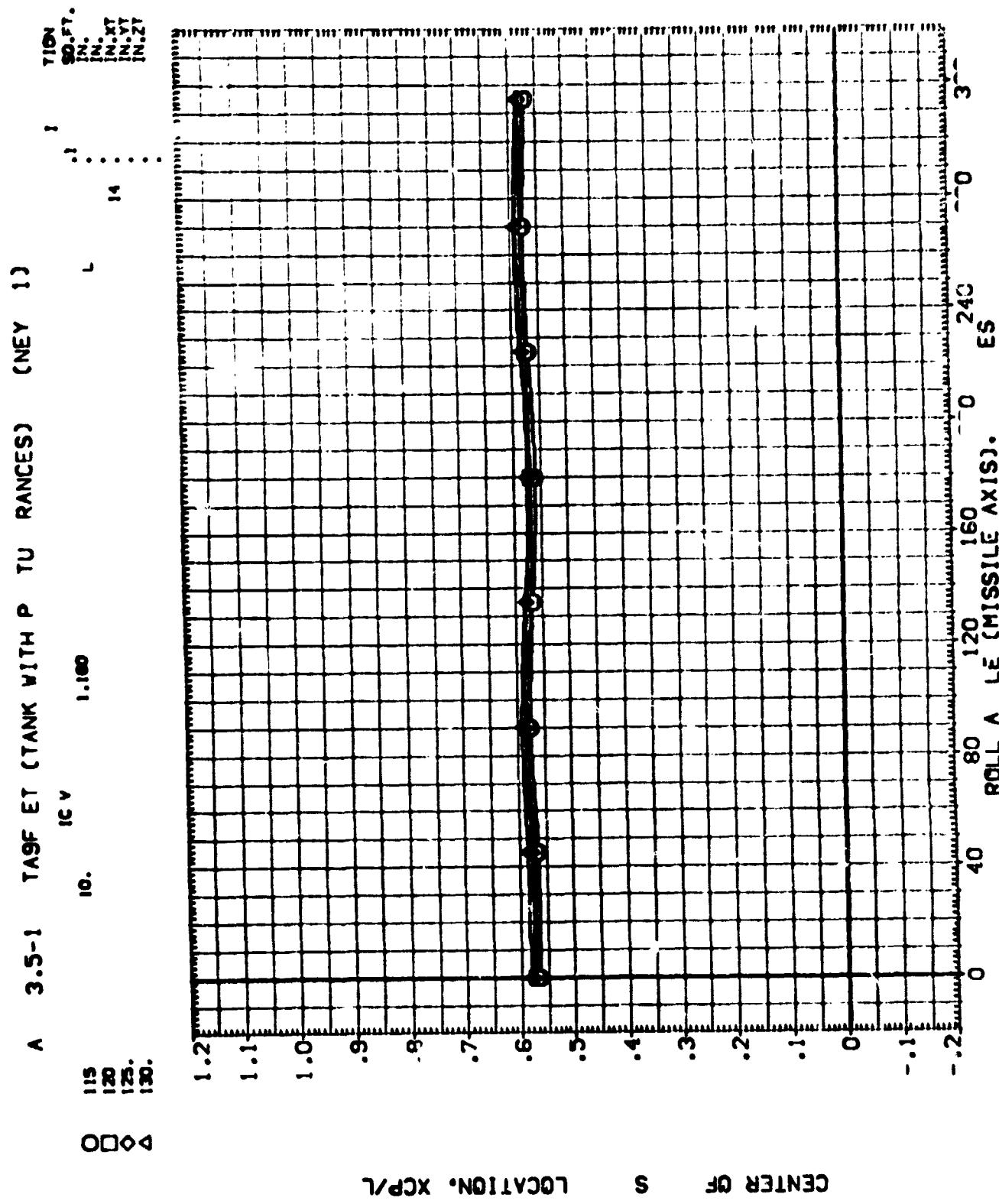


FIG. 3 COEFFICIENTS VS. ANGLE OF ROLL

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ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

PARAMETRIC VALUES
 ALPHA 135.
 140.00 RNL 1.150
 145.00
 150.00

□ ◇ △

REFERENCE INFORMATION
 SREF 594.1360 SQ.FT.
 LREF 300. IN.
 BREF 350. IN.
 XMRP 1406. IN.XT
 YMRP 1406. IN.YT
 ZMRP 1406. IN.ZT
 SCALE

CENTER OF PRESSURE LOCATION, XCP/L

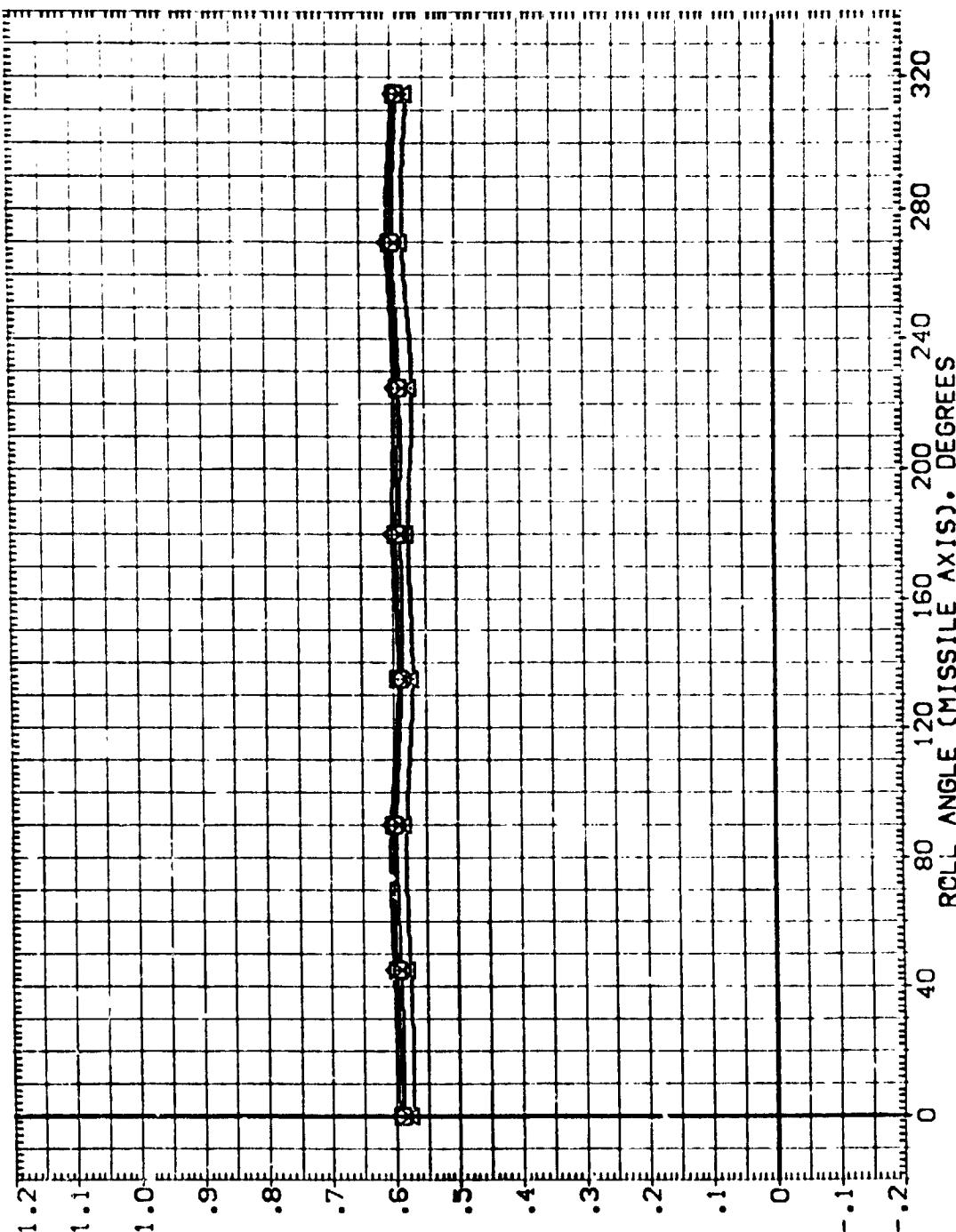
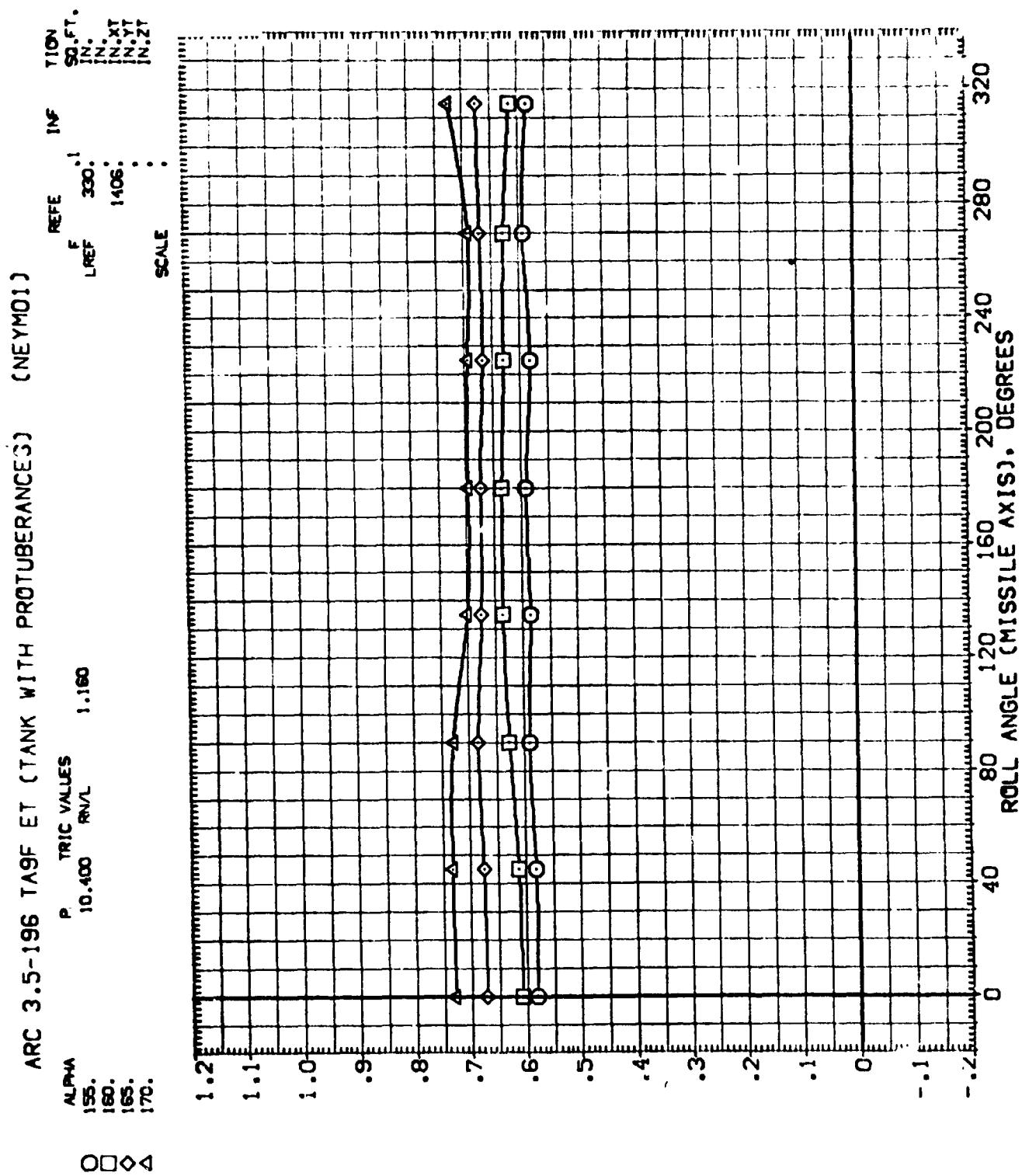


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL



CENTER OF PRESSURE LOCATION, XCP/L

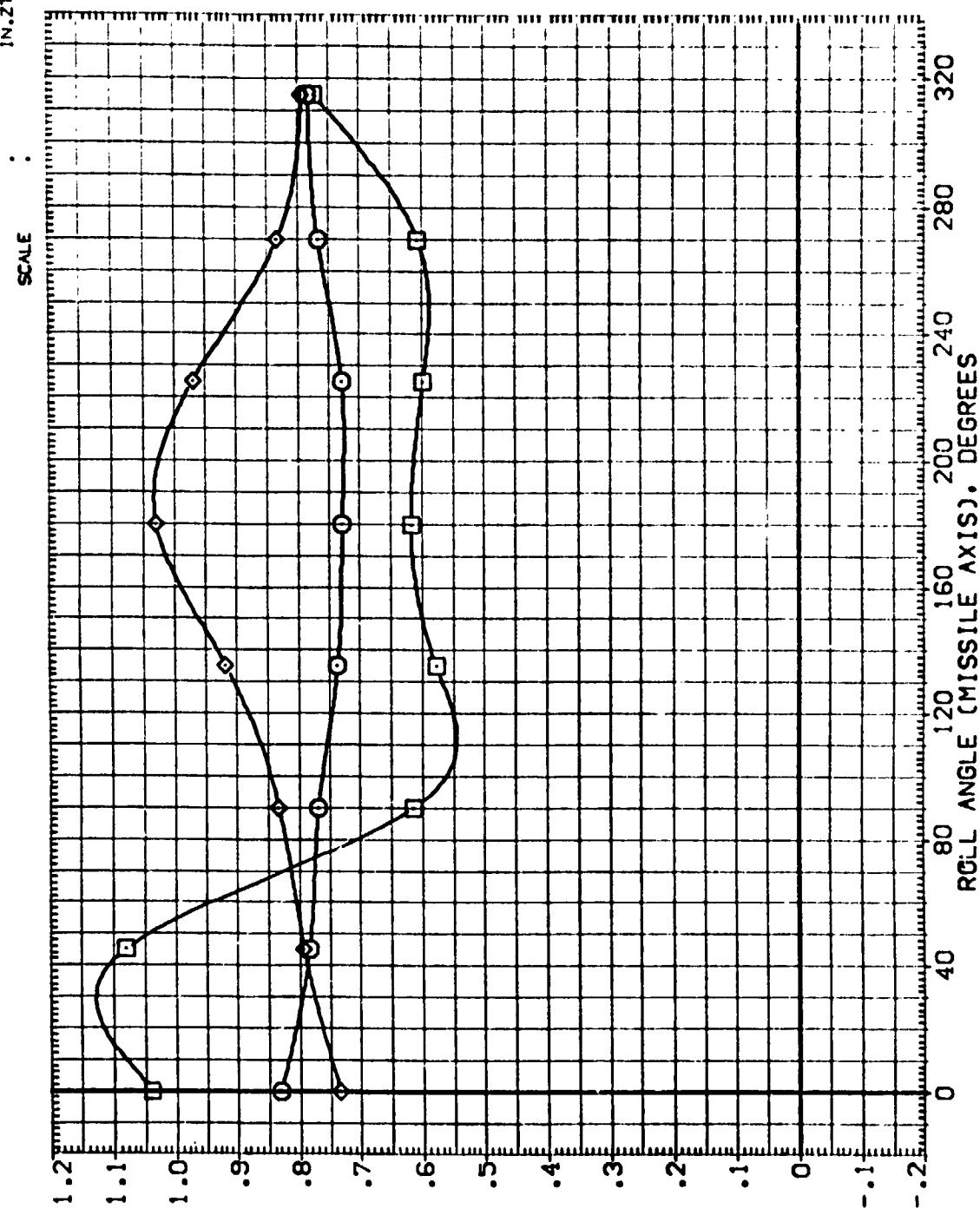
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (NEYMO1)

P_{TRIC V} = 10,400
S = 1.160
175.
160.
165.

TANK
SQ.FT.
594.1360
REF
LREF
BREF
XREF
IN.XT
IN.YT
IN.ZT

REF
LREF
BREF
XREF



CENTER OF PRESSURE LOCATION, DCP/L

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

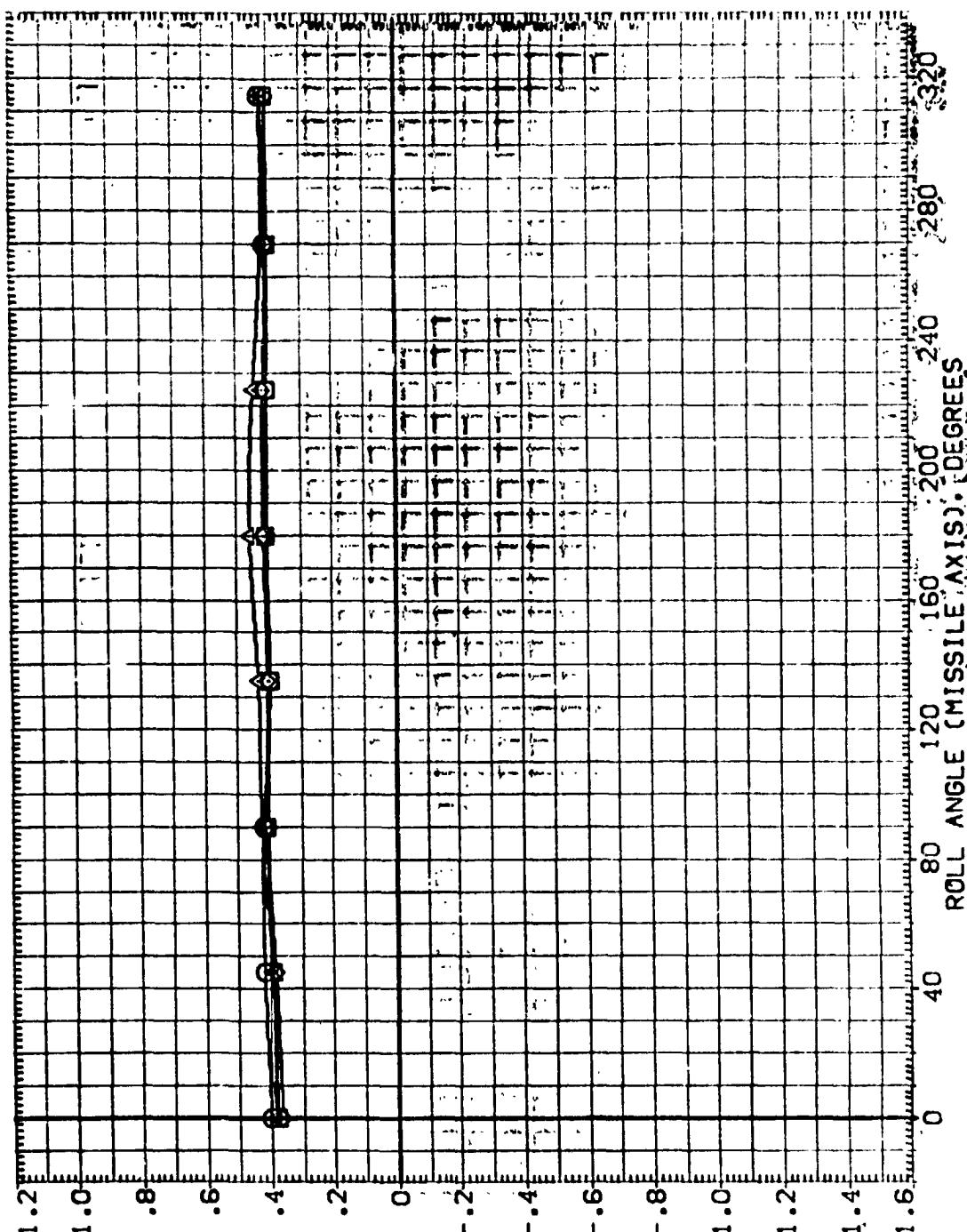
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (PEYMO1)

POLAR COEFFICIENTS
ROLL 10.400 ROLL 1.160

LEAF
REF
XRP
YRP
ZRP

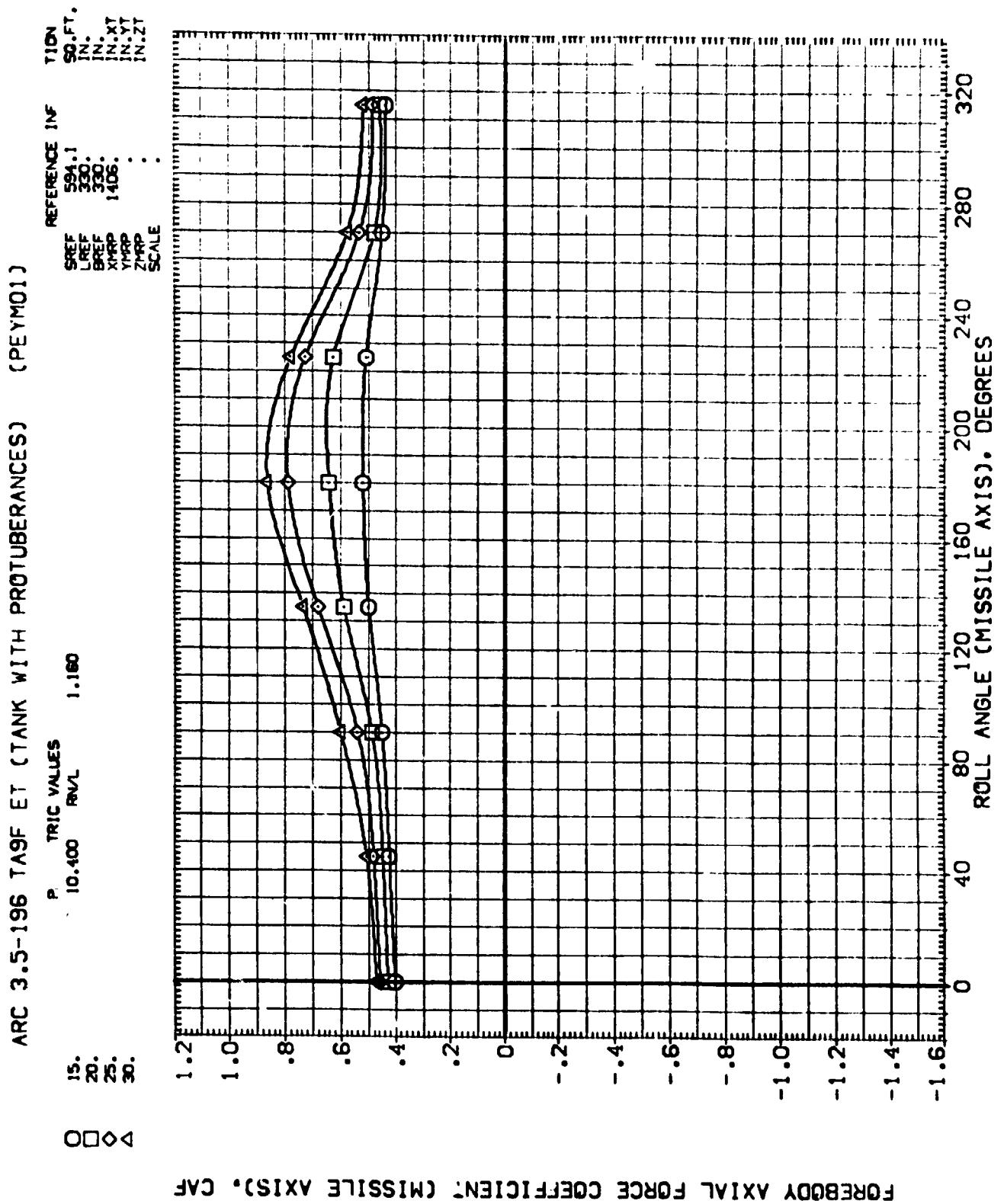
1405

SCALE



FORCEBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAF

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL



FORCEBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAF

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (PEYMOI)

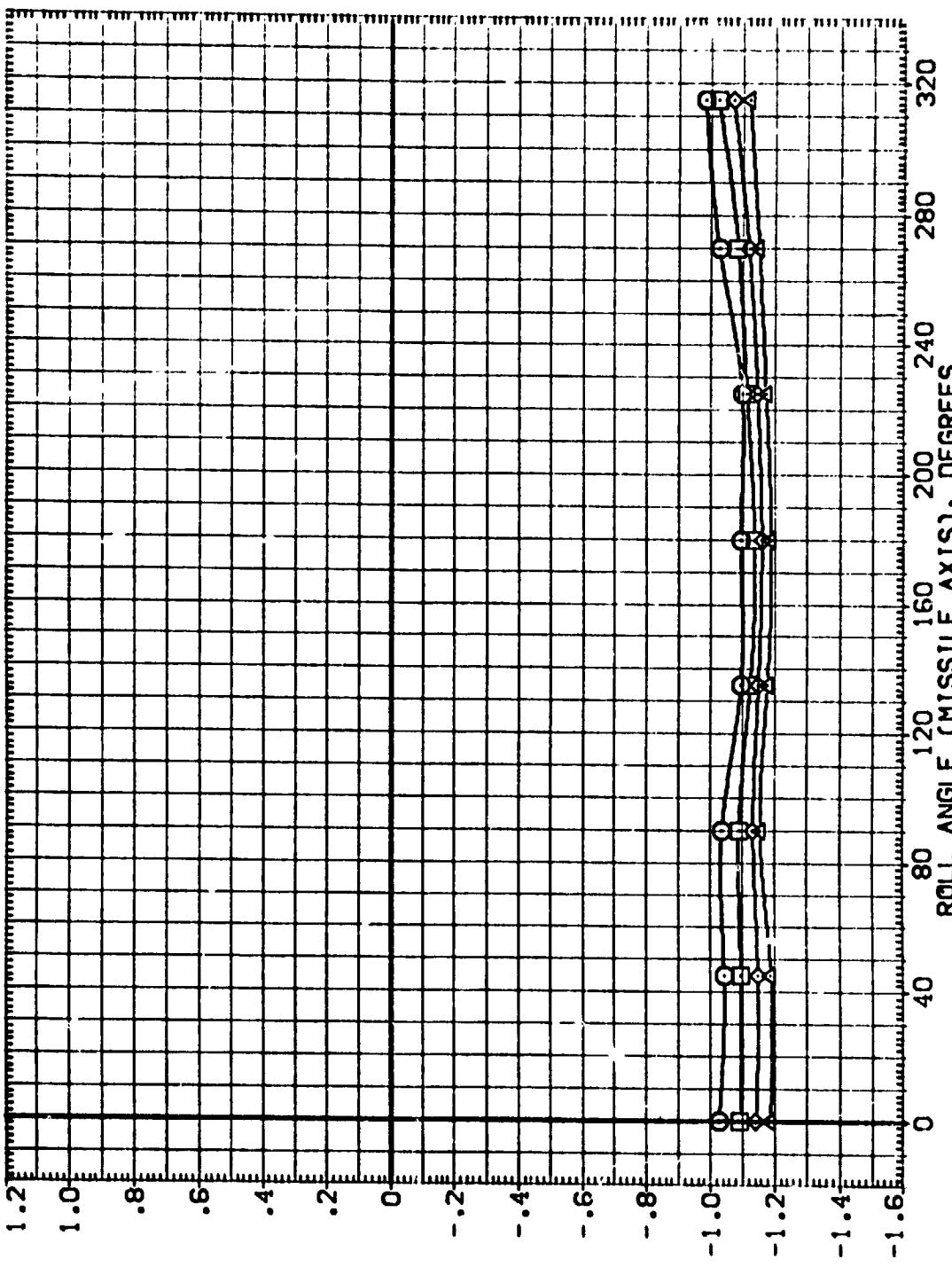


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (PEYMO1)

1.100
1.0.
1.00
1.05.
1.10.
1.15.
1.20.
1.25.
1.30.
1.35.
1.40.
1.45.
1.50.

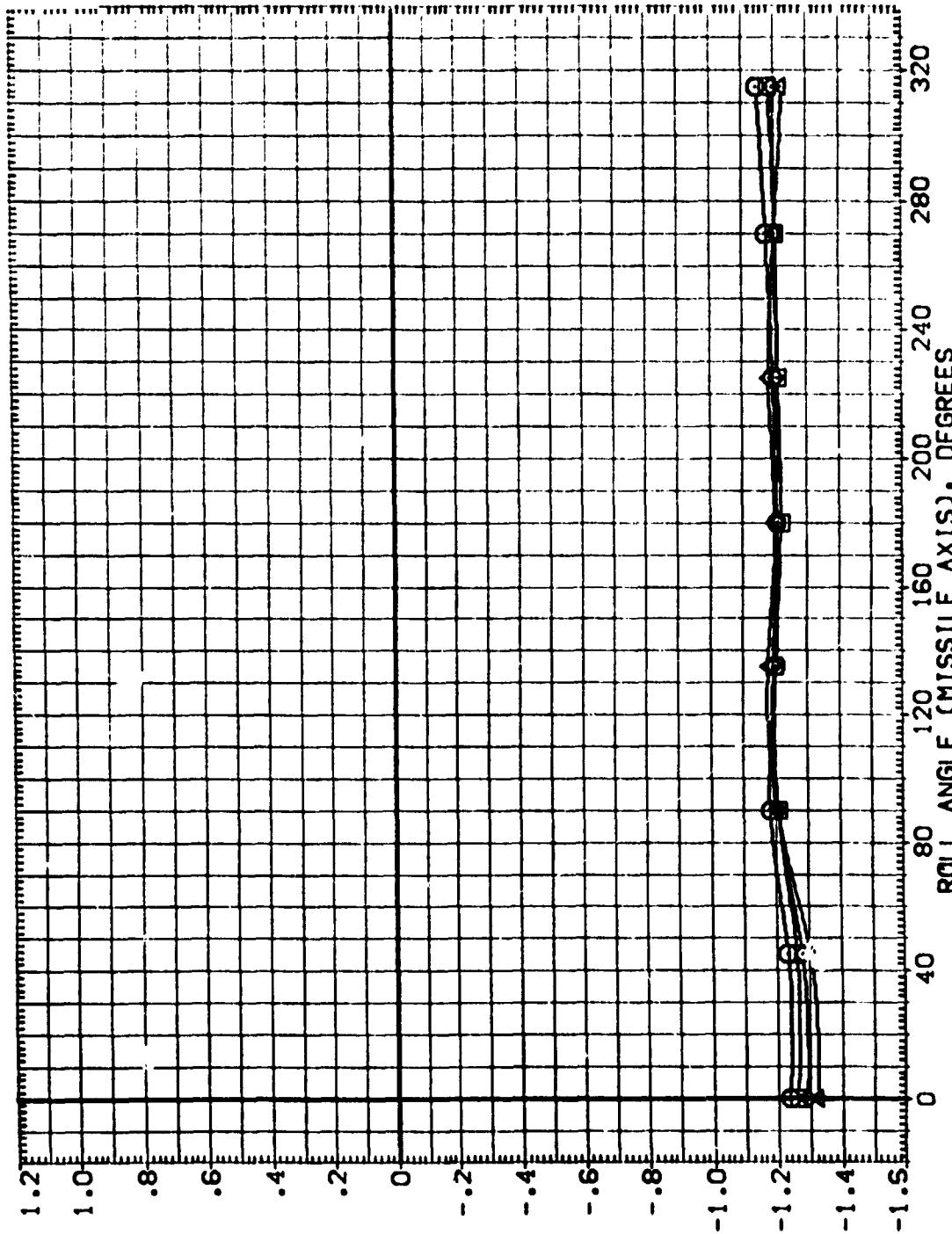


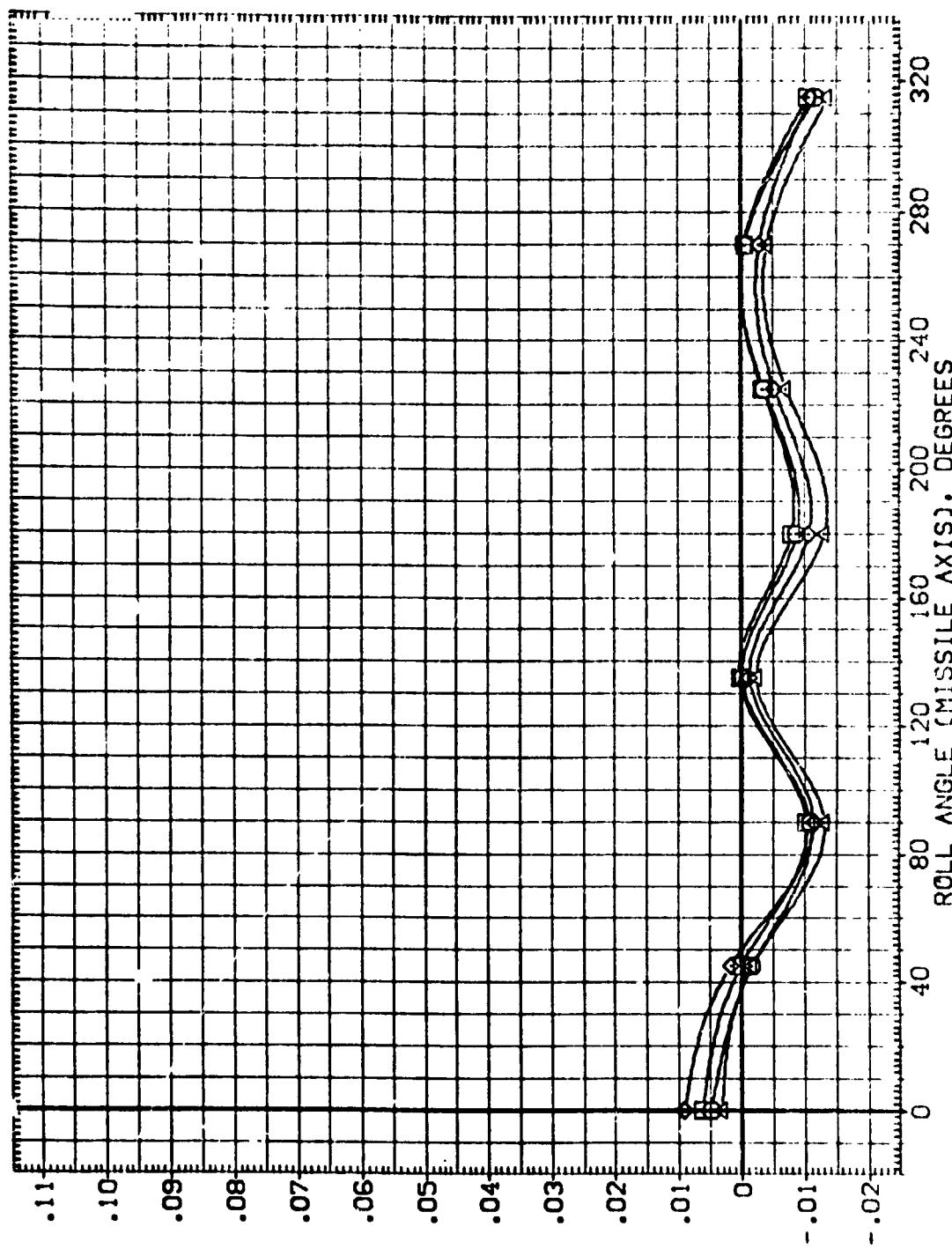
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (PEYMO1)

P₁ TRIC VALUES
MAX 10.400 ROLL 1.160
5.
10.

○ □ ◇ ▲

REFERENCE 1
594.1
IN.
LREF
1406.
IN.XT
IN.YT
IN.ZT
SCALE



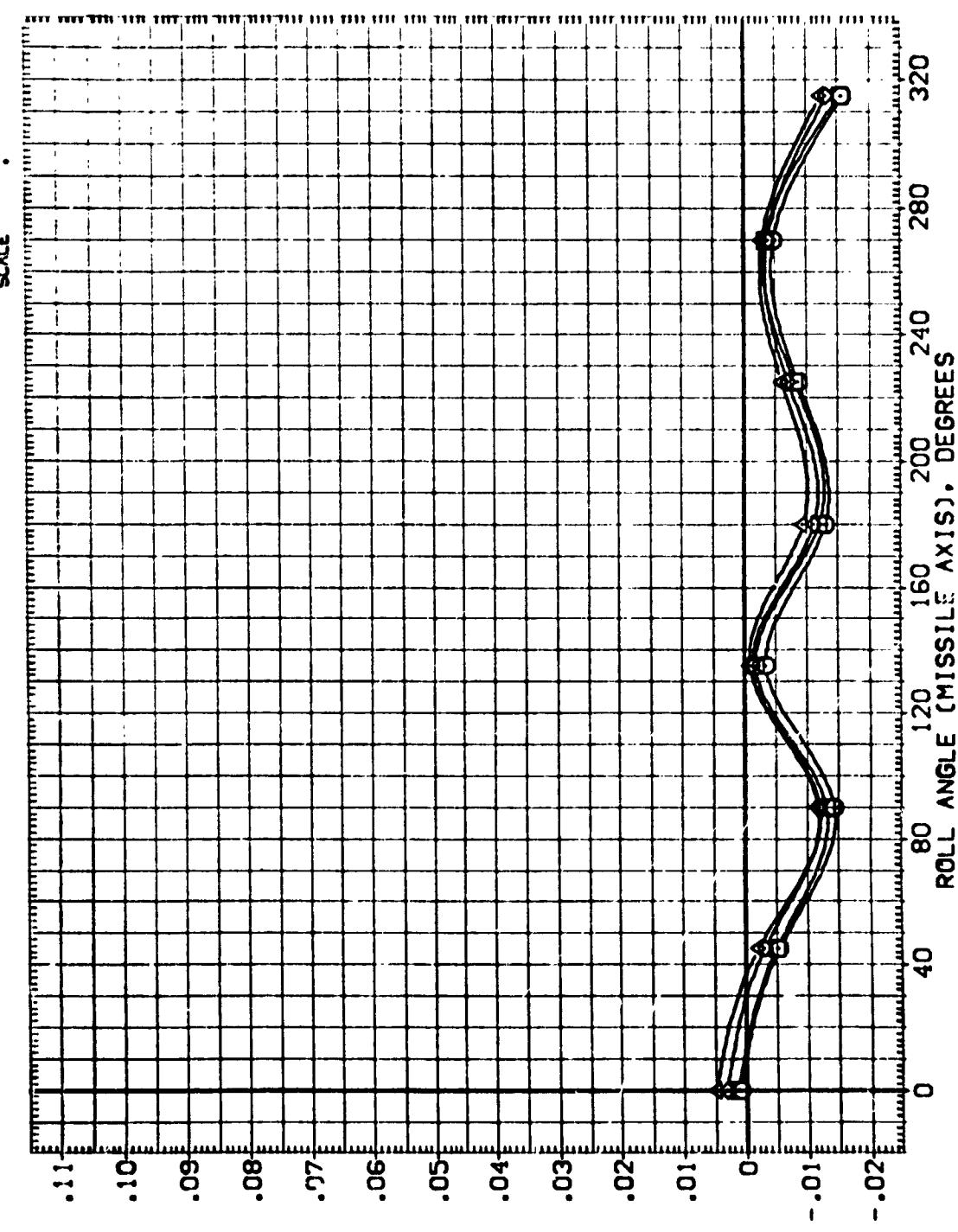
BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS), CAB

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (PEYMO1)

$\Delta \phi_{10}$
15. PA TRIC VALUES 1.160
20.
25.
30.

REFE 594.1
LREF 300.
BREF 146.
IN. IN. IN. IN. IN. IN.
XT YT ZT



BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAB

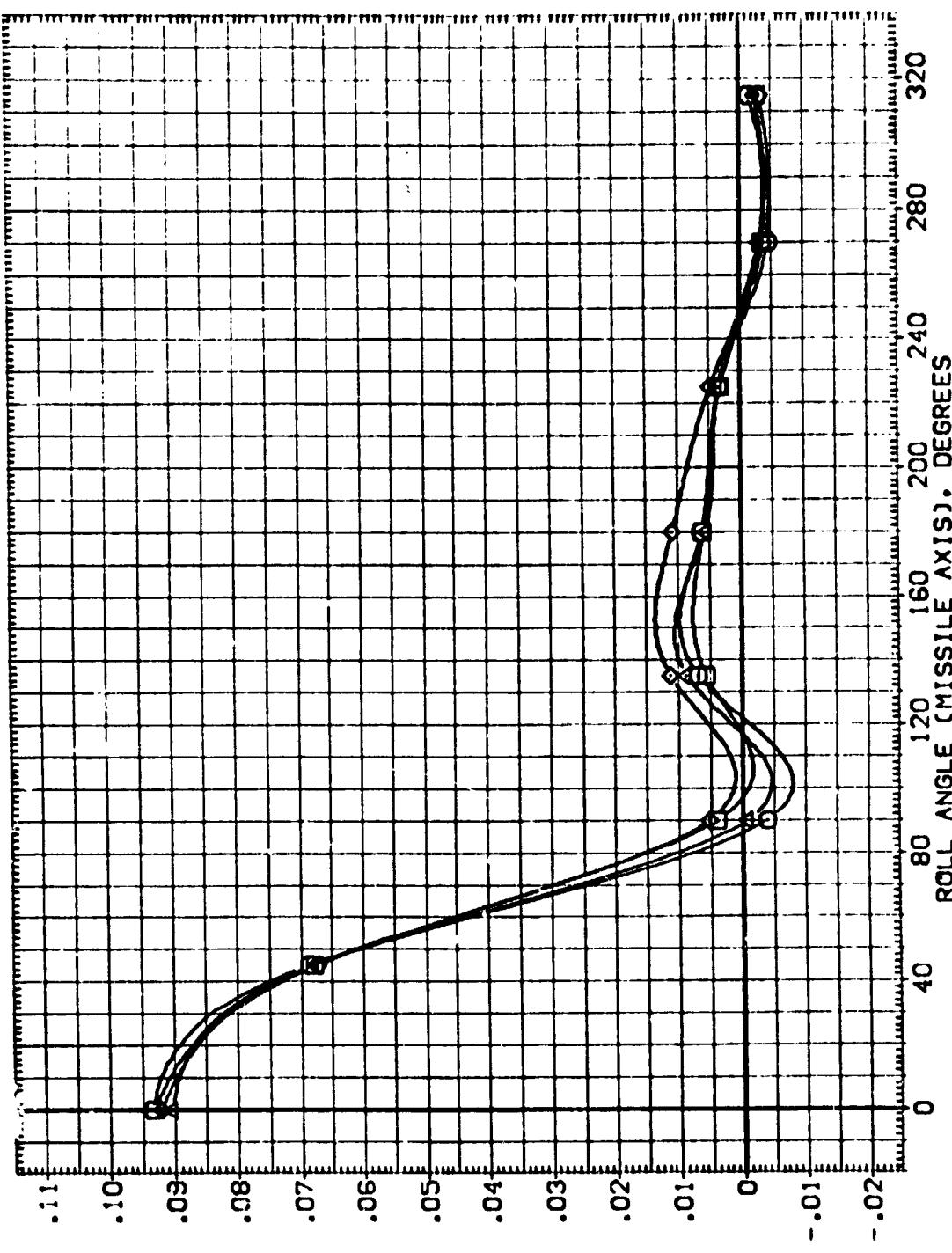
FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

ARC 3.5-196 TAGF ET TANK WITH PROTUBERANCES) (PEYMO1)

ROLL ANGLE (DEGREES)	TRIC VALUES
150.	.10.400
155.	
160.	
165.	

○ □ ◆ △

REFERENCE
SPEED.
REF. 300.
REF. 300.
1465.
YMRP.
SCALE.



BASE AXIAL FORCE COEFFICIENT (MISSILE AXIS), CAB

FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL

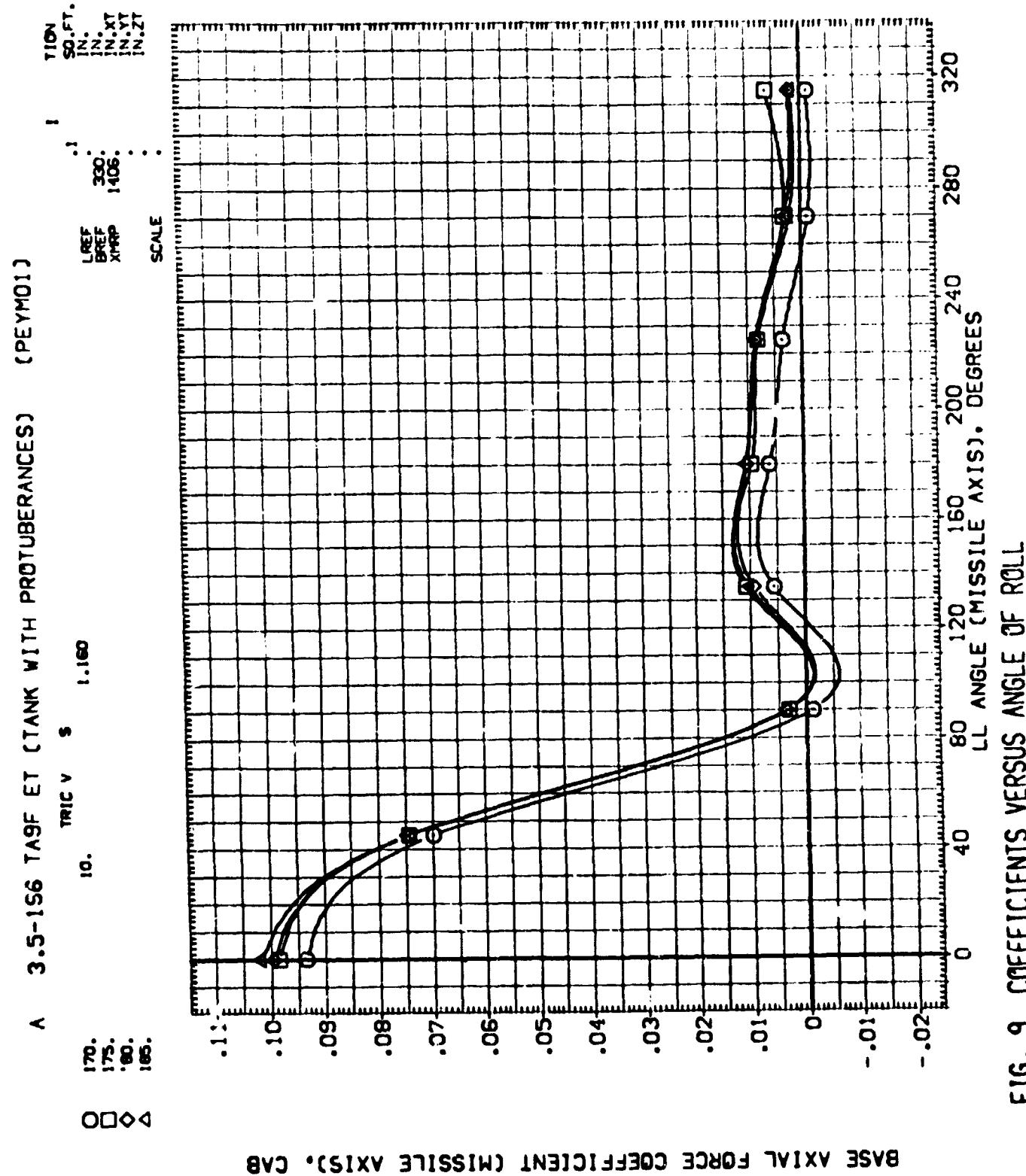
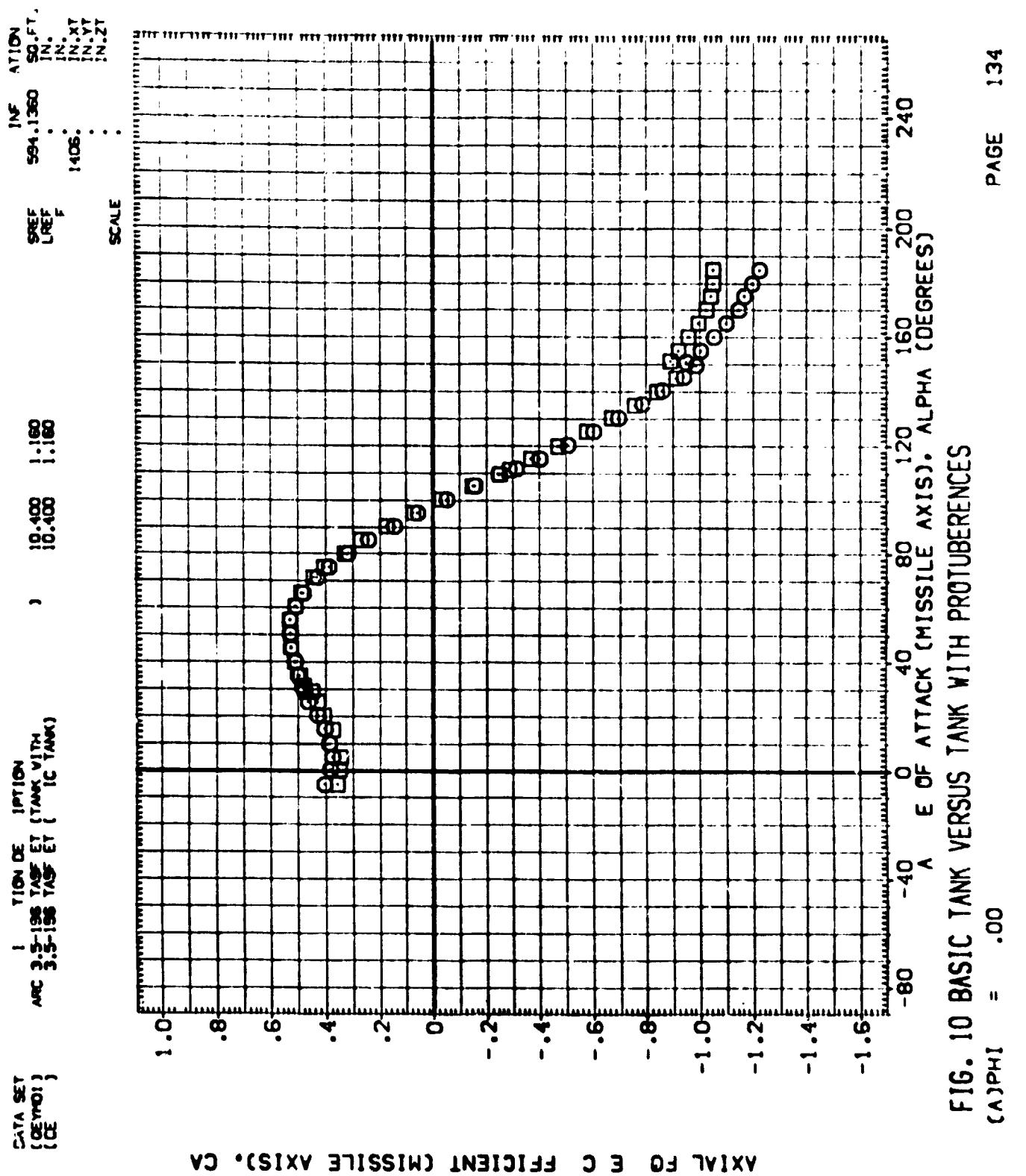
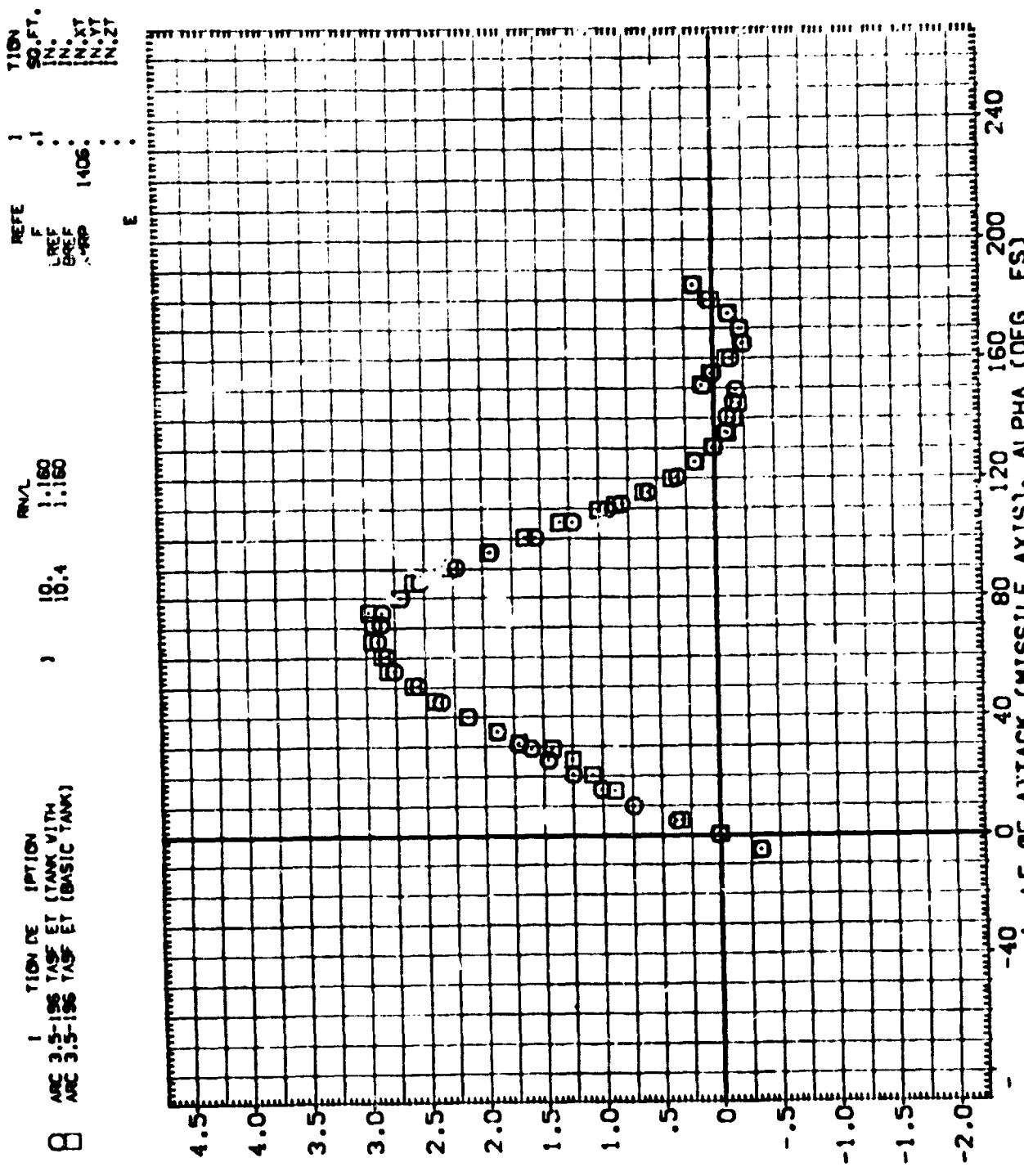


FIG. 9 COEFFICIENTS VERSUS ANGLE OF ROLL



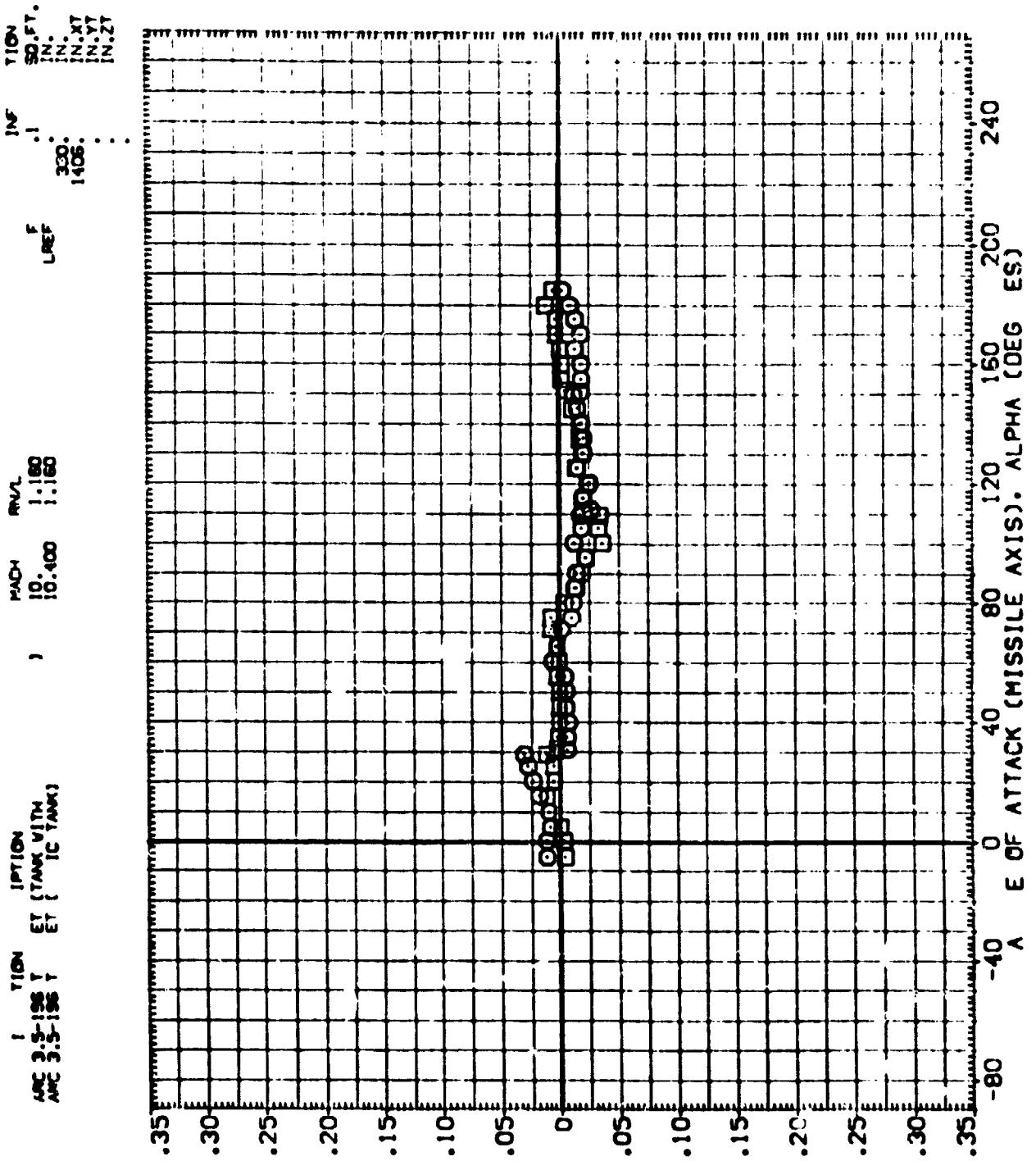
P PADING PAGE BLANK N



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CL

$(\Delta)\Phi_1 = .00$

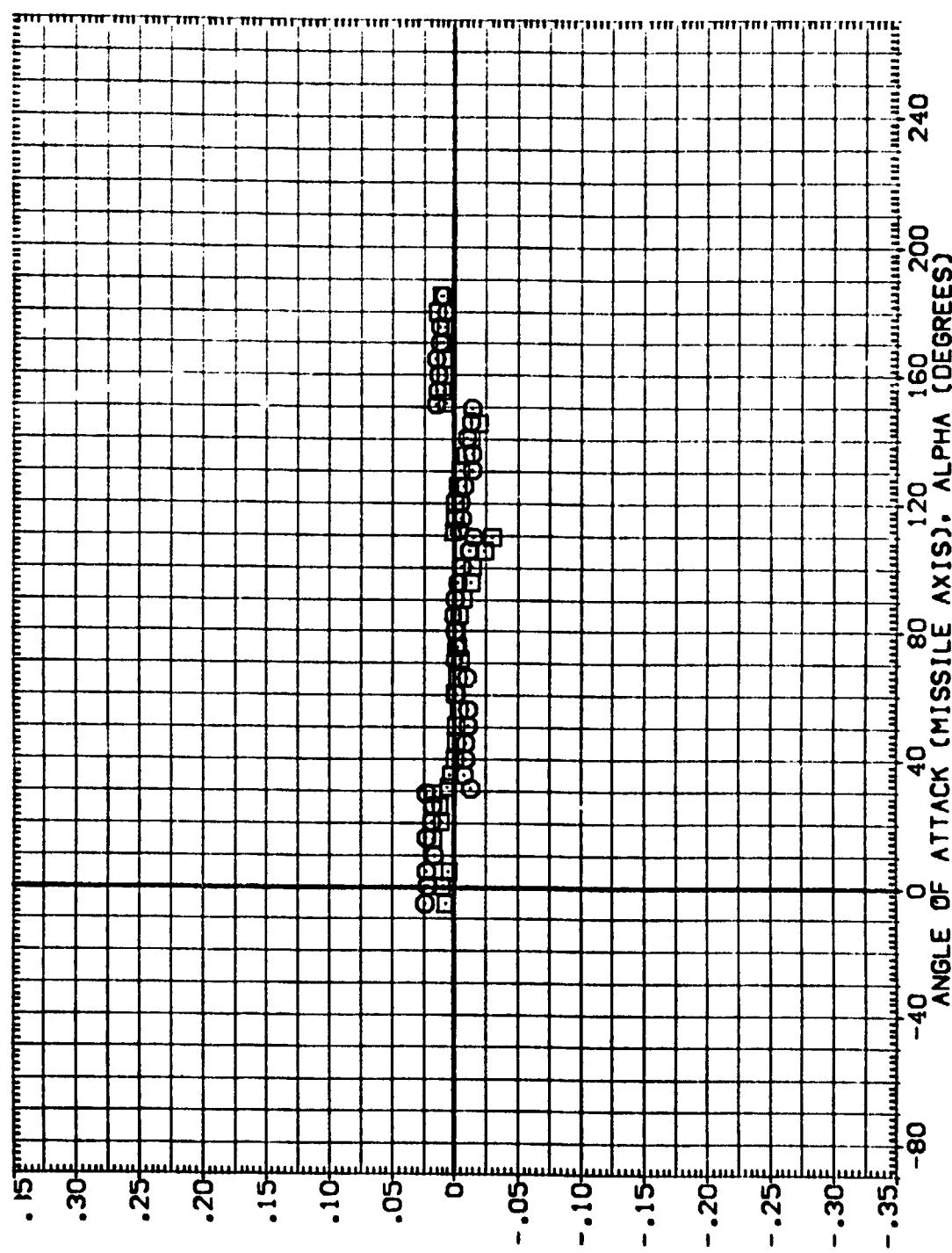
FIG. 10 BASIC TA VERSUS TANK WITH PROTUBERENCES



SIDE-FORCE COEFFICIENT (MISSILE AXIS). CYM

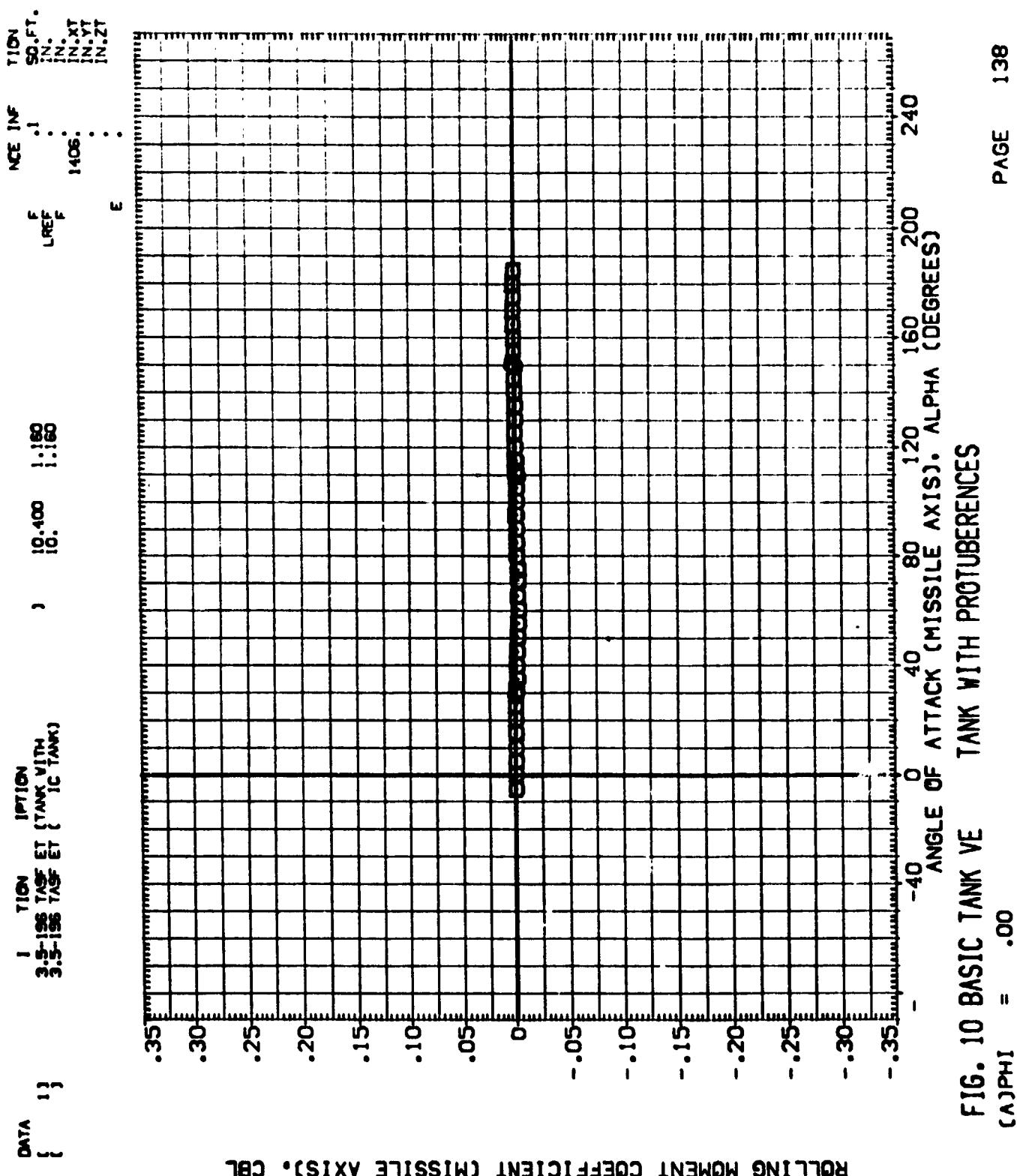
FIG. 10 BASIC TA VE S TANK WITH PROTUBERENCES
 $C_{\text{side}} = .00$

DATA SET 1 TION
 {CE 8 ARC 3.5-196 TASF ET [TANK WITH T S) 10.400 1.180 RNL
 {CE 3.5-196 TASF ET [BASIC TANK] T S) 10.400 1.180 RNL
 REFERENCE 504.1 INF
 LREF 300. IN.
 BREF 300. IN.
 1405. IN.XT
 1405. IN.YT
 1405. IN.ZT



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERENCES
 $(\Delta\phi)_I = .00$



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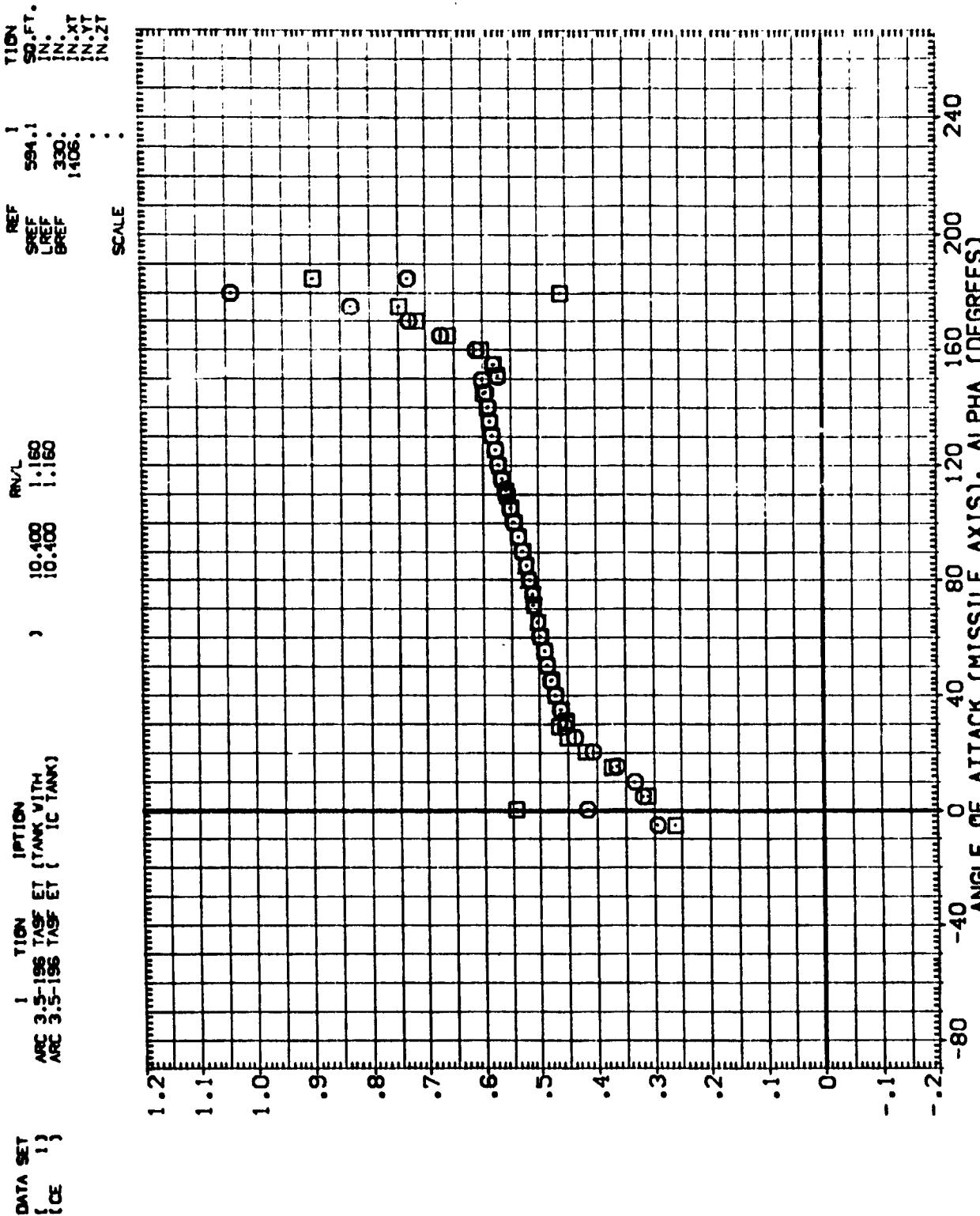


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERENCES
(A)PHI = .00

DATA { 1 } 3.5 IN. TANK WITH PROTUBERANCES
IN. FT.
IN.
IN.XT
IN.YT
IN.ZT

10: 1.169
10: 1.162

1.2
1.0
.8
.6
.4
.2
0
-.2
-.4
-.6
-.8
-1.0
-1.2
-1.4
-1.6

{ 1 }
1406.

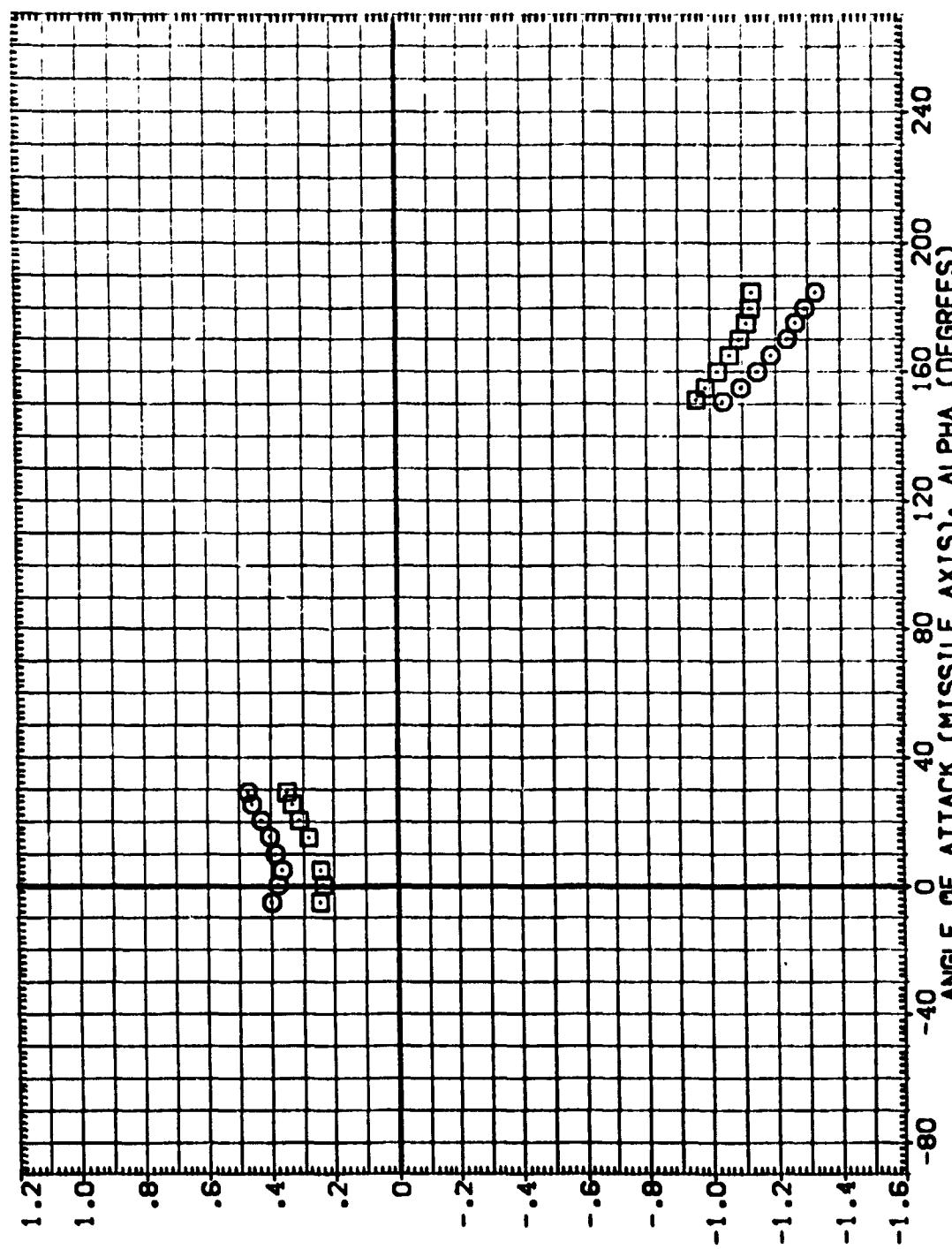
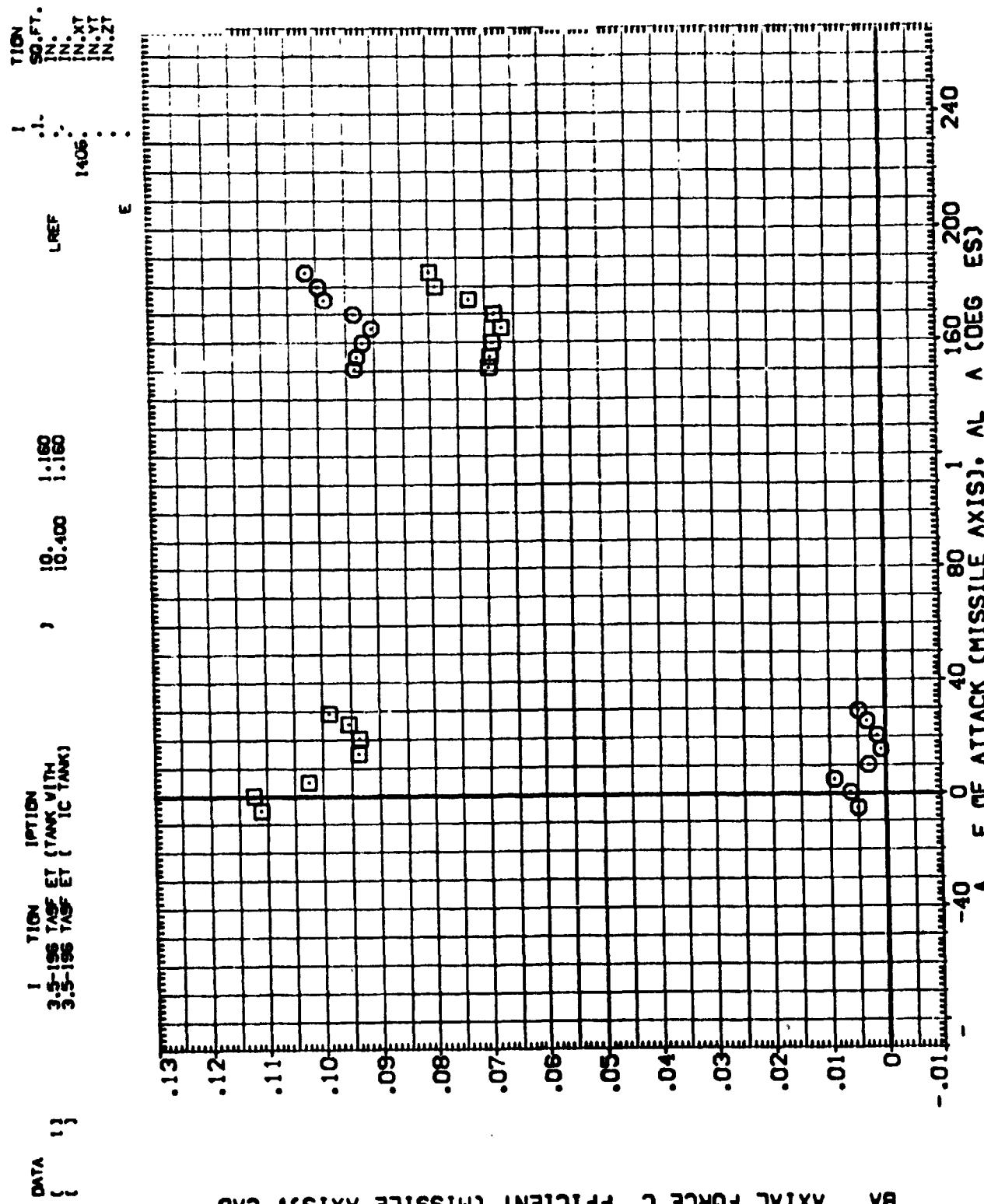


FIG. 10 BASIC TANK VE US TANK WITH PROTUBERANCES

CAPHI = .00

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BA AXIAL FORCE C EFFICIENT (MISSILE AXIS), CA8

FIG. 10 BASIC TA VE US TANK WITH P TUBERENCES
 $\alpha_{\text{PHI}} = .00$

ARC 3.5-1 TAGF ET (TANK WITH PROTUBERANCES) (LEYMO1)

PHI 10. IC V 1.160 LREF 1405. SCALE .1 TION SQ.FT.
 .1 IN. IN. XT IN. YT IN. ZT
 .25 .30 .20 .15 .10 .05 .0 .-05 .-10 .-15 .-20 .-25 .-30 .-35 .-40
 O

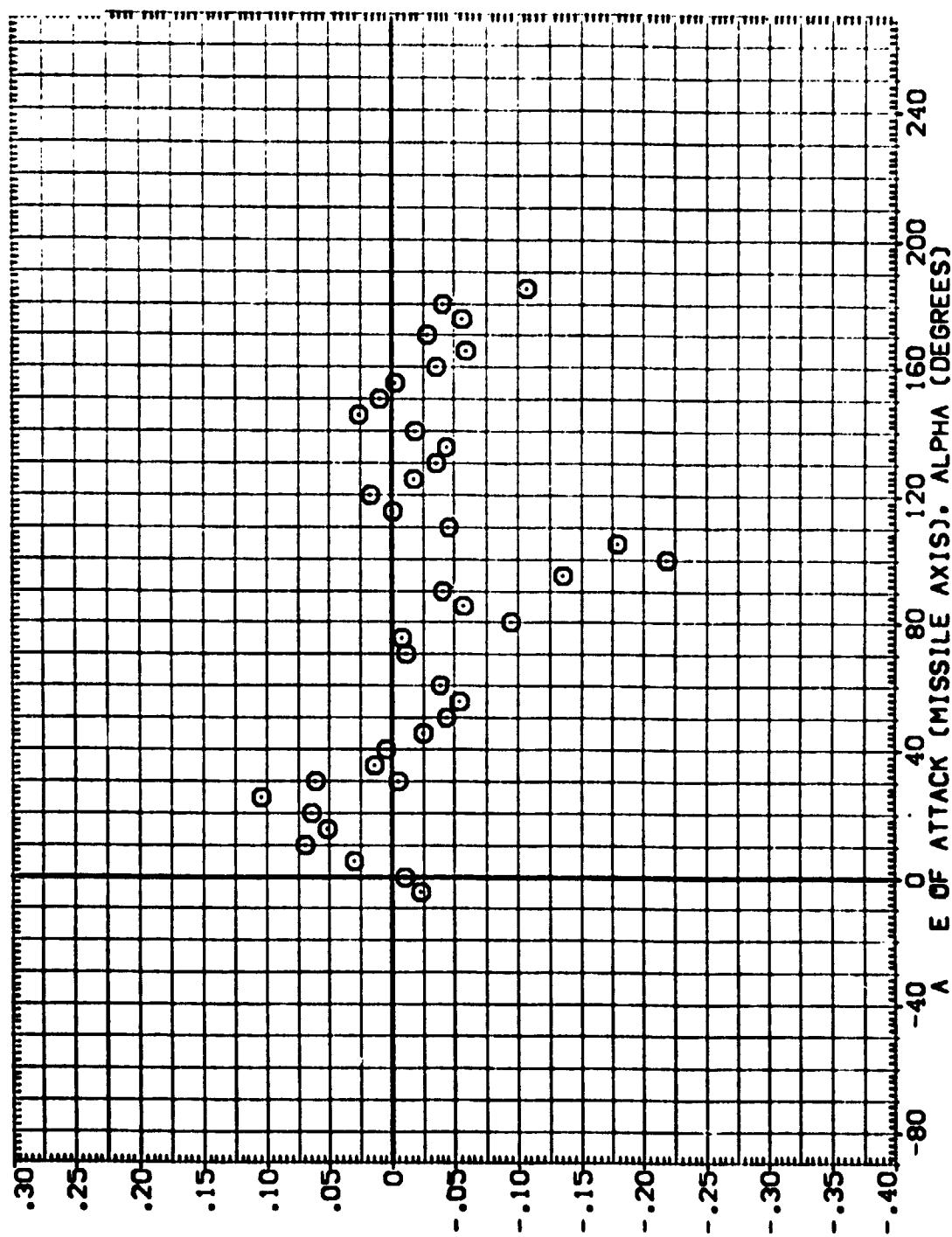


FIG. 10 BASIC TA VERSUS TA WITH PROTURBANCES

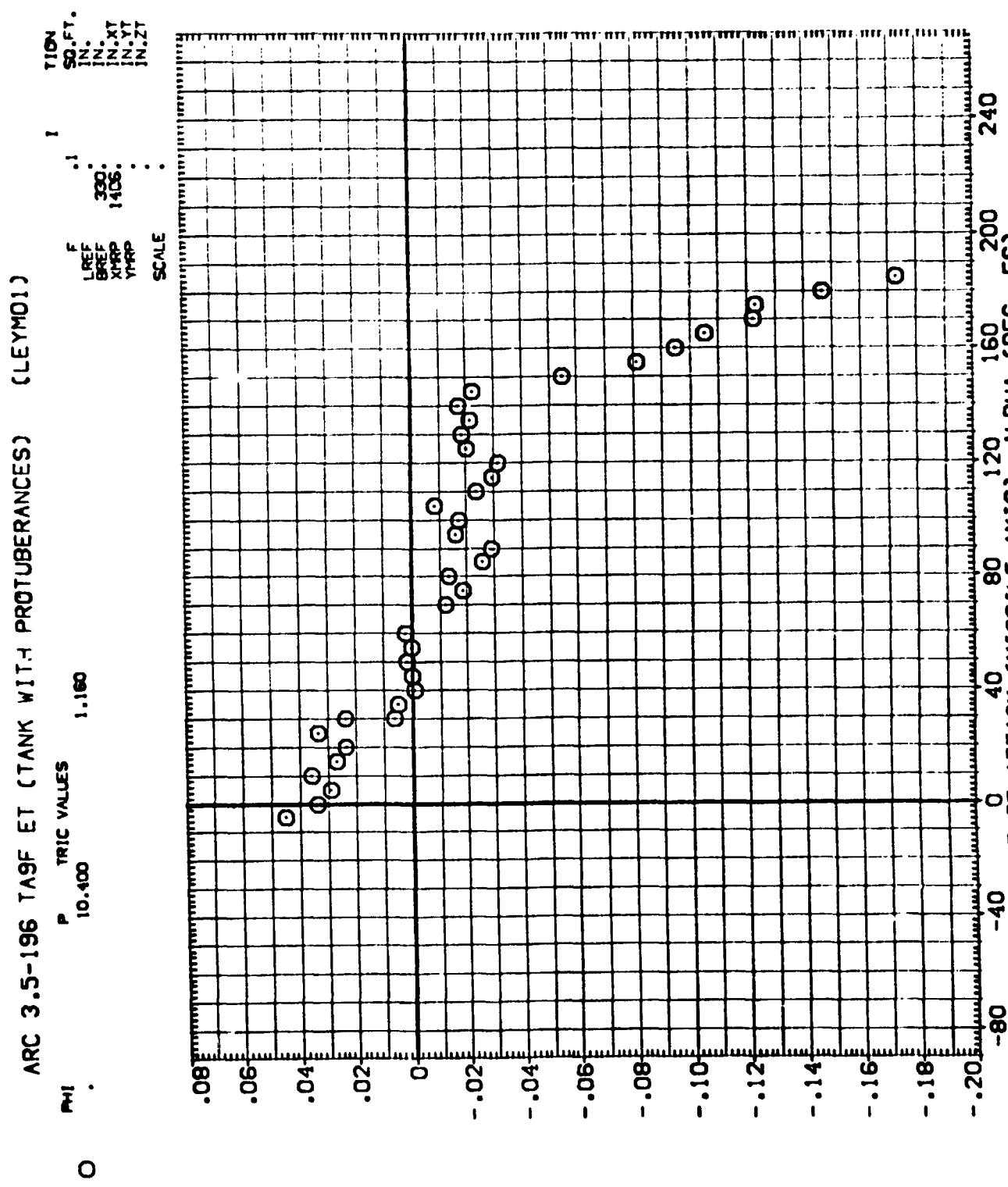
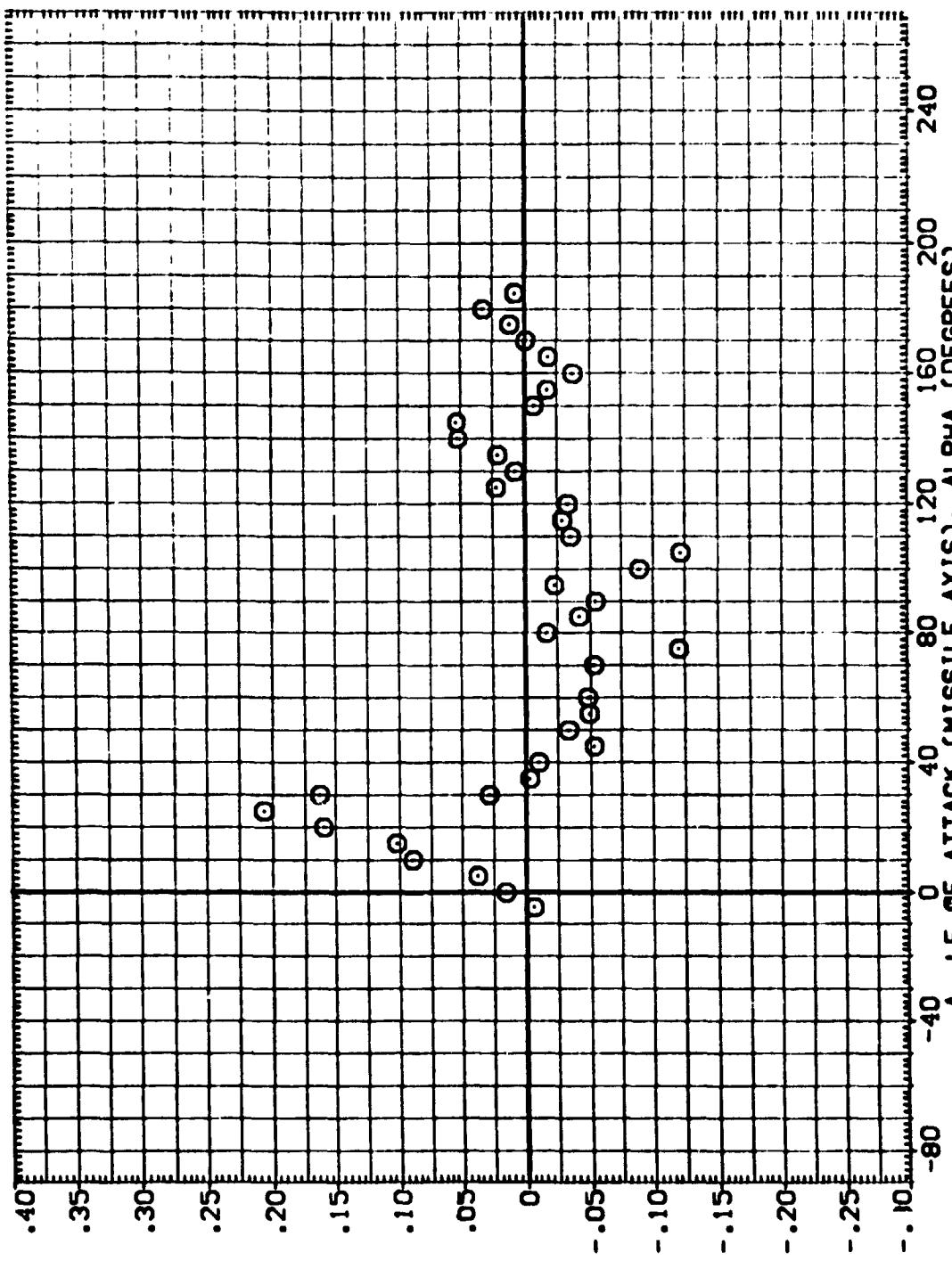


FIG. 10 BASIC TANK VE US TANK WITH PROTUBERANCES

ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (LEYMO1)

TRIC V 10.400 1.180
LREF 330.
BREF 1106.
IN. 1.106.
IN. XT
IN. YT
IN. ZT
SCALE



INCREMENTAL PITCHING MOMENT COEFFICIENT (MILLIGE AXIS). LMM

FIG. 10 BASIC TANK VS TANK WITH PROTUBERANCES

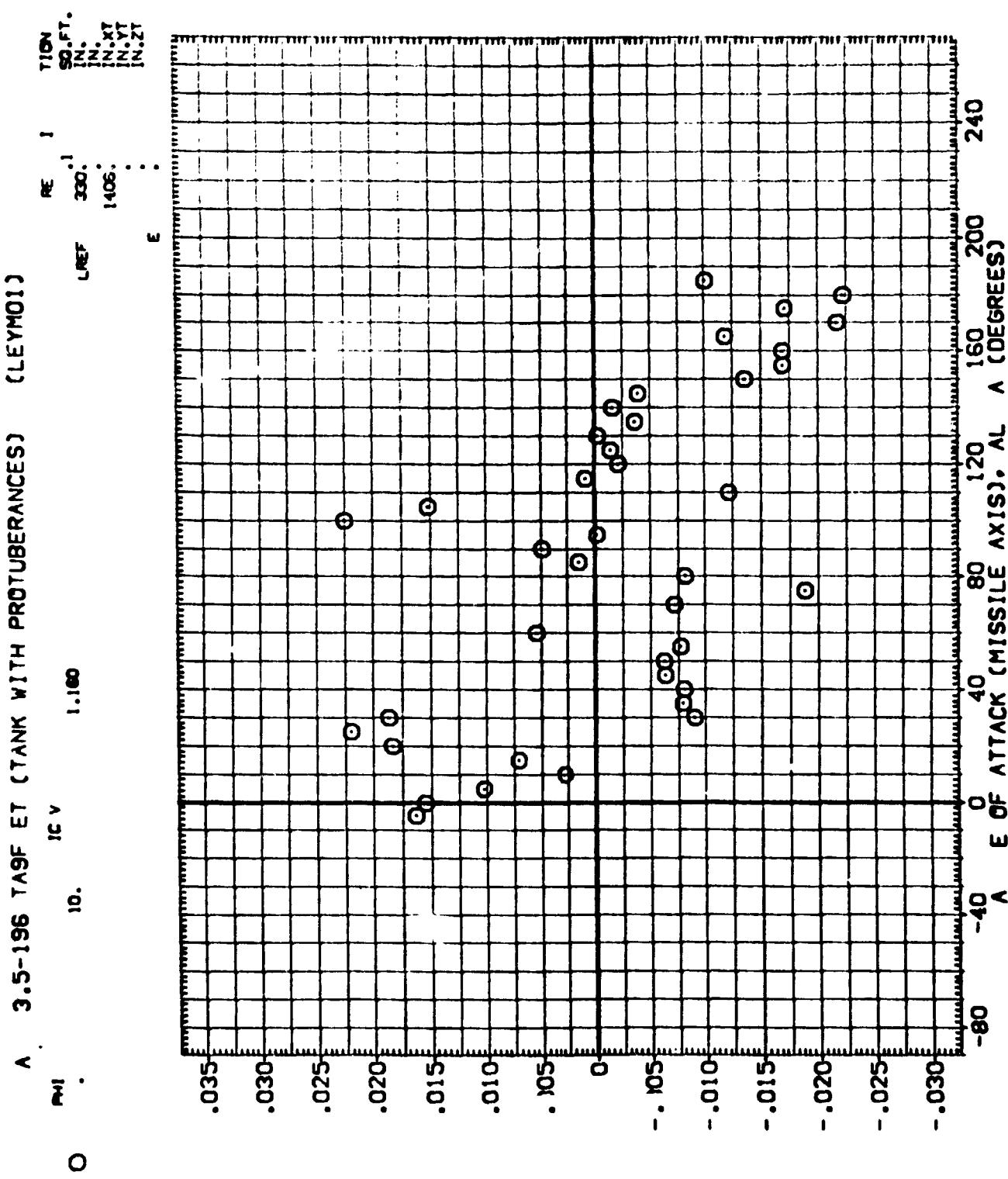
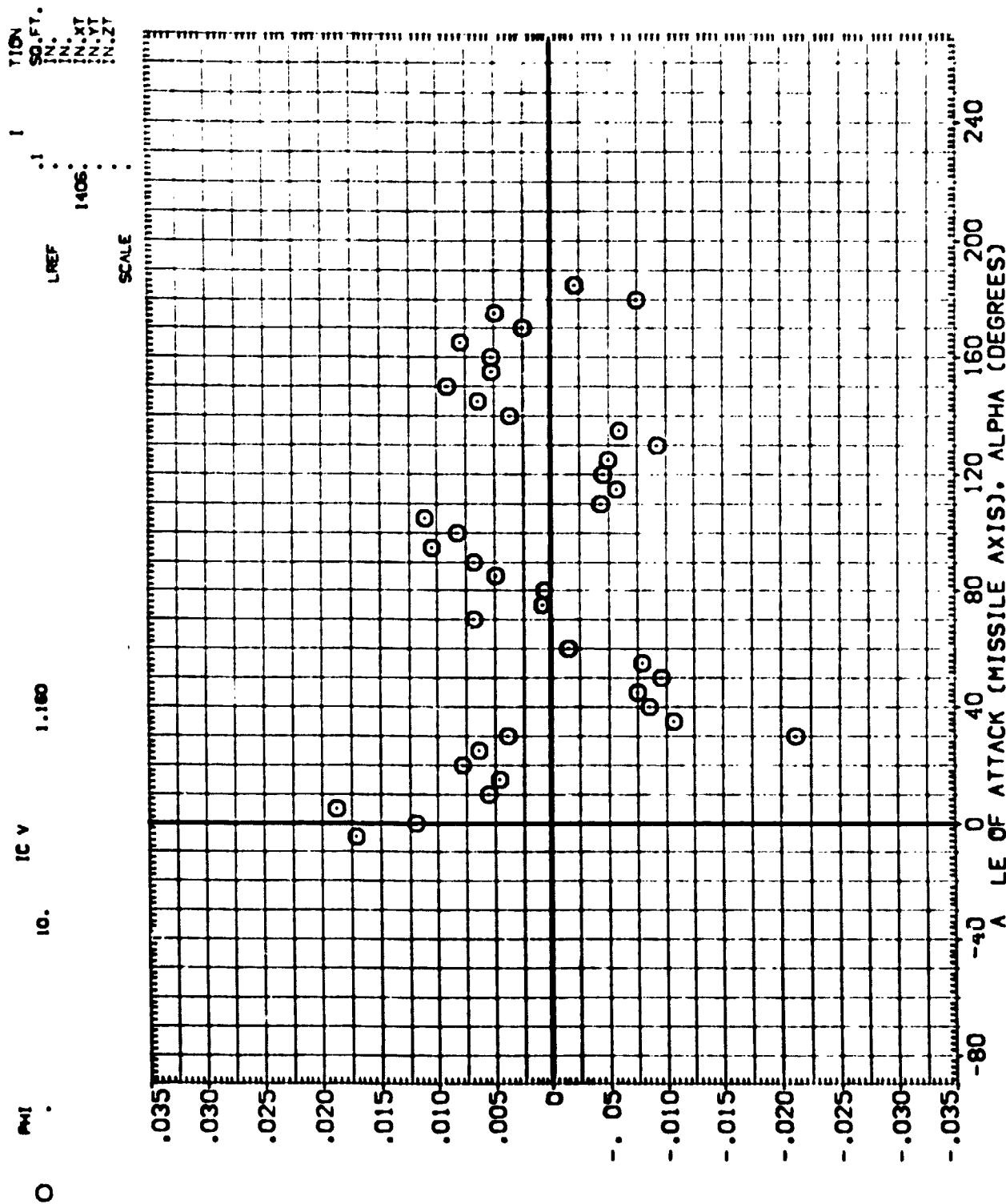


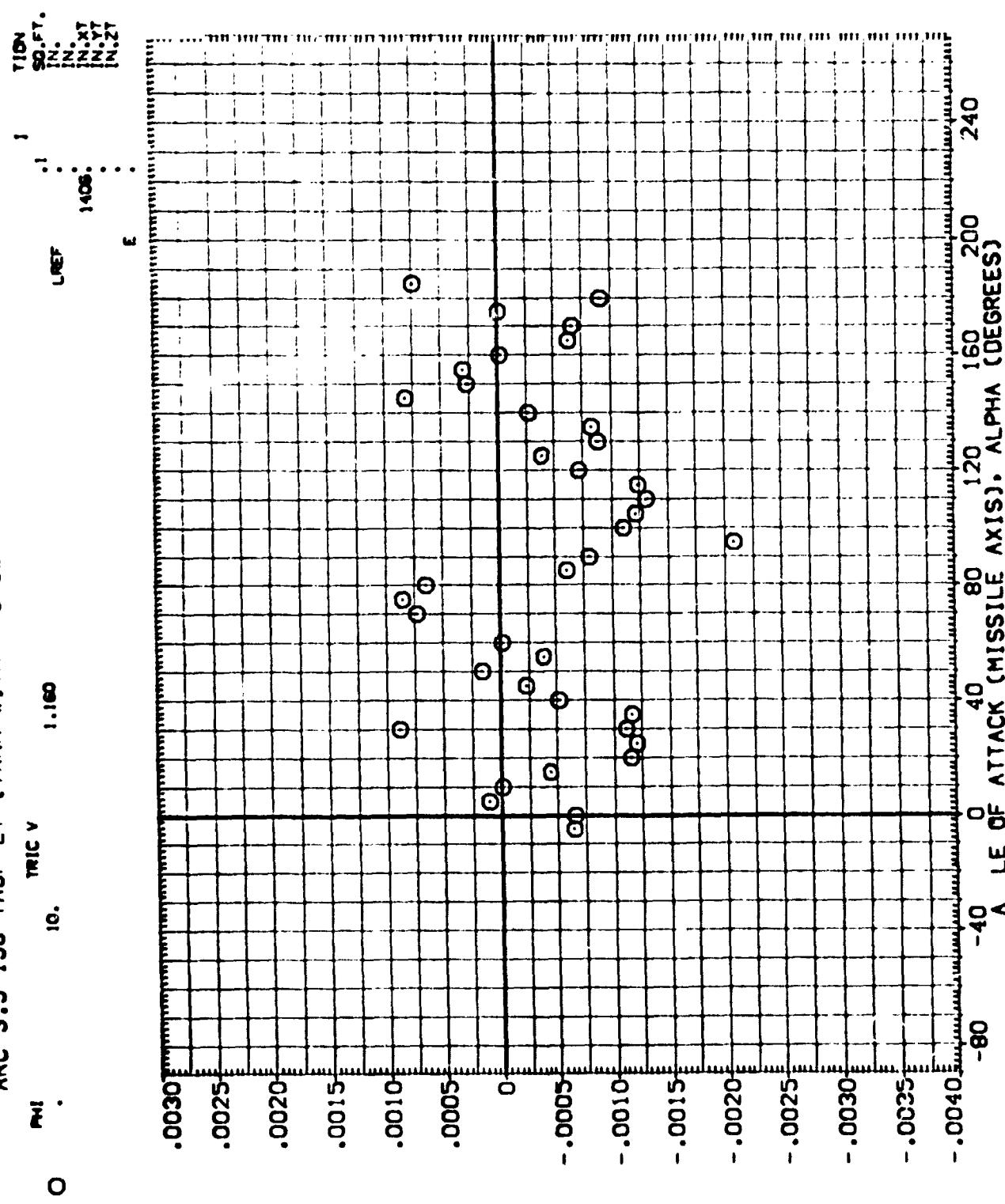
FIG. 10 BASIC TANK WITH PROTUBERANCES

ARC 3.5-196 TAGF ET (TANK WITH P TUBERANCES) (LEYMOI)



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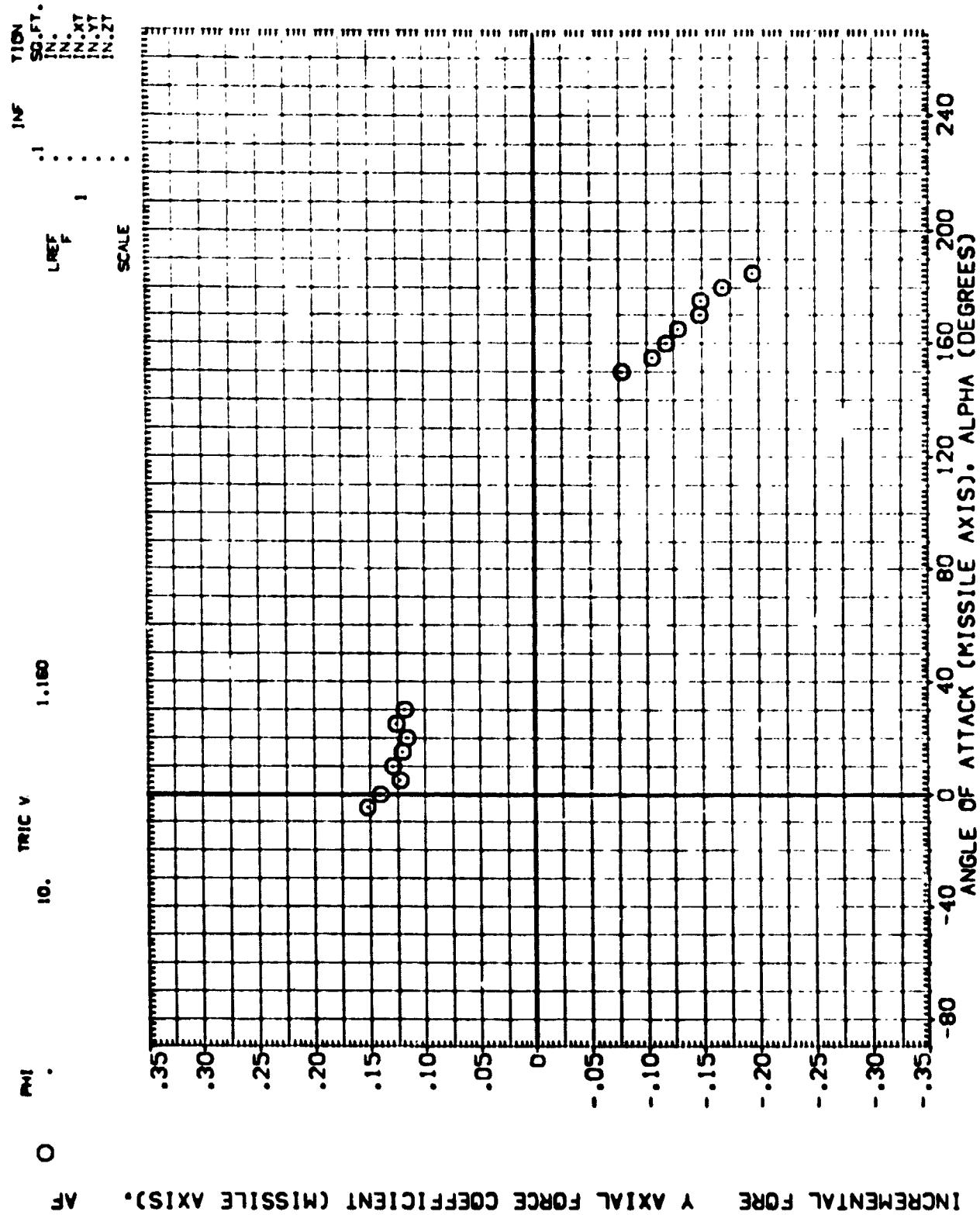
ARC 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (LEYMO1)

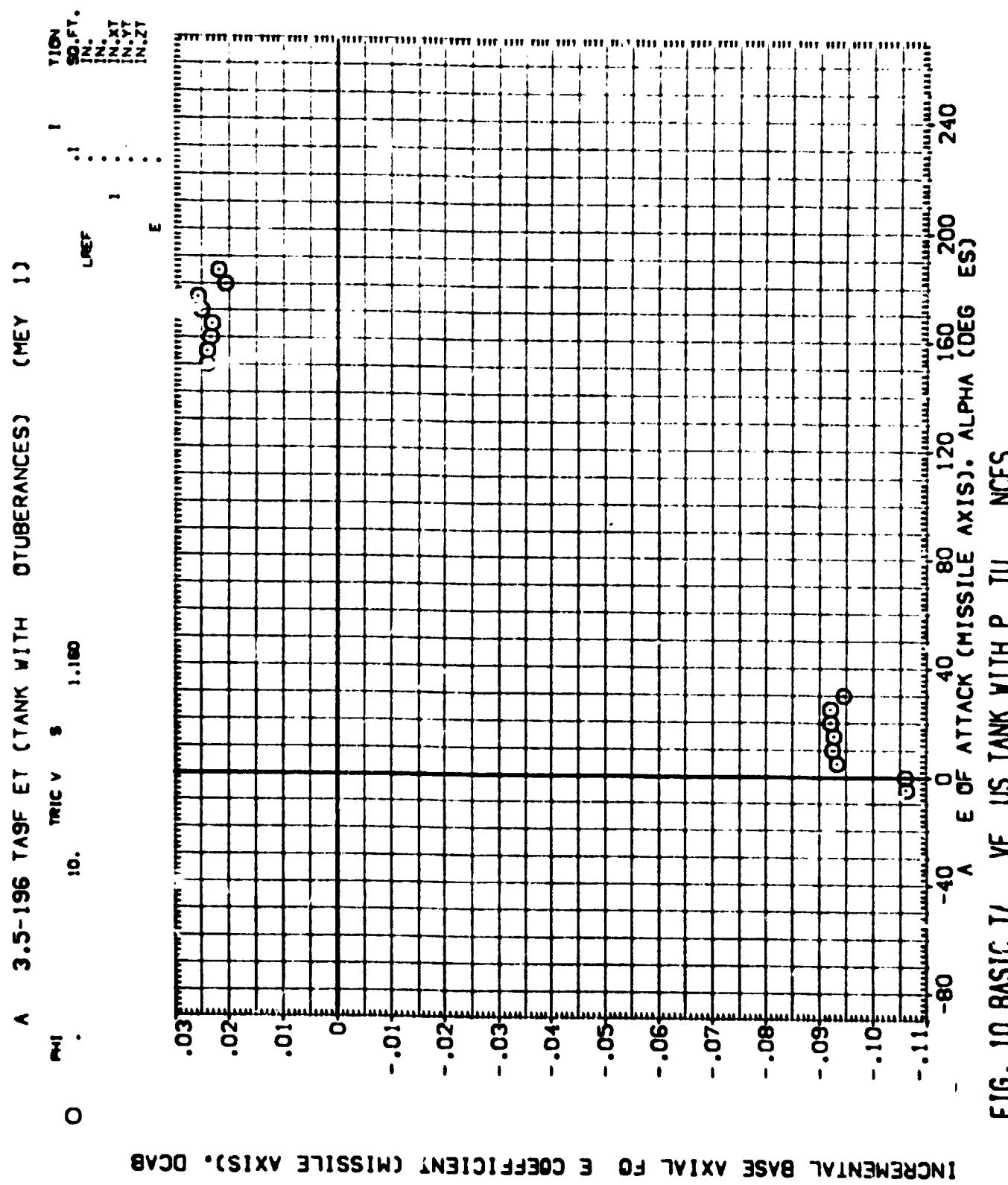


INCREMENTAL ROLLING MOMENT COEFFICIENT (MISSILE AXIS).

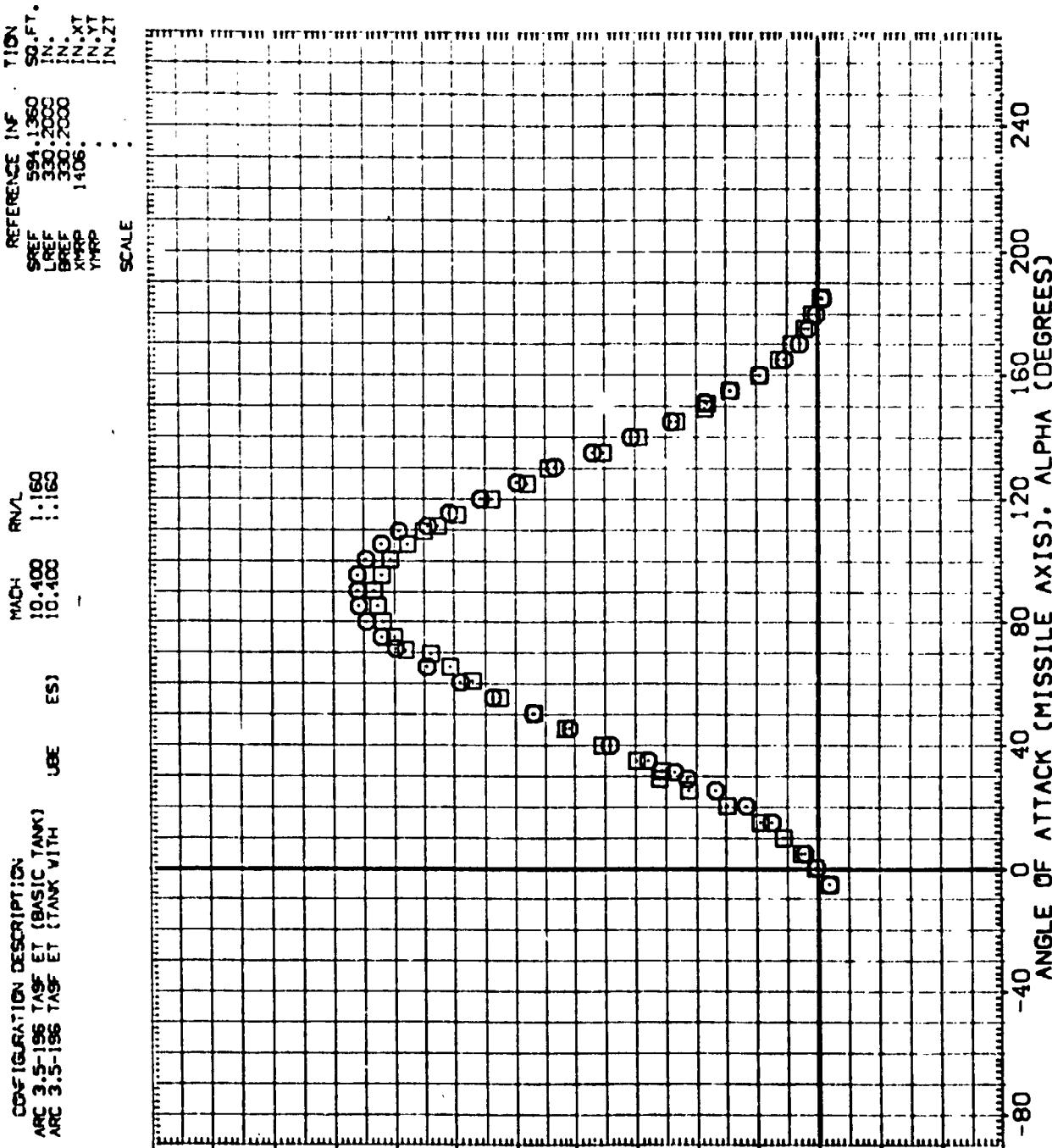
FIG. 10 BASIC TANK VERSUS TANK WITH P TUBERENCES

A 3.5-196 TAGF ET (TANK WITH PROTUBERANCES) (MEYMO1)





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NORMAL-FORCE COEFFICIENT (MISSILE AXIS). CNM

FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERENCES
 $\alpha_{\text{JPHI}} = .00$ (B) 180.00

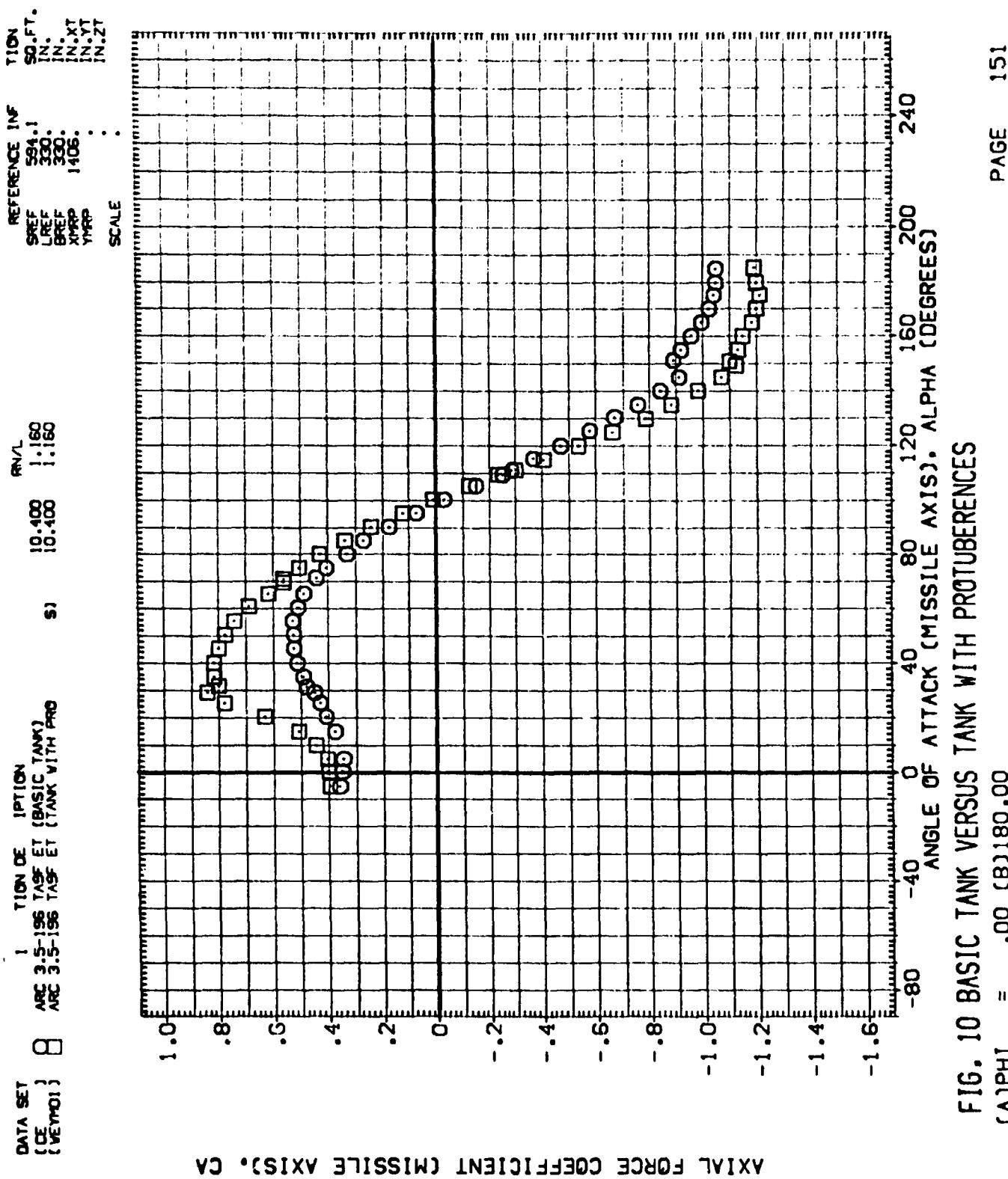


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERANCES

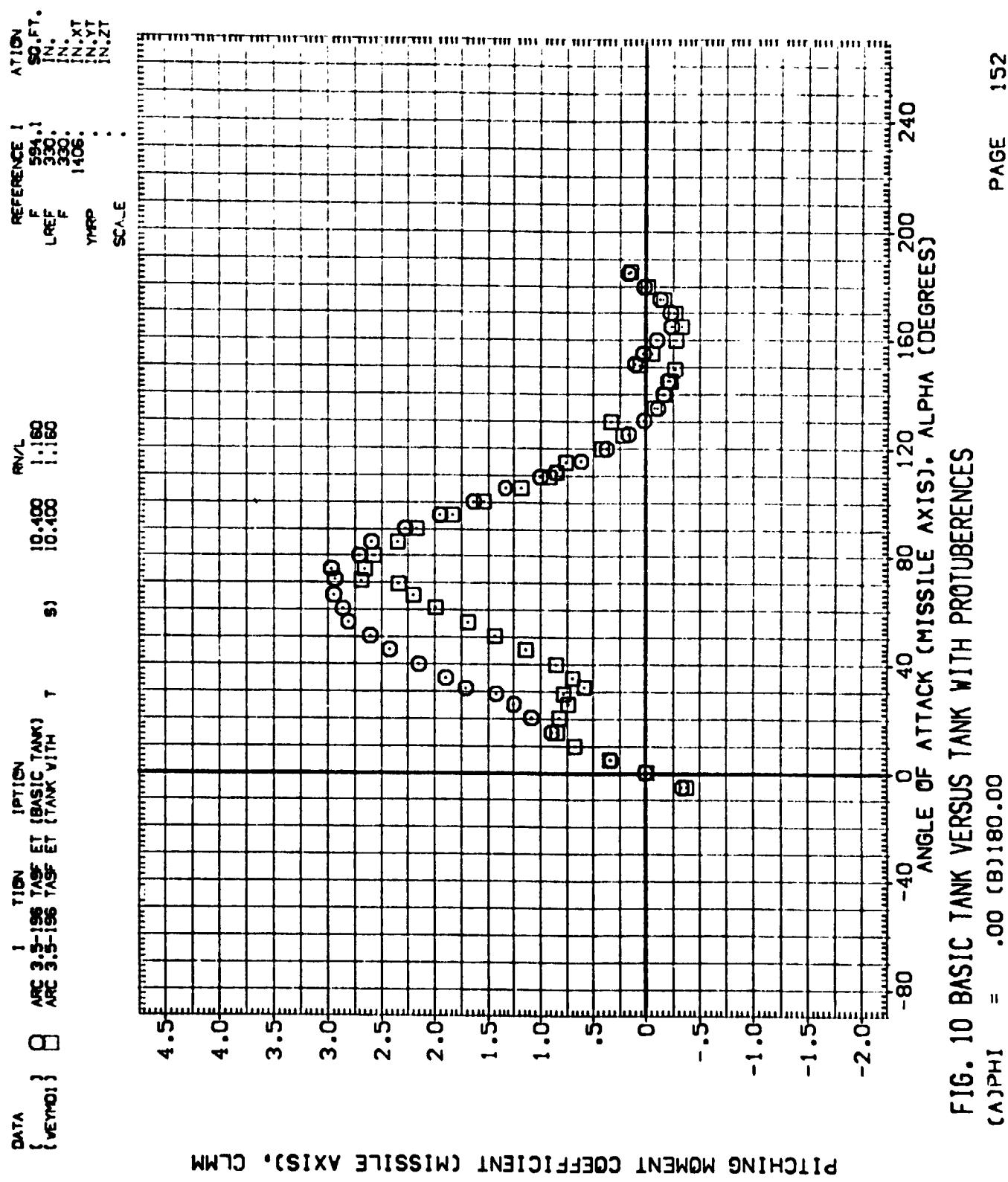


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERANCES

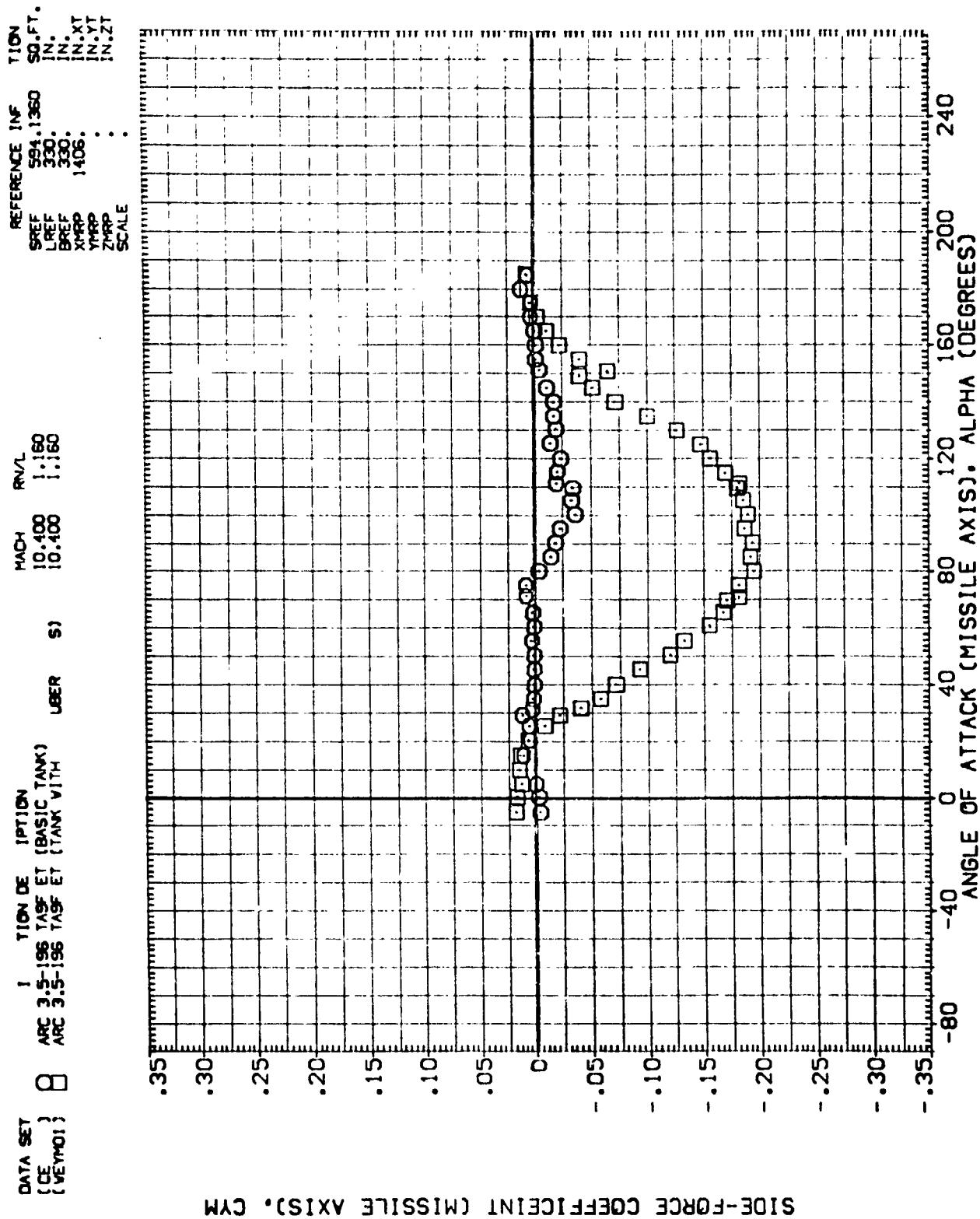


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERANCES

(A)PHI = .00 (B)180.00

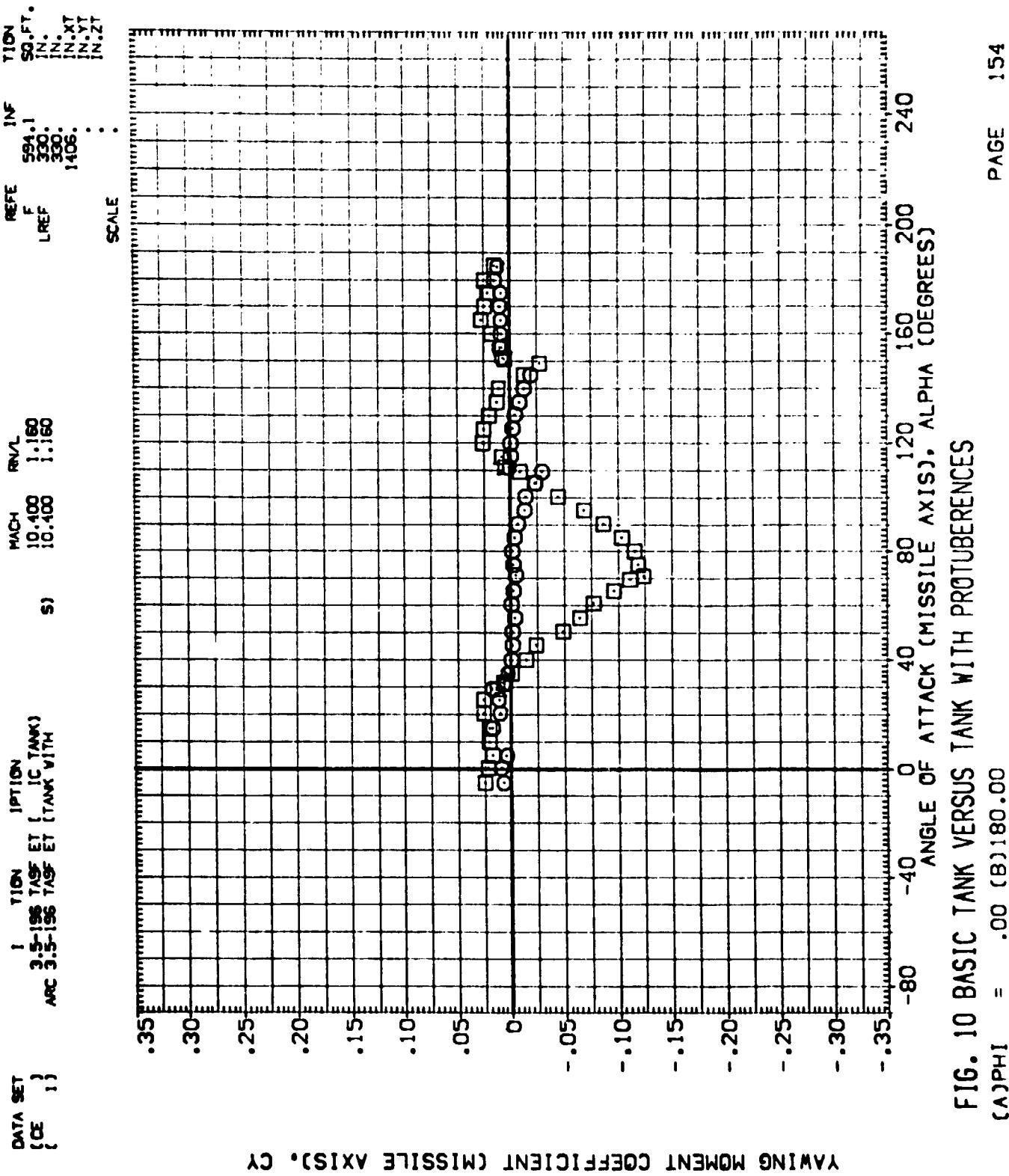
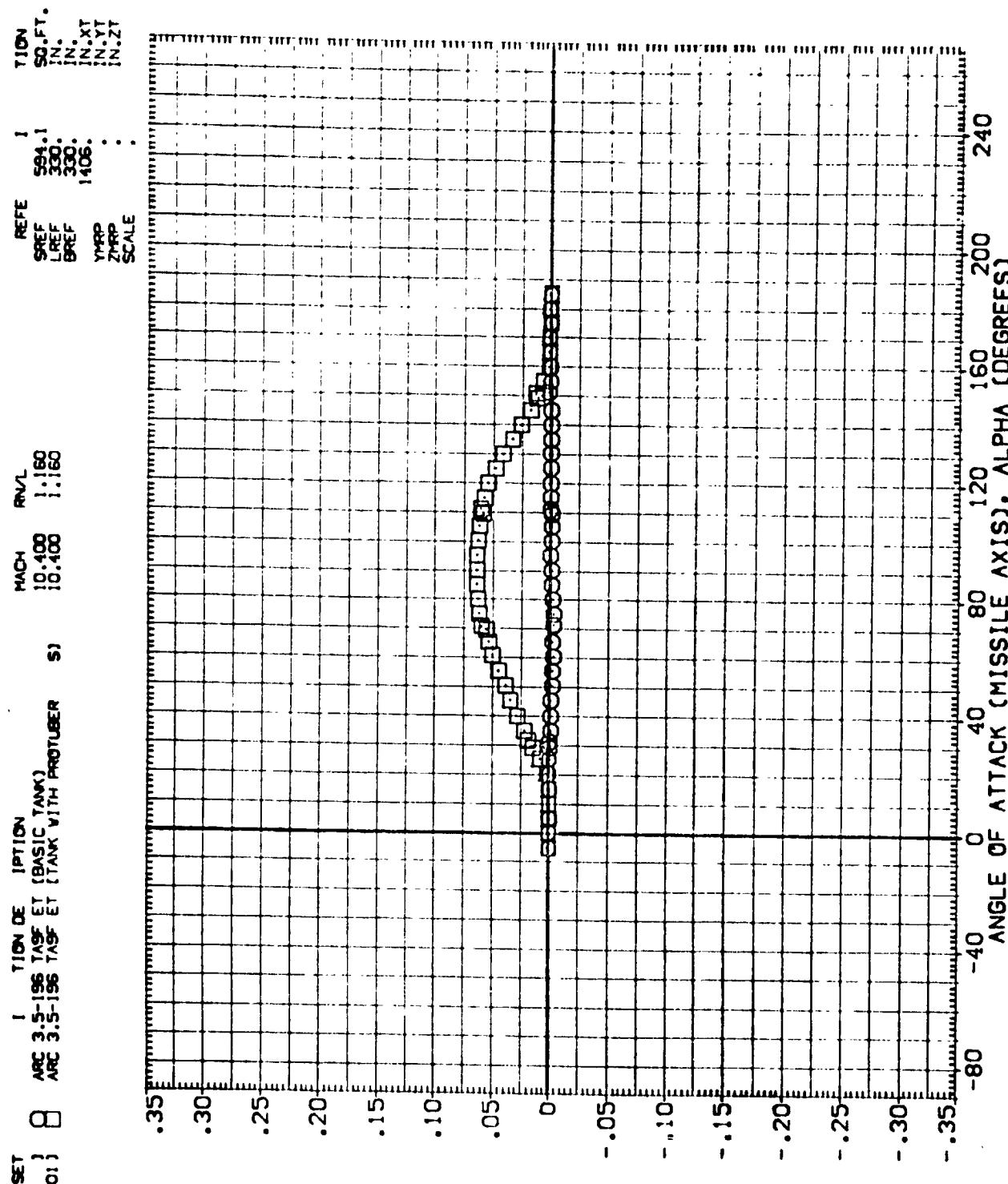


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERENCES

DATA SET I TION DE IPION
 [CE] ARC 3.5-196 TAG ET [BASIC TANK]
 [VERMO] ARC 3.5-196 TAG ET [TANK WITH PROTUBERENCES]



ROLLING MOMENT COEFFICIENT (MISSILE AXIS), CBL

FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERENCES
 $\text{CA}(\text{PHI}) = .00 \text{ (B)}180.00$

DATA SET 8 TION DE POSITION
 (CE) ARC 3:5-180 TAG ET (BASIC TANK)
 (VEMO1) / TANKE TANKE
 LER S) 10.400 1.160
 10.400 1.160

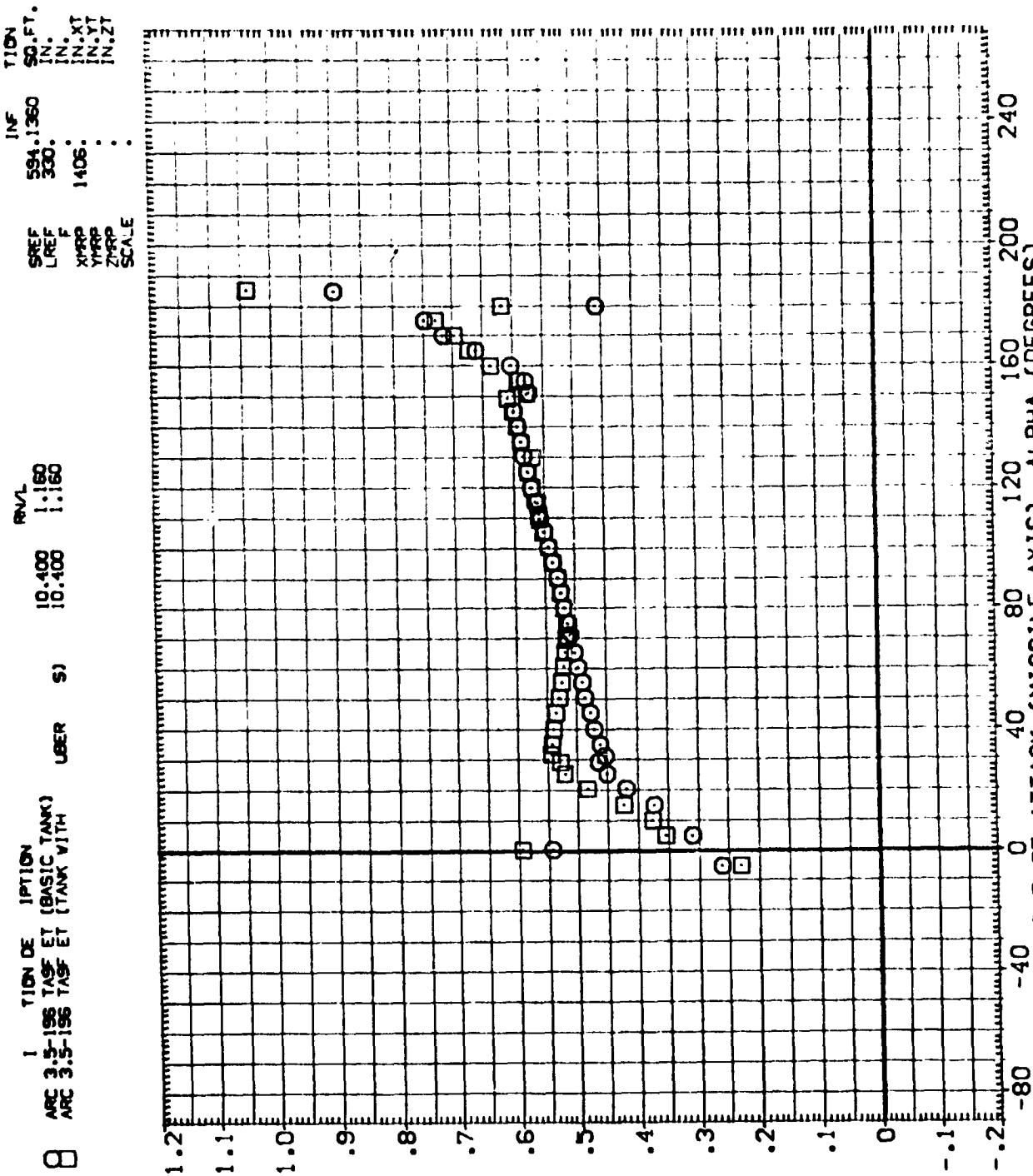


FIG. 10 BASIC TANK VERSUS TANK WITH PROTUBERANCES
 $(\Delta\phi)_1 = .00$ (B) 180.00

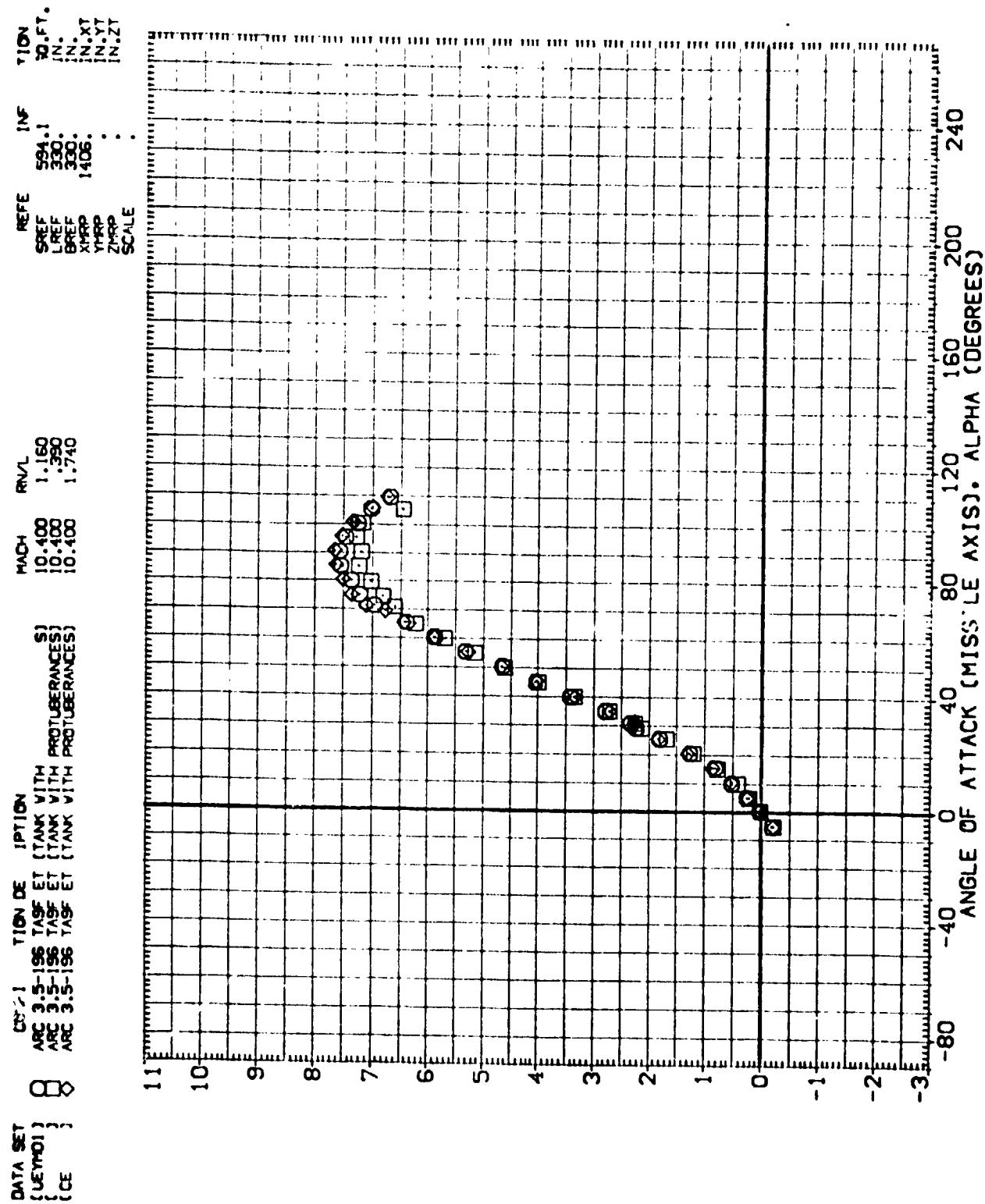


FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $\text{C}_A\text{PHI} = .00$

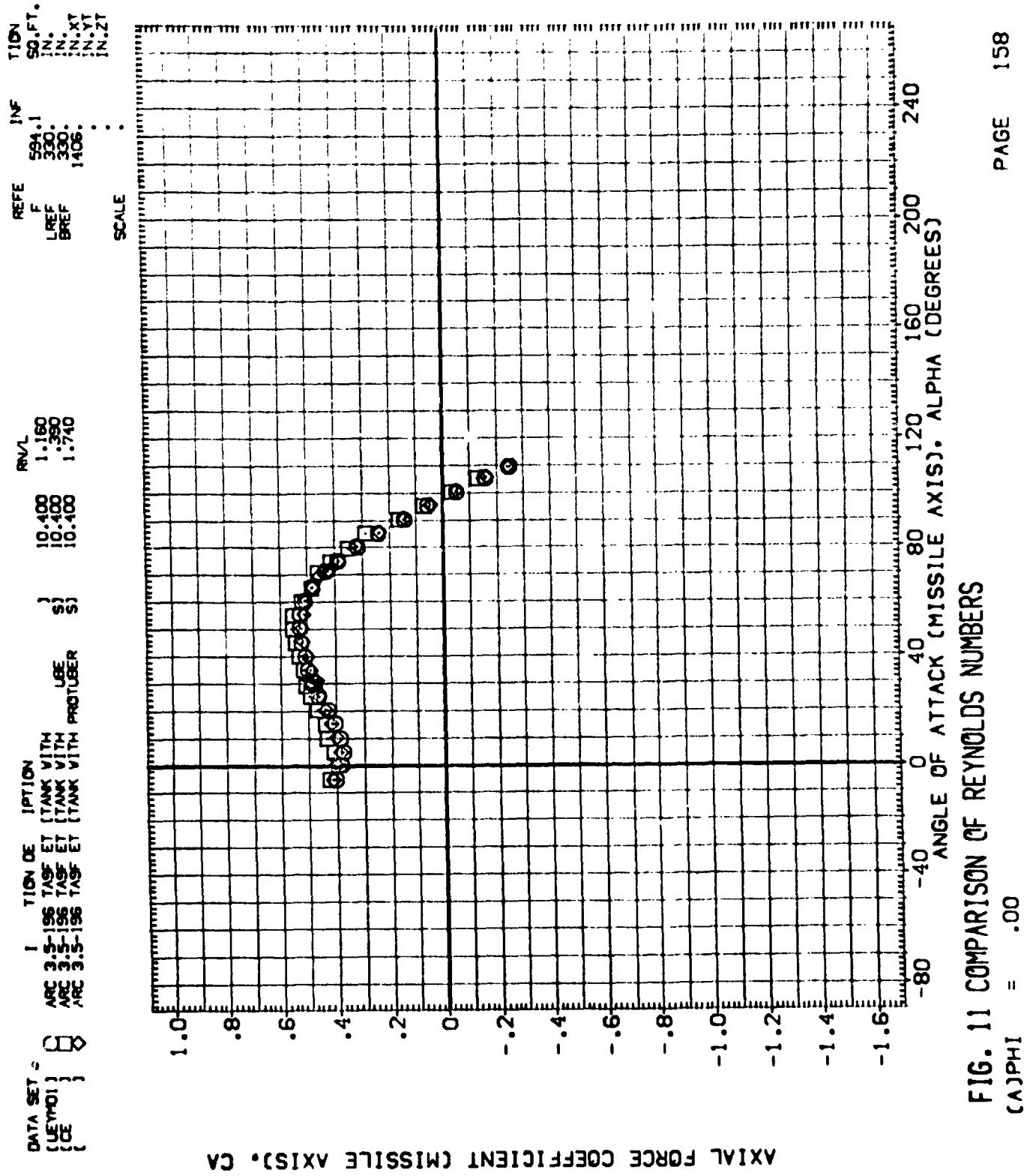
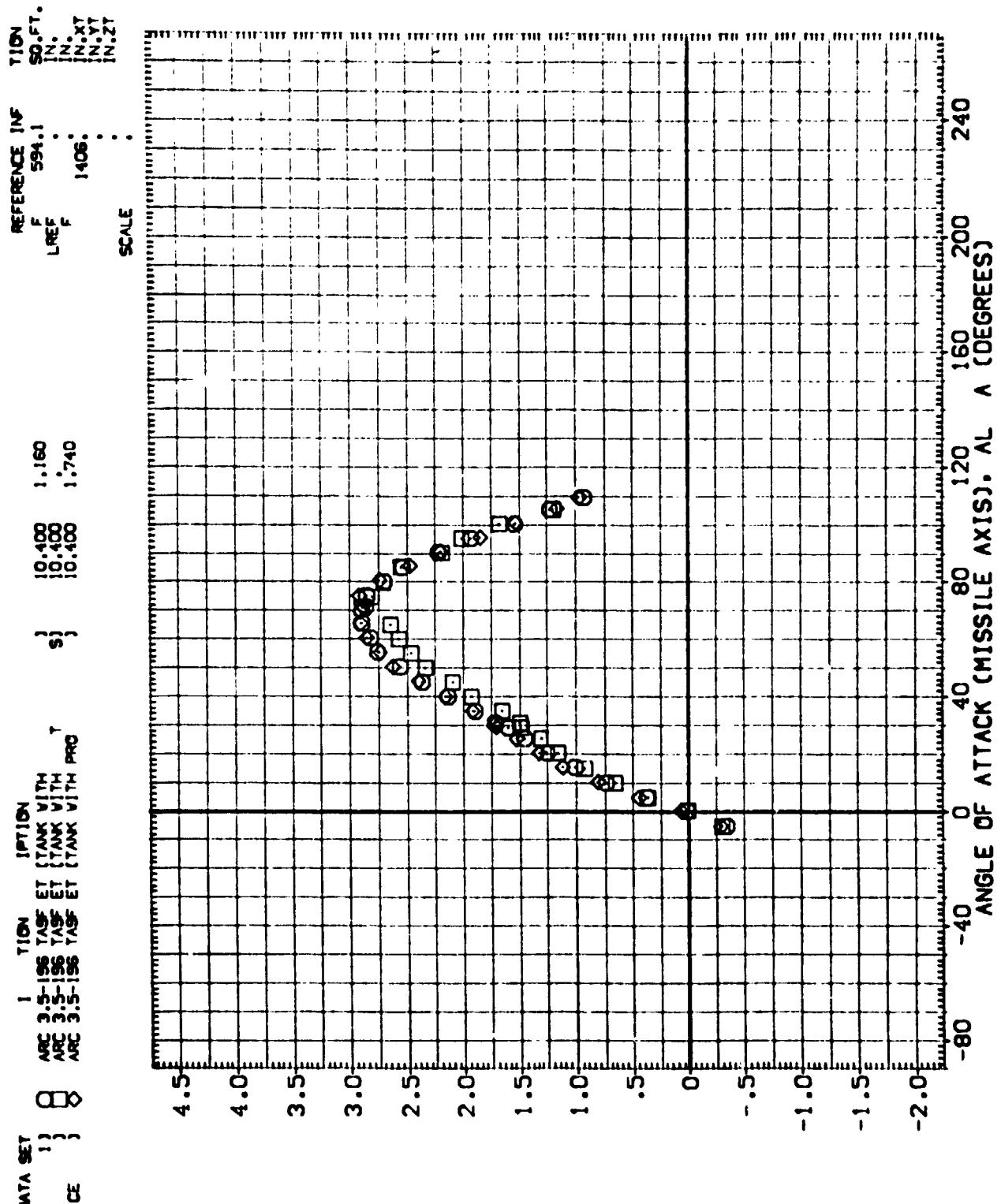
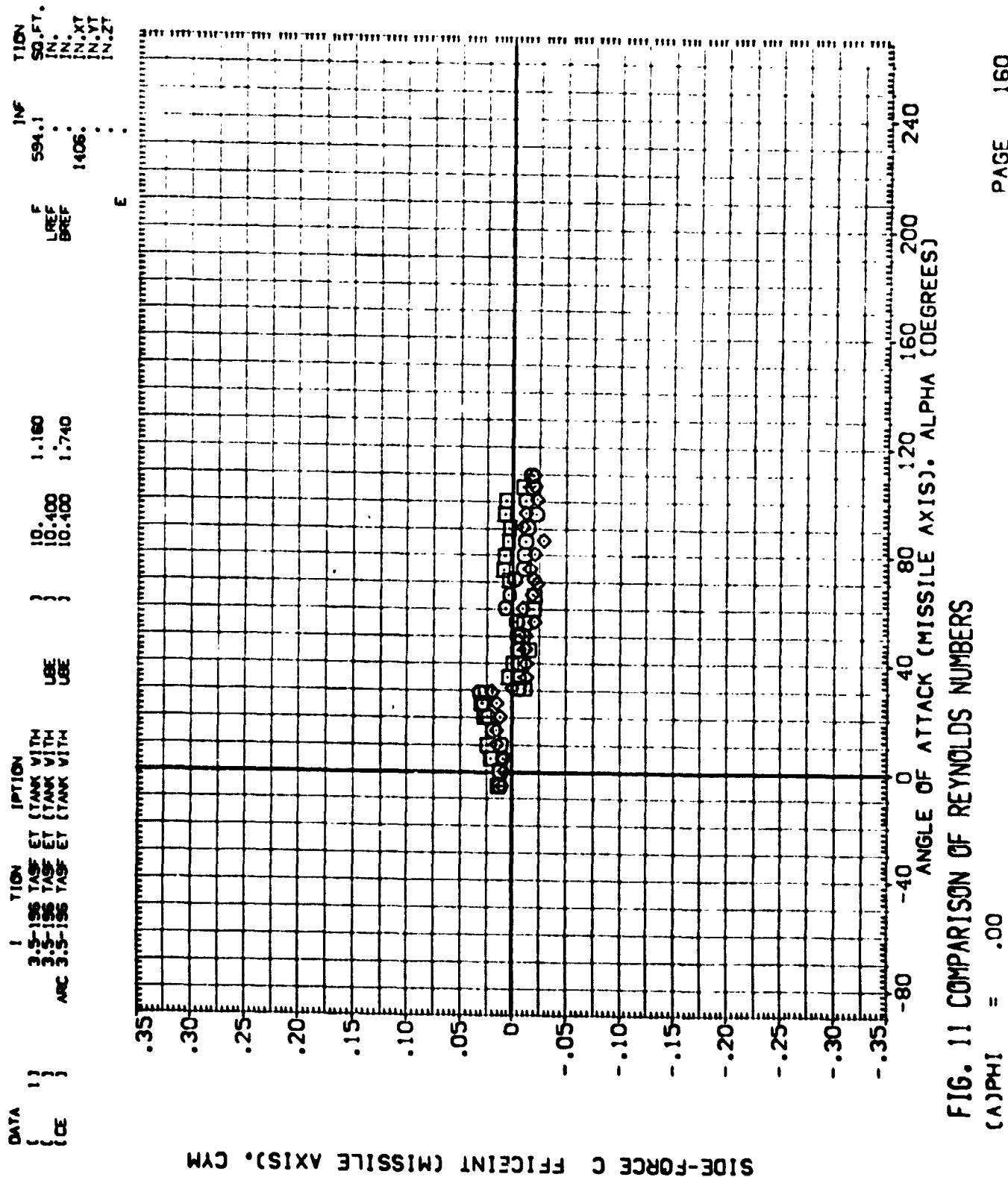
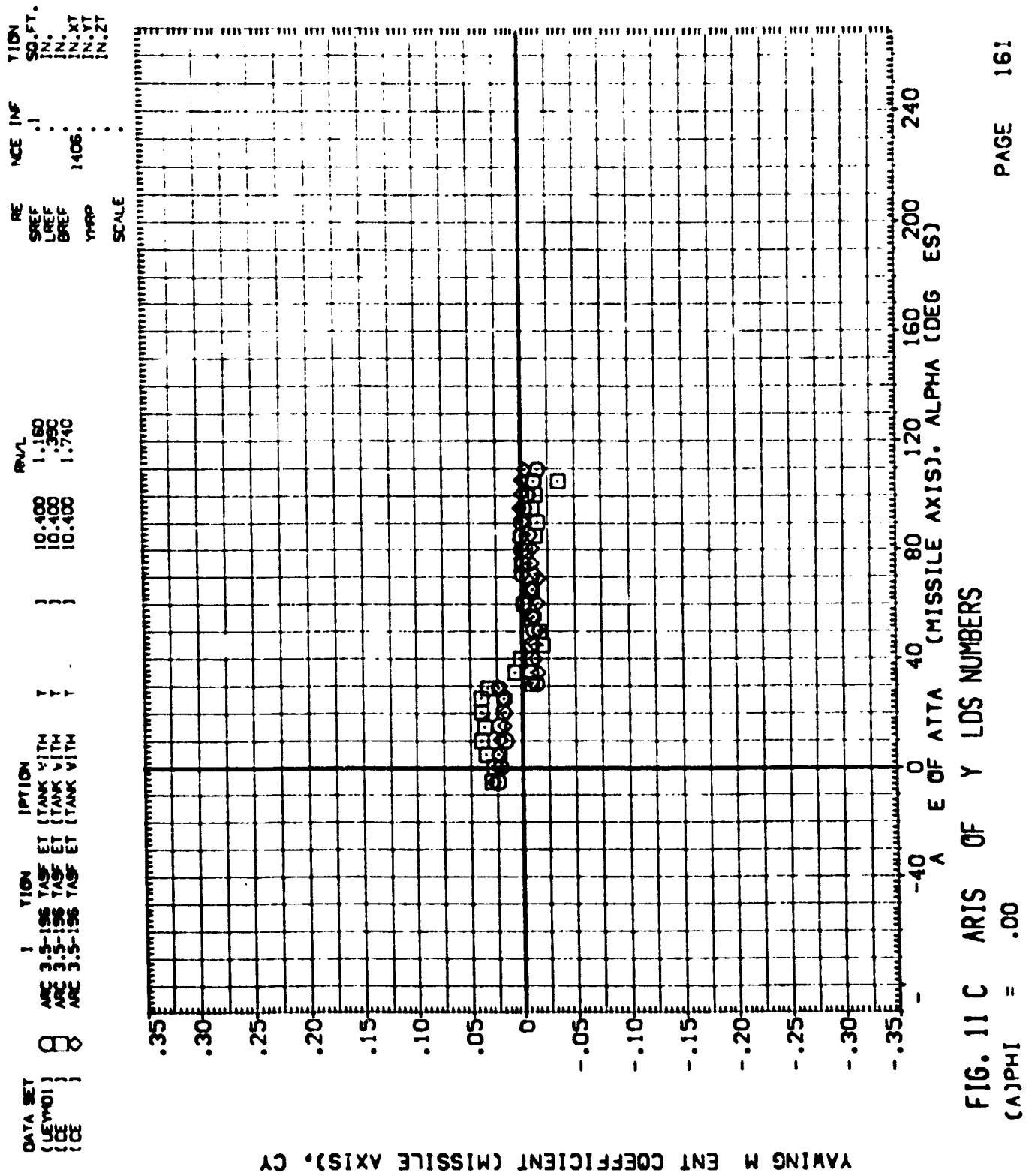


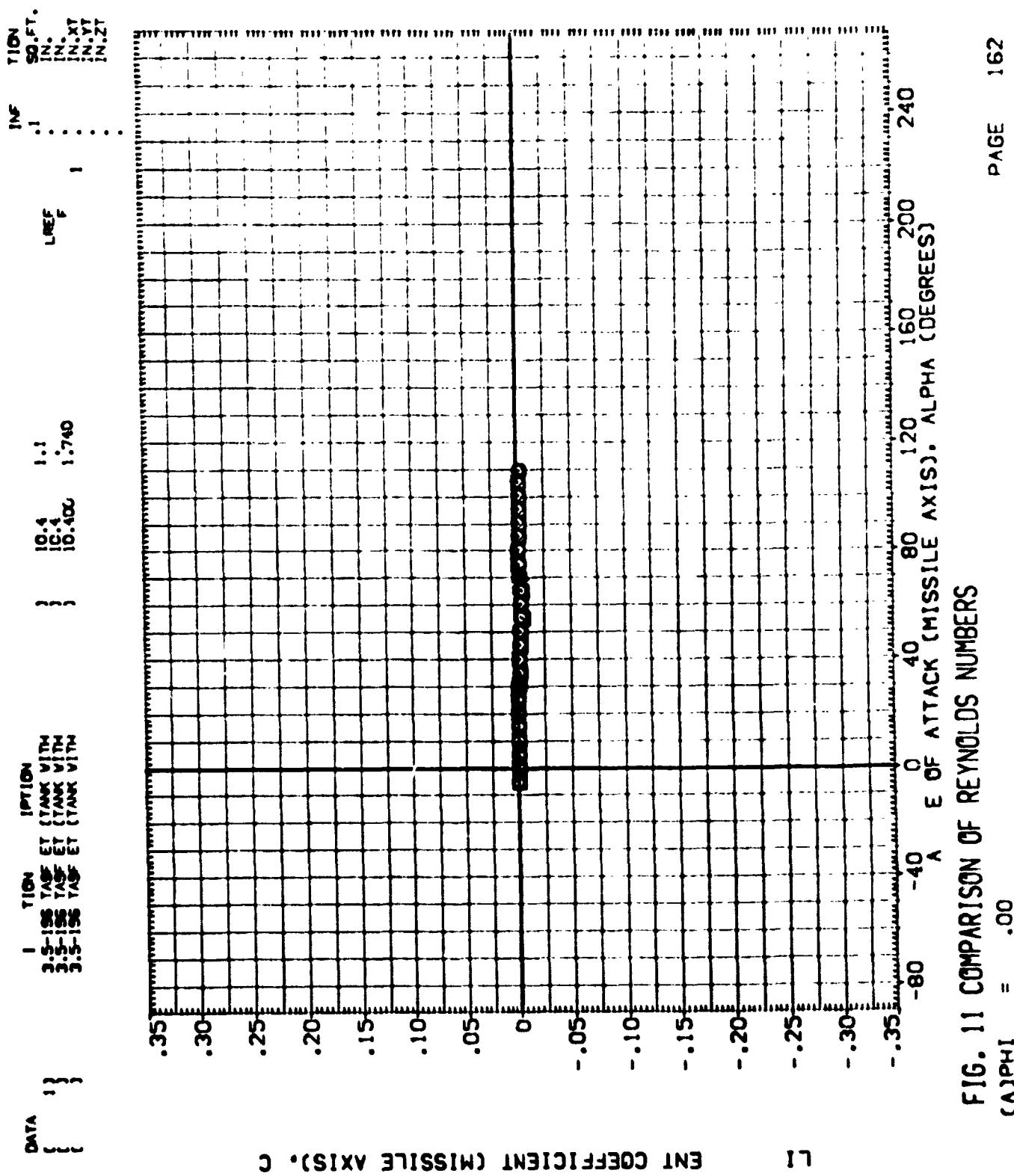
FIG. 11 COMPARISON OF REYNOLDS NUMBERS

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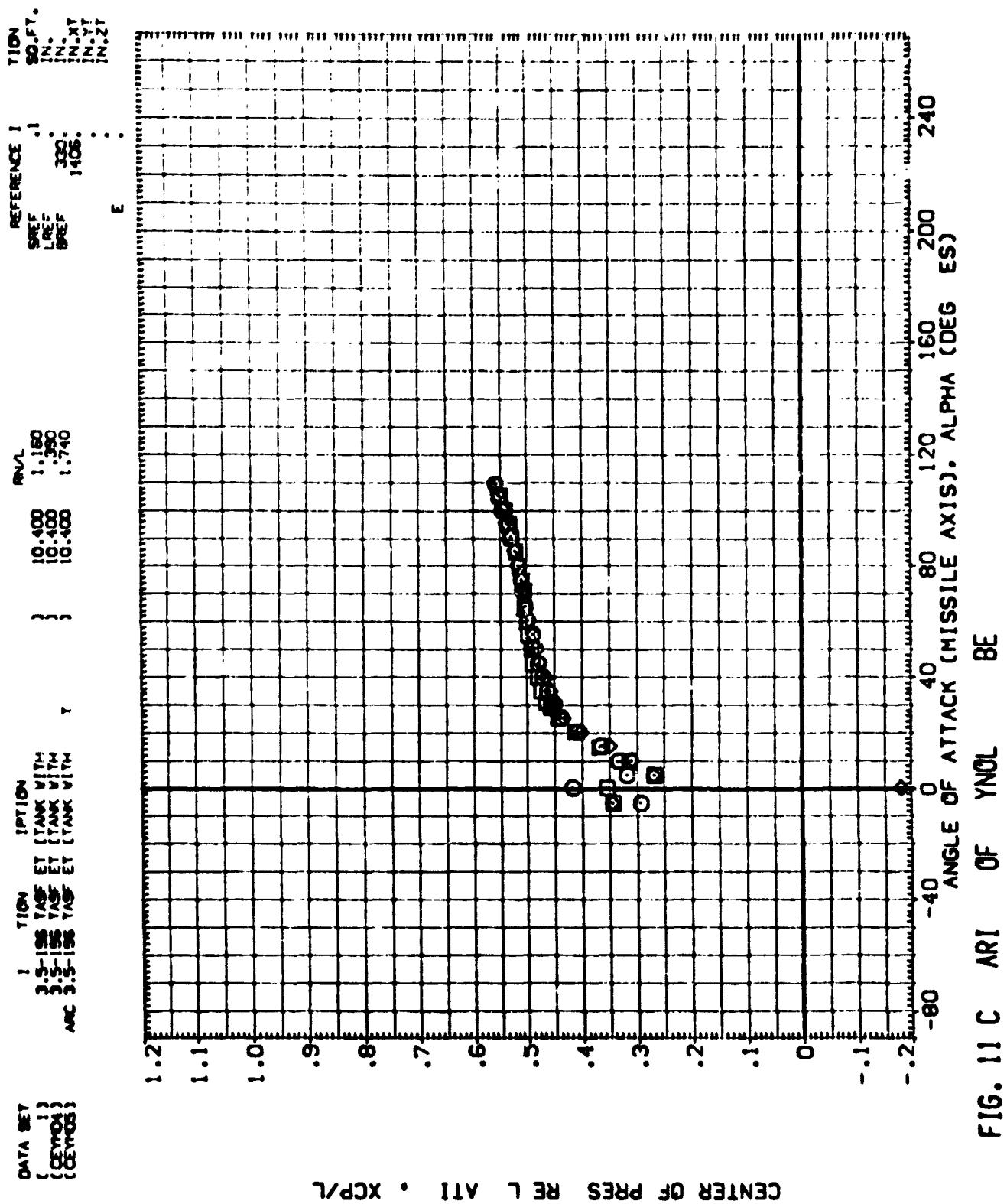
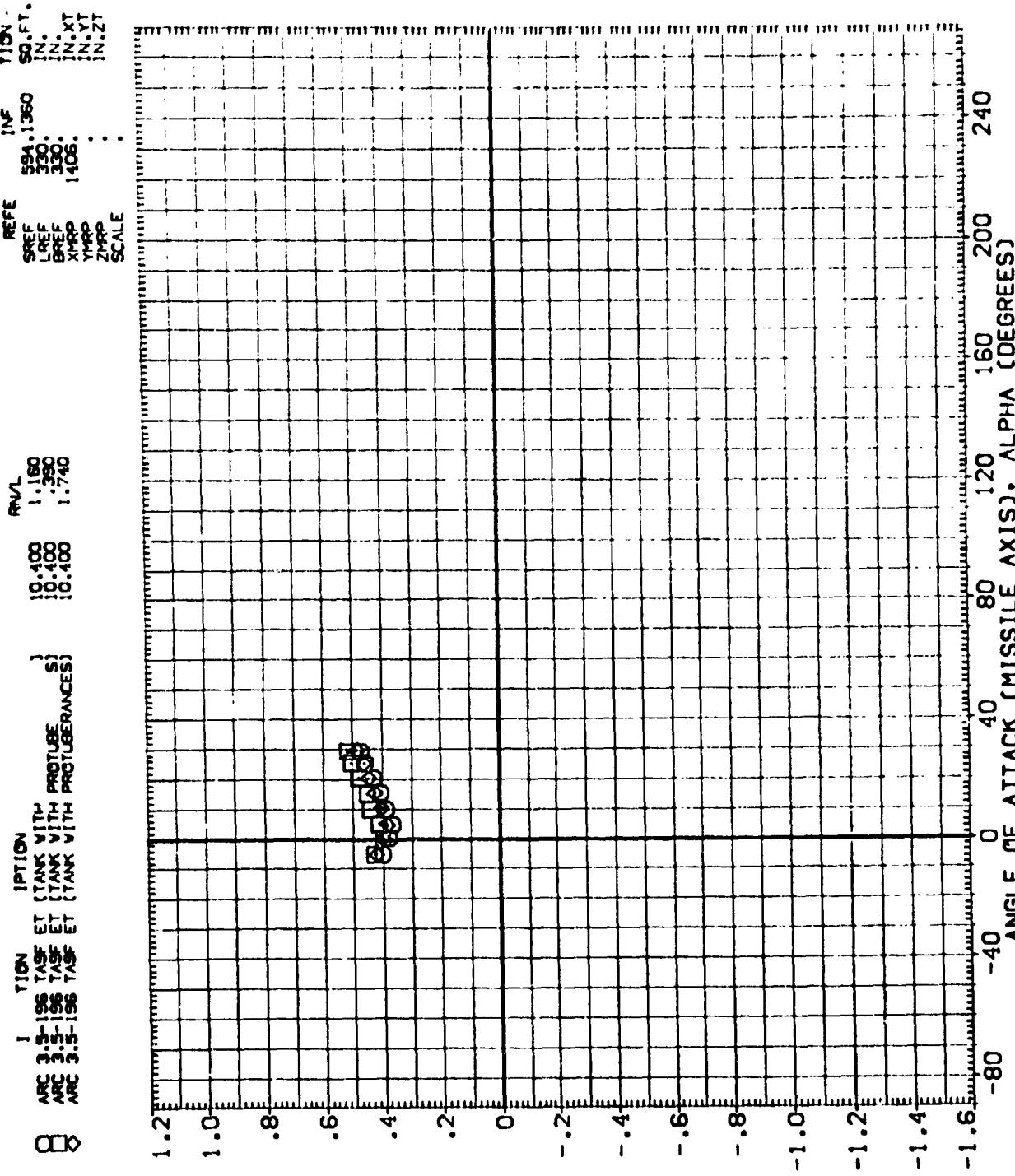


FIG. 11 C ARI OF YNOL BE
($\Delta\phi$) = .00

DATA SET 8 TION
 { VENUS } ARC 3.5-196 TAGF ET [TANK WITH PROTEUS]
 { BETHA4 } ARC 3.5-196 TAGF ET [TANK WITH PROTEUS]
 { BETHA4 } ARC 3.5-196 TAGF ET [TANK WITH PROTEUS]



FOREBODY AXIAL FORCE COEFFICIENT (MISSILE AXIS). CAF

FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $(\Delta \rho \Phi) = .00$

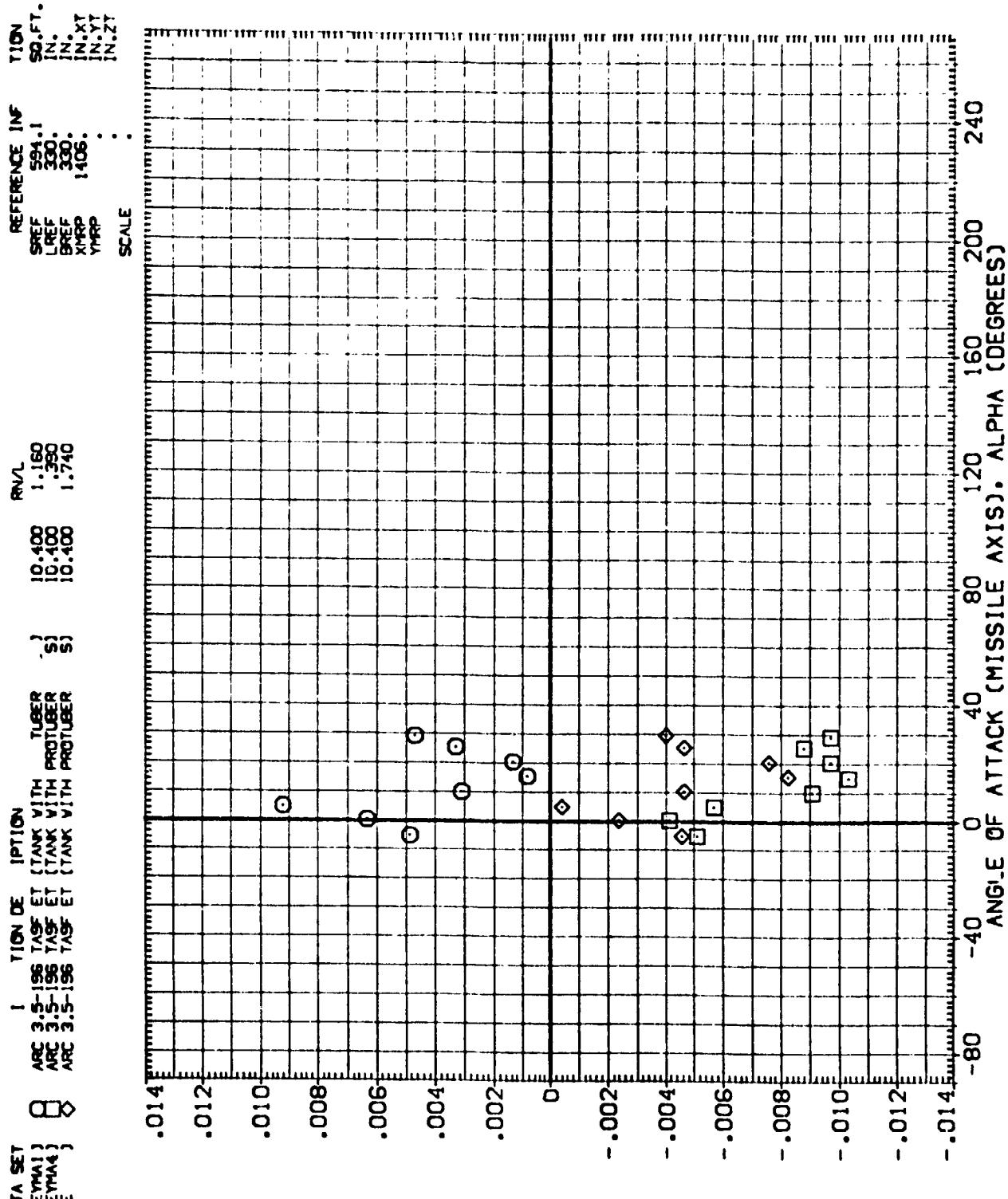


FIG. 11 COMPARISON OF REYNOLDS NUMBERS

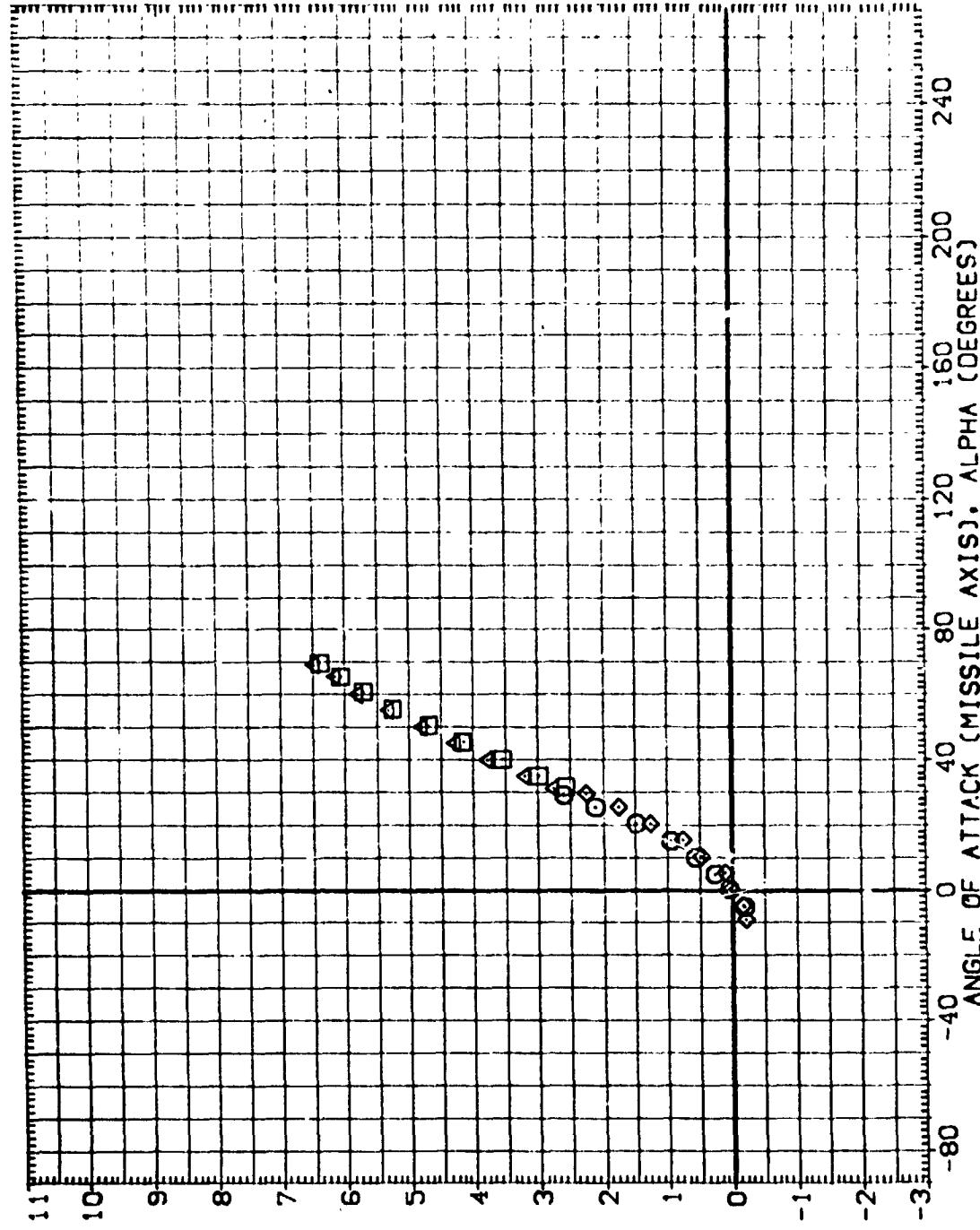
$(\Delta \rho)_1 = .00$

REFERENCE INFORMATION

SREF	594.1360	SO. FT.
LREF	330.	IN.
BREF	330.	IN.
	1406.	IN.
	1407.	IN.

DATA SET ACTION DE OPTION

(CEYMA1)	ARC 3.5-196	TASF ET	[TANK WITH PROTUBERANCES]	S1
(CEYMA2)	ARC 3.5-196	TASF ET	[TANK WITH PROTUBERANCES]	S1
(REYMA6)	ARC 3.5-196	TASF ET	[TANK WITH PROTUBERANCES]	S1
(REYMG6)	ARC 3.5-196	TASF ET	[TANK WITH PROTUBERANCES]	S1



NORMAL-FORCE COEFFICIENT (MISSILE AXIS). CNM

FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $(\Delta \rho \dot{V}) = 180.00$

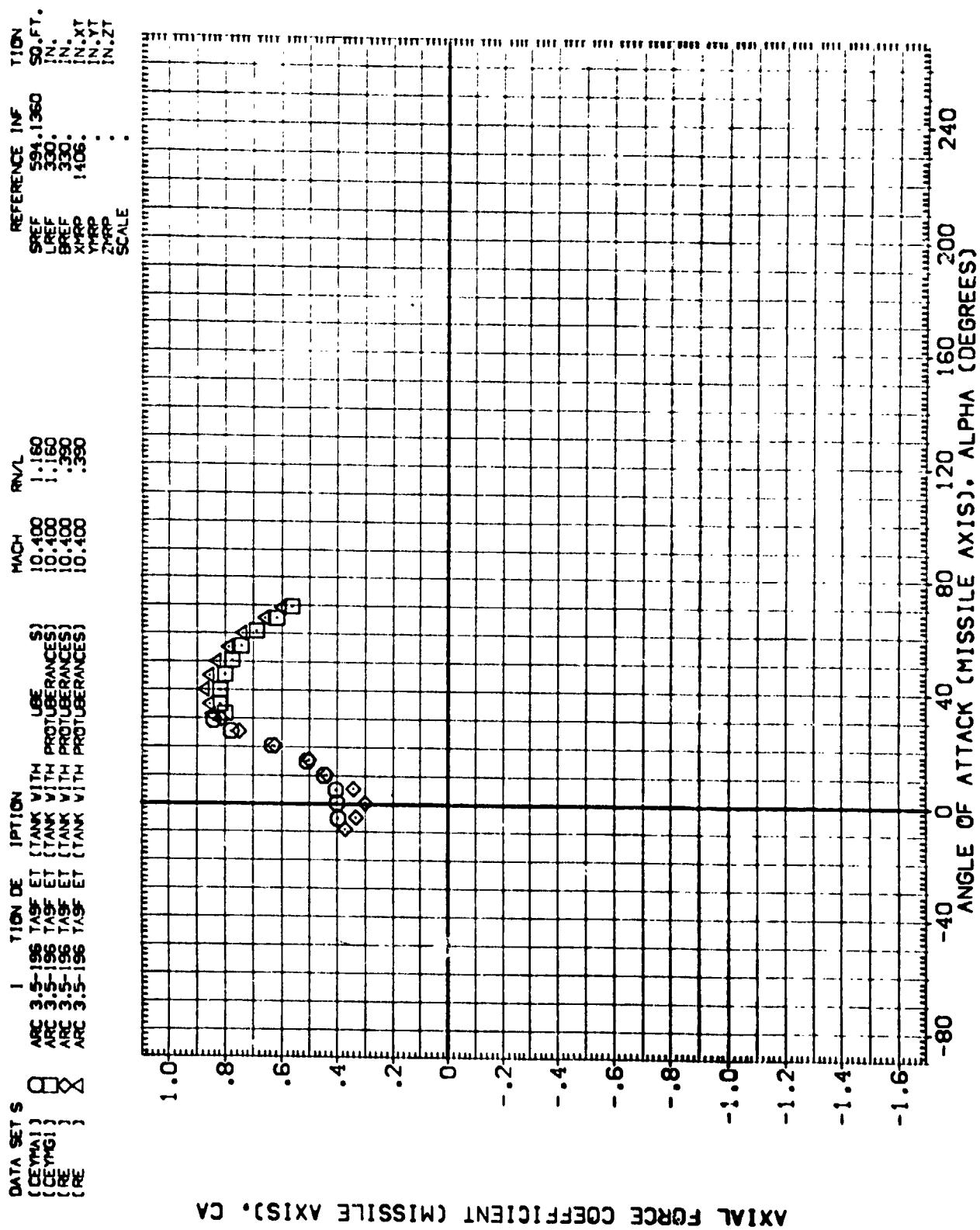
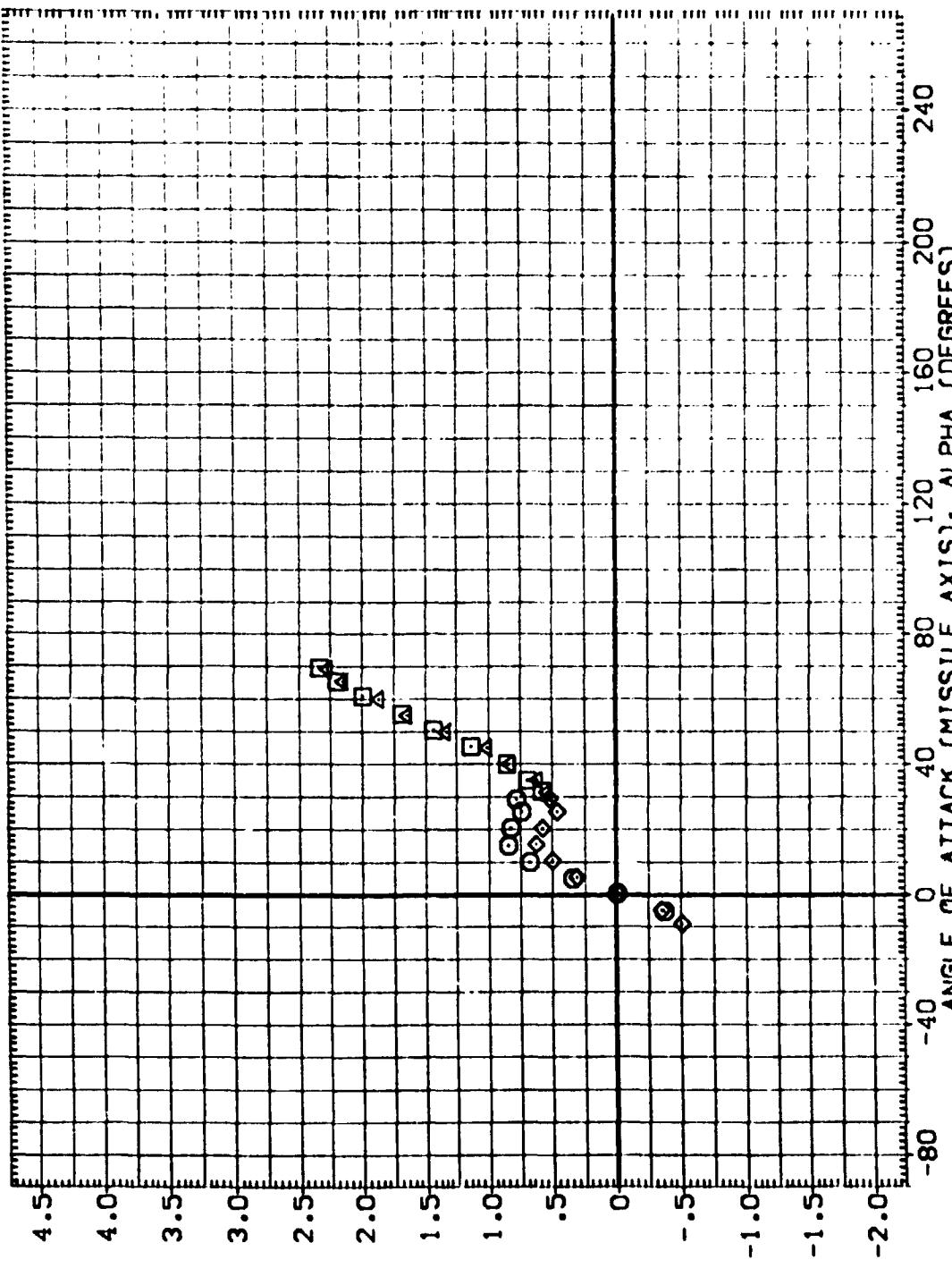


FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $(\alpha \rho H) = 180.00$

DATA SET
 { CEMAI } O 1. TION DE. IPTION
 { CEMGI } X 2.
 { CEM } X 3.
 { RE } X 4.

REFERENCE ! T16N
 MACH 1.160 1.160
 RVEL 1.160 1.160
 SREF 594.1360 50. FT.
 LREF 330. N.
 BREF 330. N.
 1406. N. XT
 YMRP 1406. N. YT
 ZMRP 1406. N. ZT
 SCALE .



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLMM

FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $\alpha\phi\pi = 180.00$

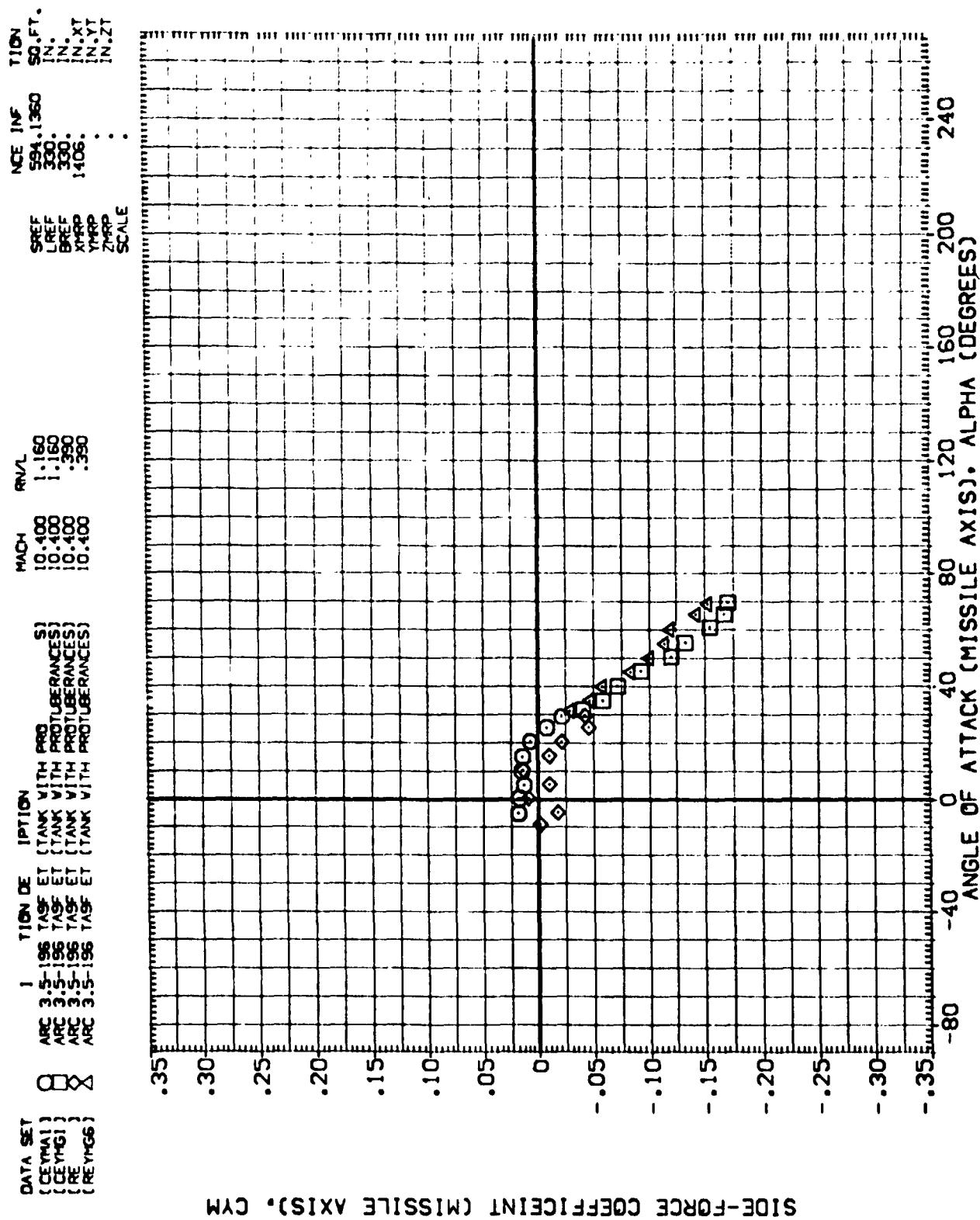
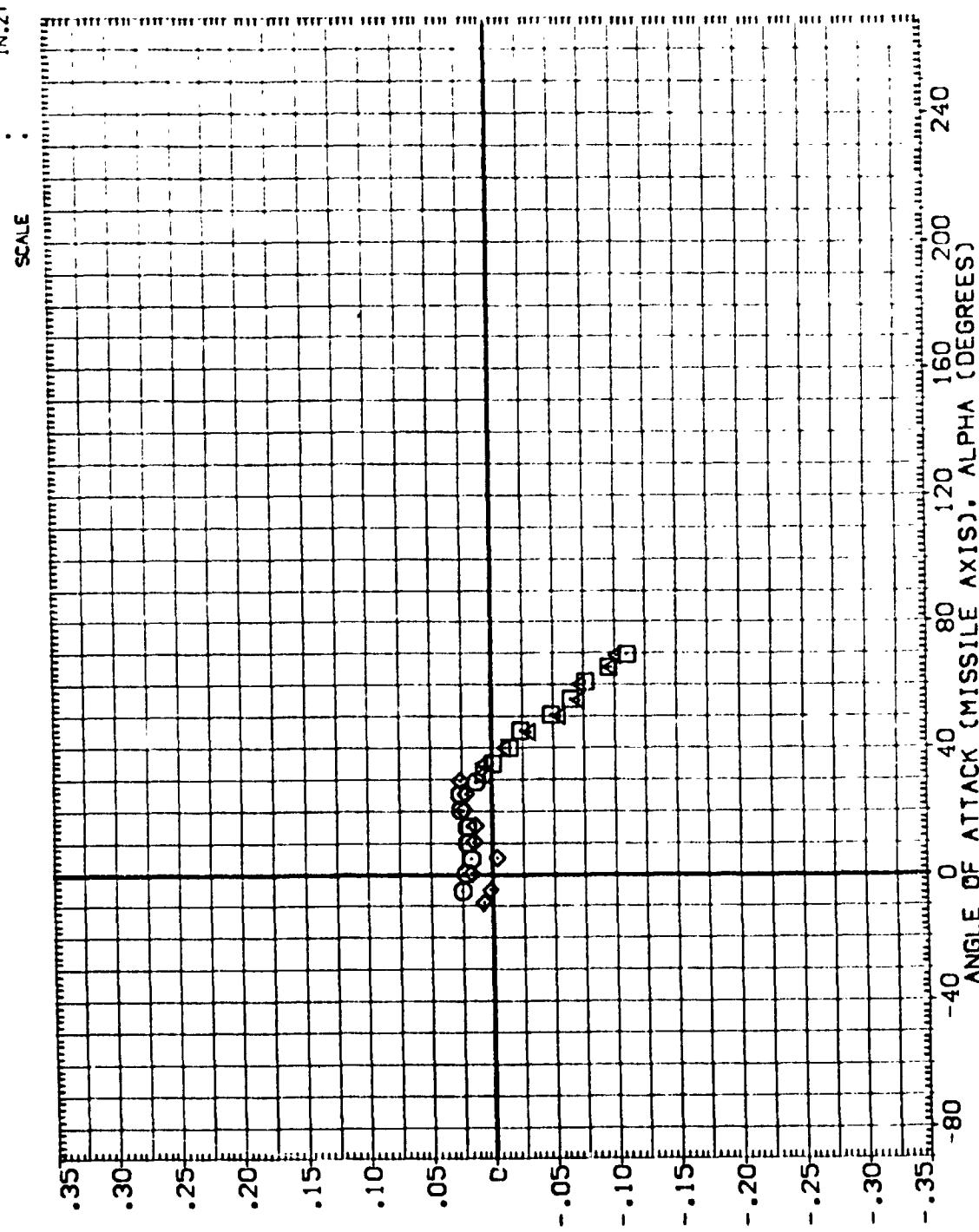


FIG. 11 COMPARISON OF REYNOLDS NUMBERS

DATA SET 1 TION DESCRIPTION
 (CEMM) ARC 3.5-136 TAG ET (TANK WITH PROTRUANCES)
 (CEMM) ARC 3.5-136 TAG ET (TANK WITH PROTRUANCES)
 (CEMM) ARC 3.5-136 TAG ET (TANK WITH PROTRUANCES)
 (CEMM) ARC 3.5-136 TAG ET (TANK WITH PROTRUANCES)

REFERENCE INFORMATION
 SREF 594.1360 SO.FT.
 LREF 330. N.
 BREF 330.2000 N.
 XMRP 1408. N.XT
 YMRP . N.YT
 ZMRP . N.ZT

MACH RV/L
 10.400 1.60
 10.400 1.60
 10.400 .250
 10.400 .250



YAWING MOMENT COEFFICIENT (MISSILE AXIS), CYNM

FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 $(\alpha/\phi) = 180.00$

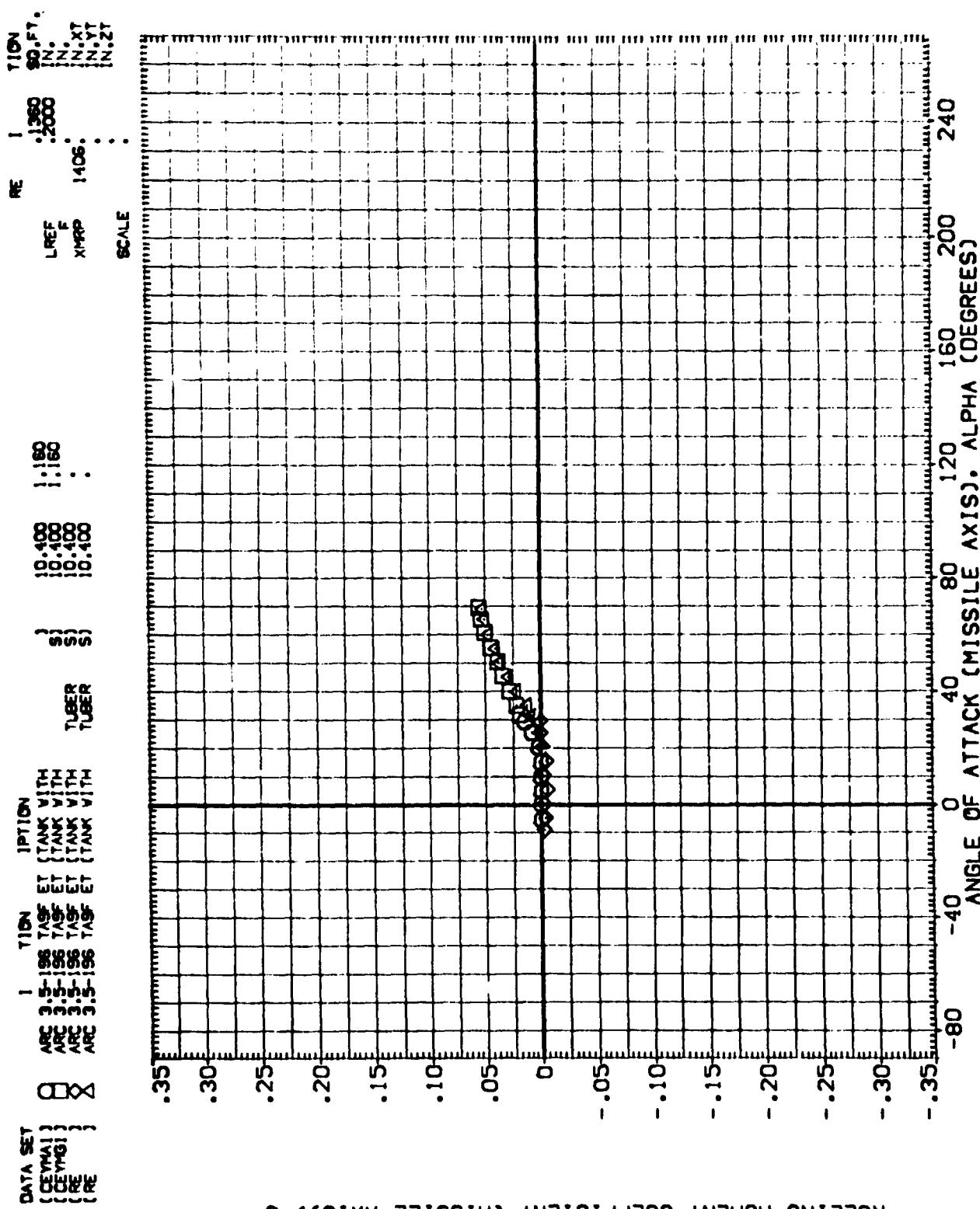


FIG. 11 COMPARISON OF REYNOLDS NUMBERS

(A) ϕ = 180.00

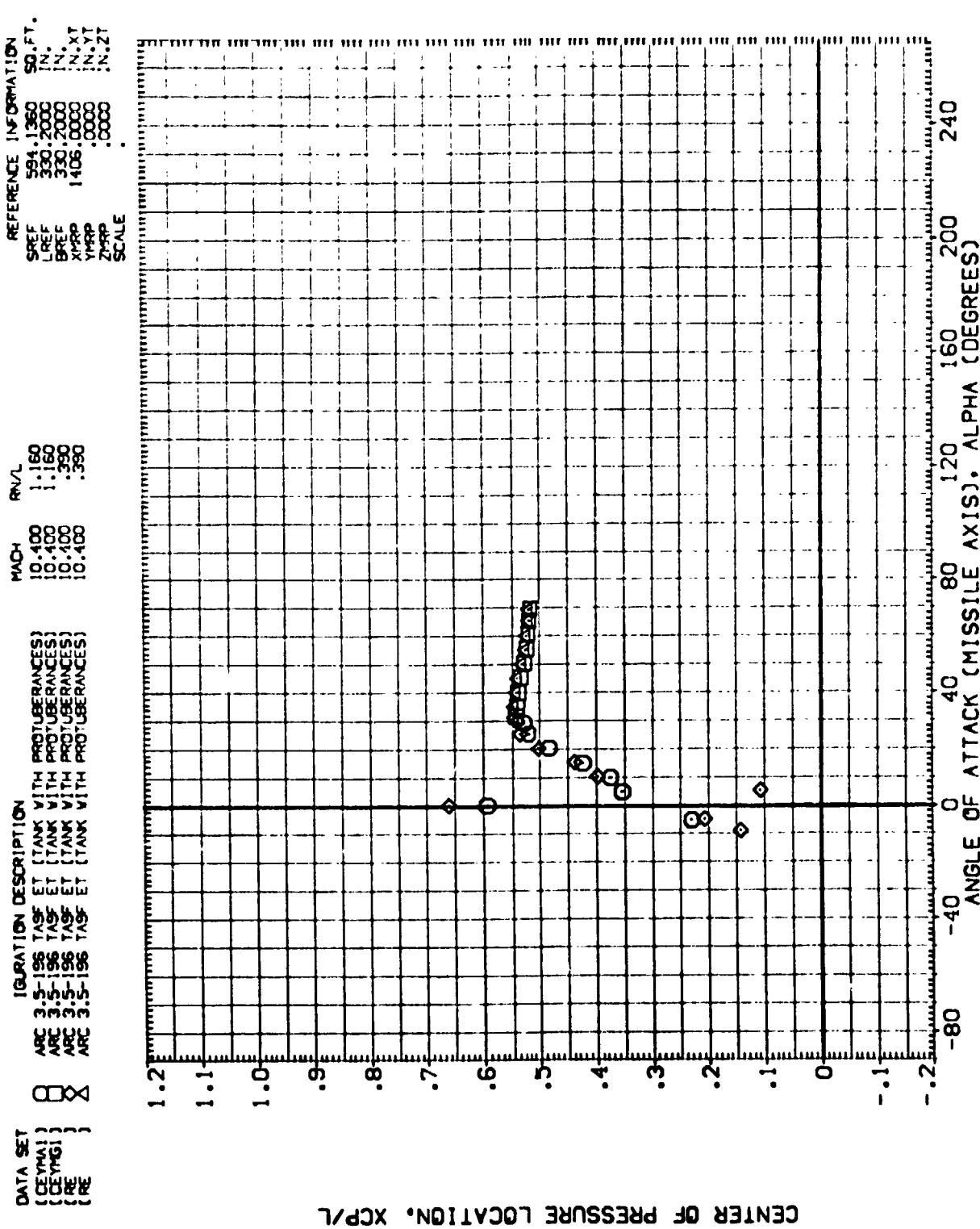


FIG. 11 COMPARISON OF REYNOLDS NUMBERS
 (α) _{PHI} = 180.00

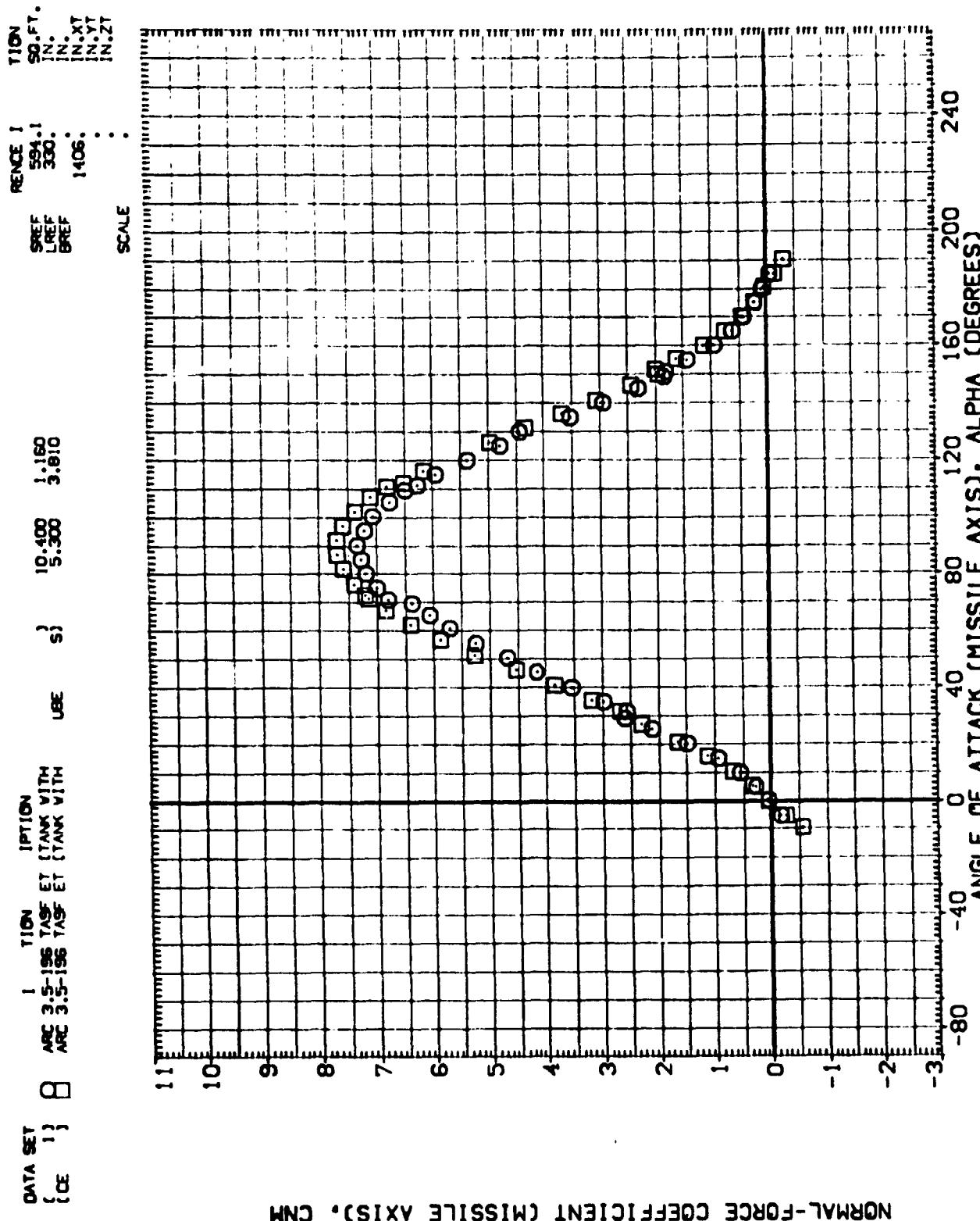


FIG. 12 MACH NUMBER AND REYNOLDS NUMBER COMPARISON
 $(\Delta\phi)_I = 180.00$

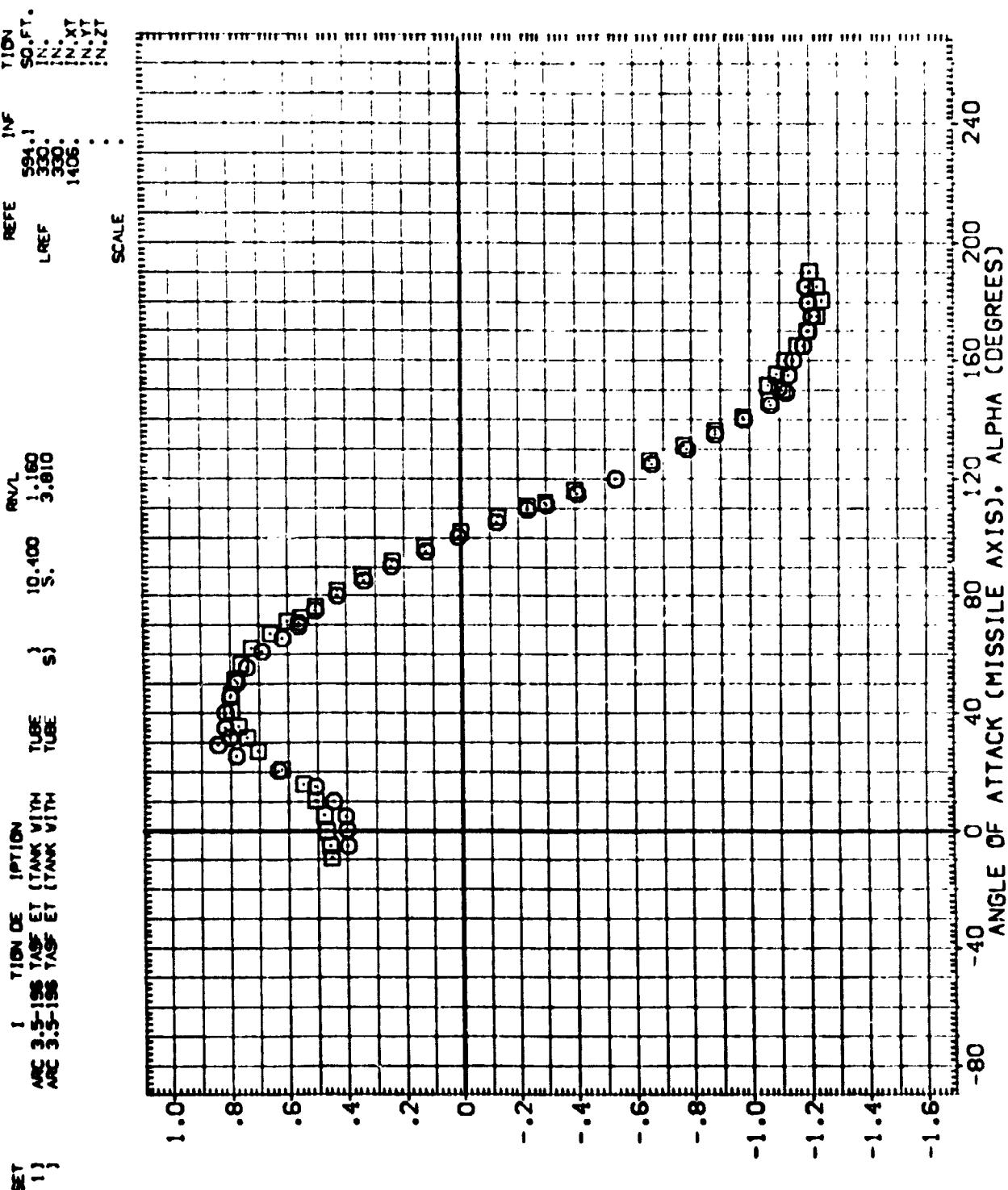
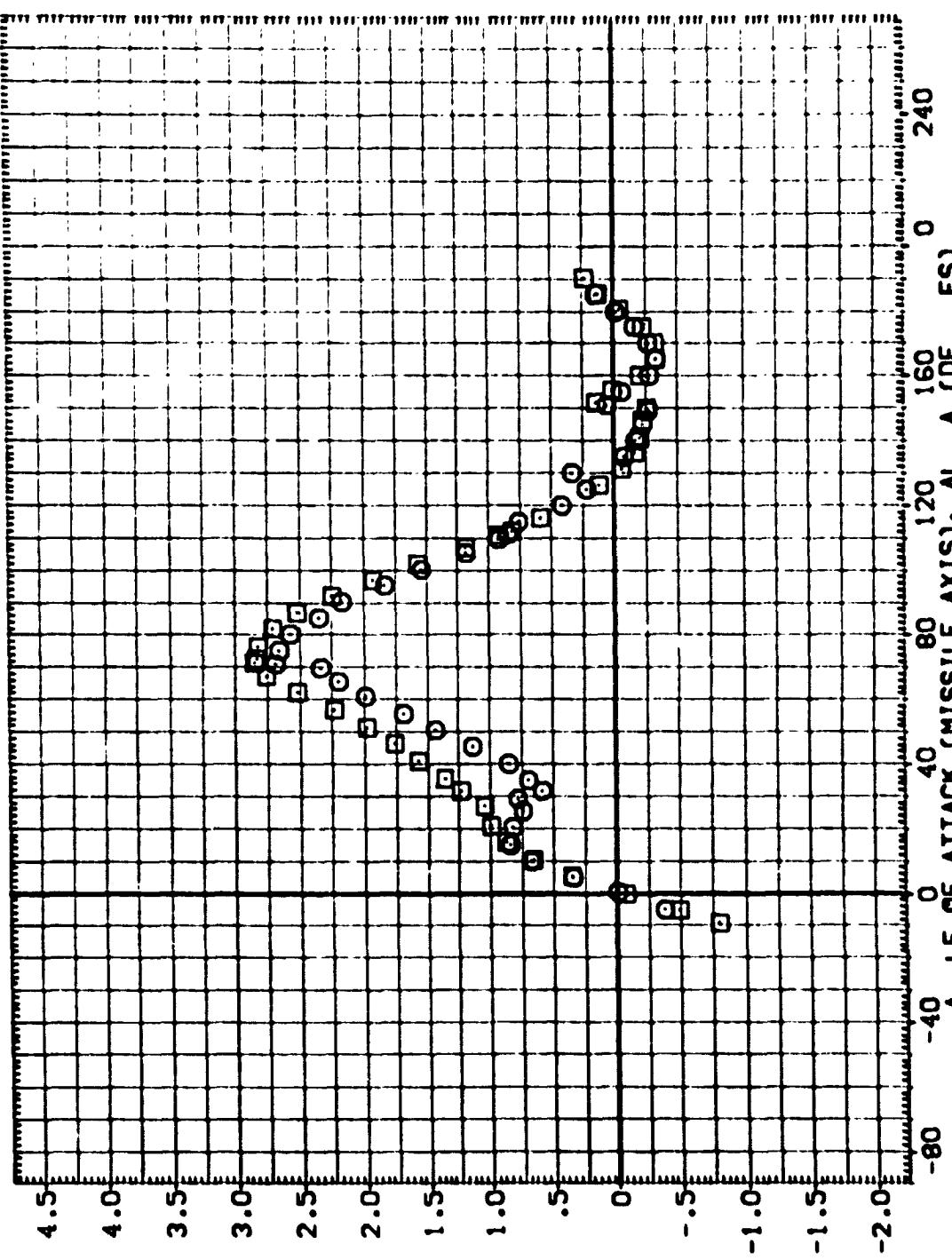


FIG. 12 MACH NUMBER AND REYNOLDS NUMBER COMPARISON
 (APHI) = 180.00

DATA
 [MEMO] 1 TION
 MACH 3.5-155 TAGE ET TANK VITR
 (CE) 3.5-155 TAGE ET TANK VITR
 1406.0
 SCALE



PITCHING MOMENT COEFFICIENT (MISSILE AXIS), CLMM

FIG. 12 MACH R AND REY LDS BER CO ARISON
 $(\Delta \rho \Phi)_1 = 1 .00$

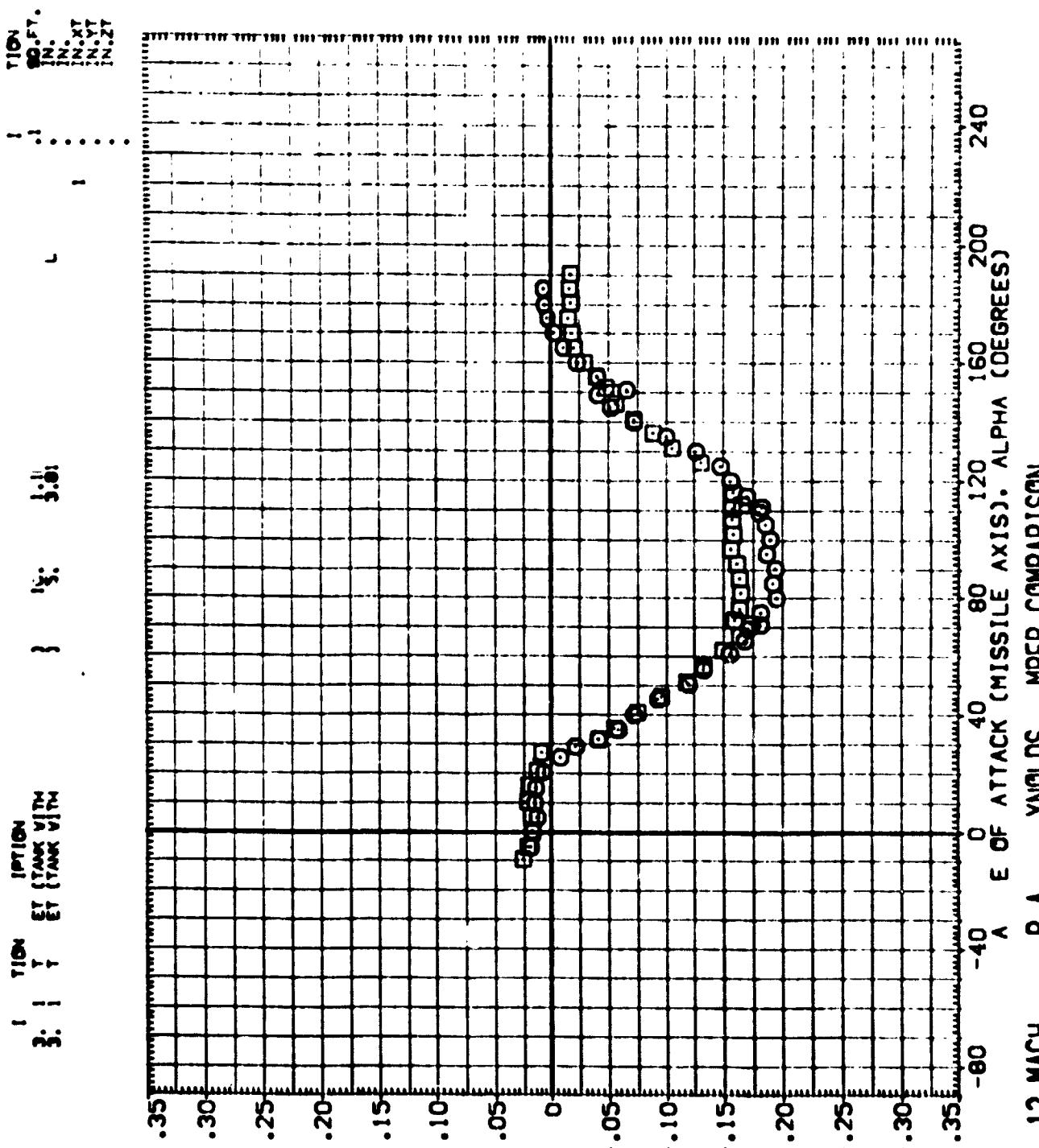


FIG. 12 MACH R A YNOLDS NUMBER COMPARISON
(W) I = 180.00

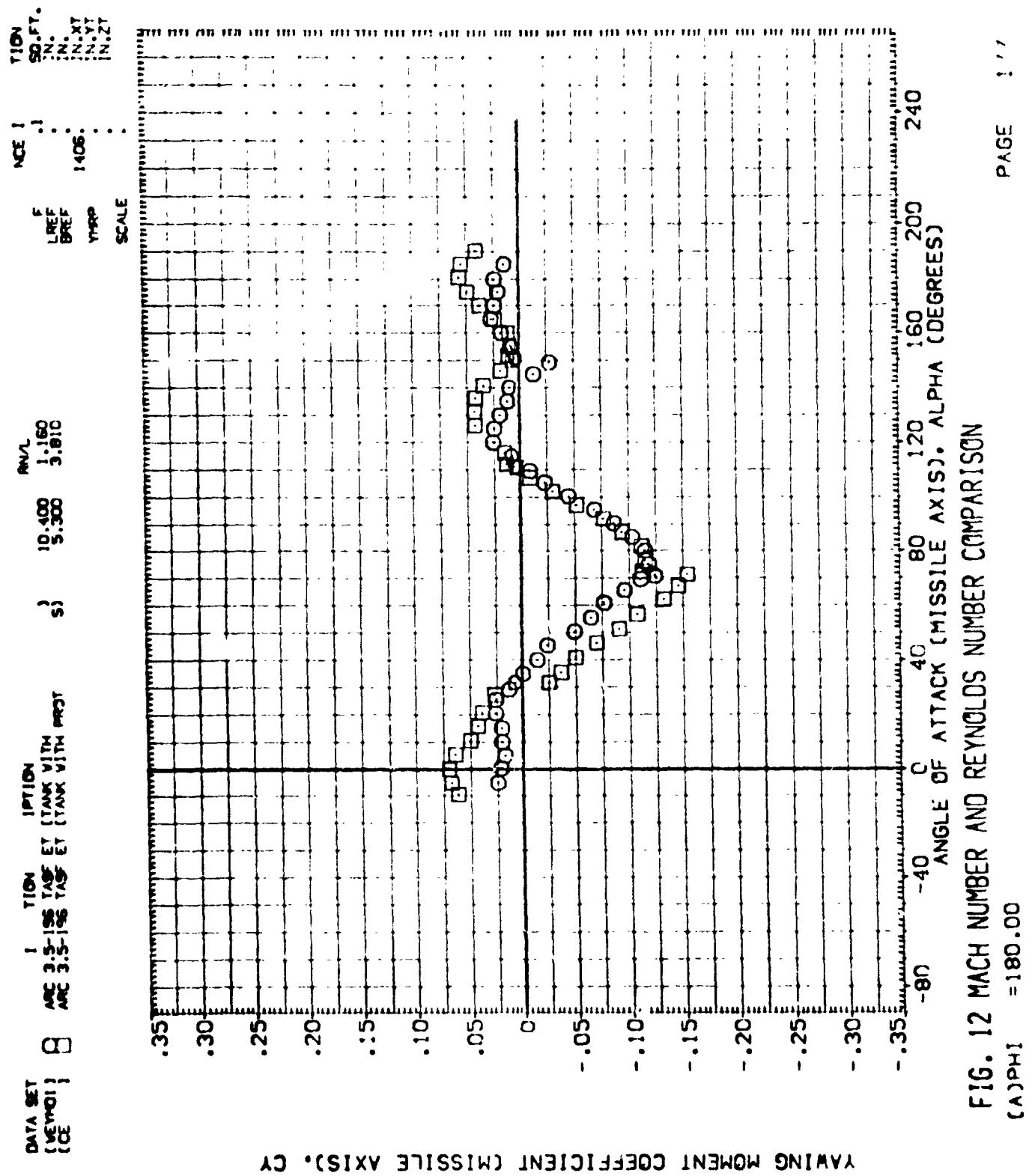
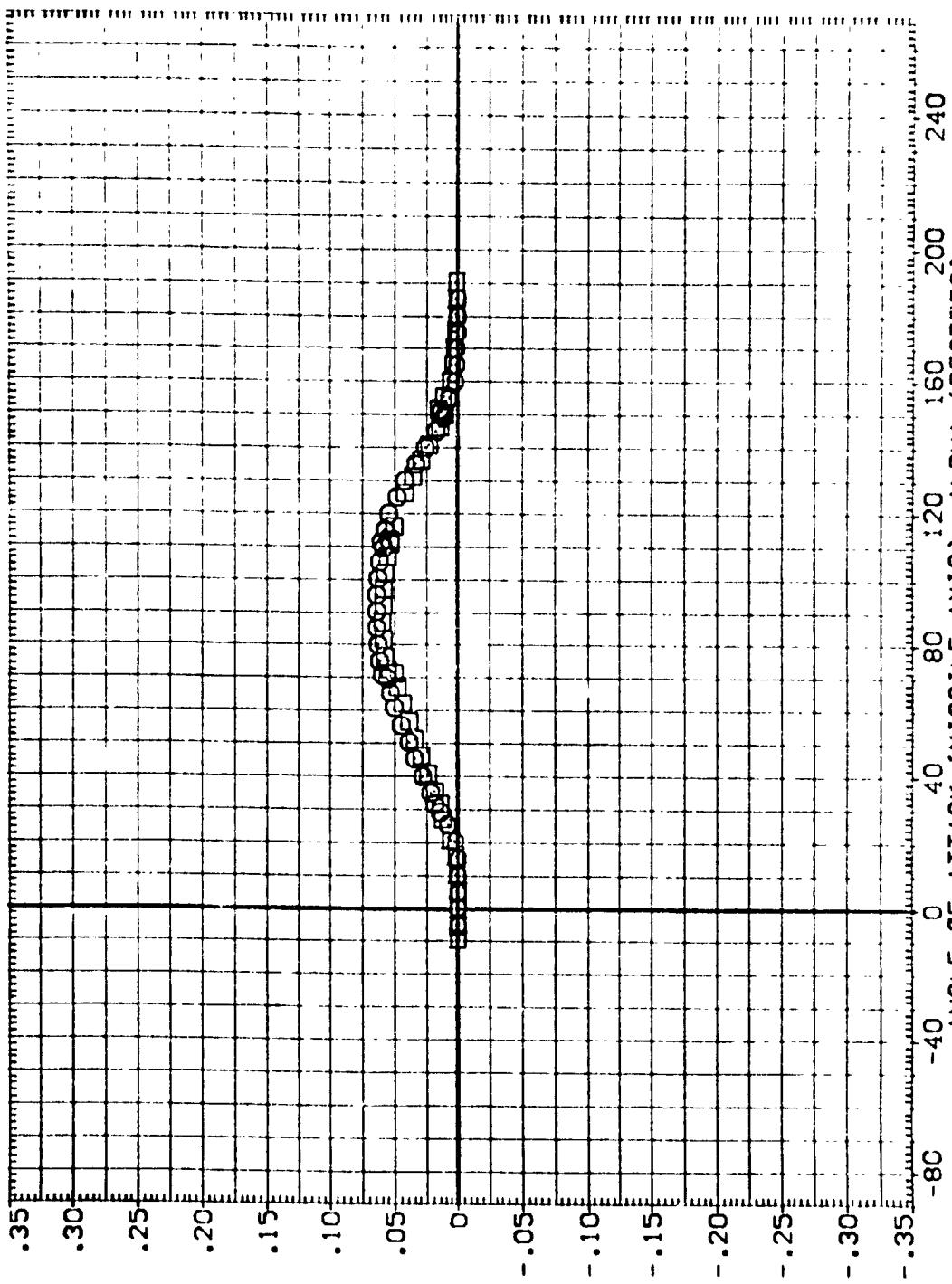


FIG. 12 MACH NUMBER AND REYNOLDS NUMBER COMPARISON

DATA SETS CONFIGURATION DESCRIPTION
 (WYHOL) ARC 3.5-196 TASF ET [TANK WITH PROTRUSIONS]
 (CEYH-33) ARC 3.5-196 TASF ET [TANK WITH PROTRUSIONS]

	MACH	R/V/L
SREF	10.460	1.160
LREF	5.300	3.810
BREF		
XMRP	330.2000	N.
YMRP	1406.0000	N. XT
ZMRP	.0000	N. ZT
SCALE	.0362	



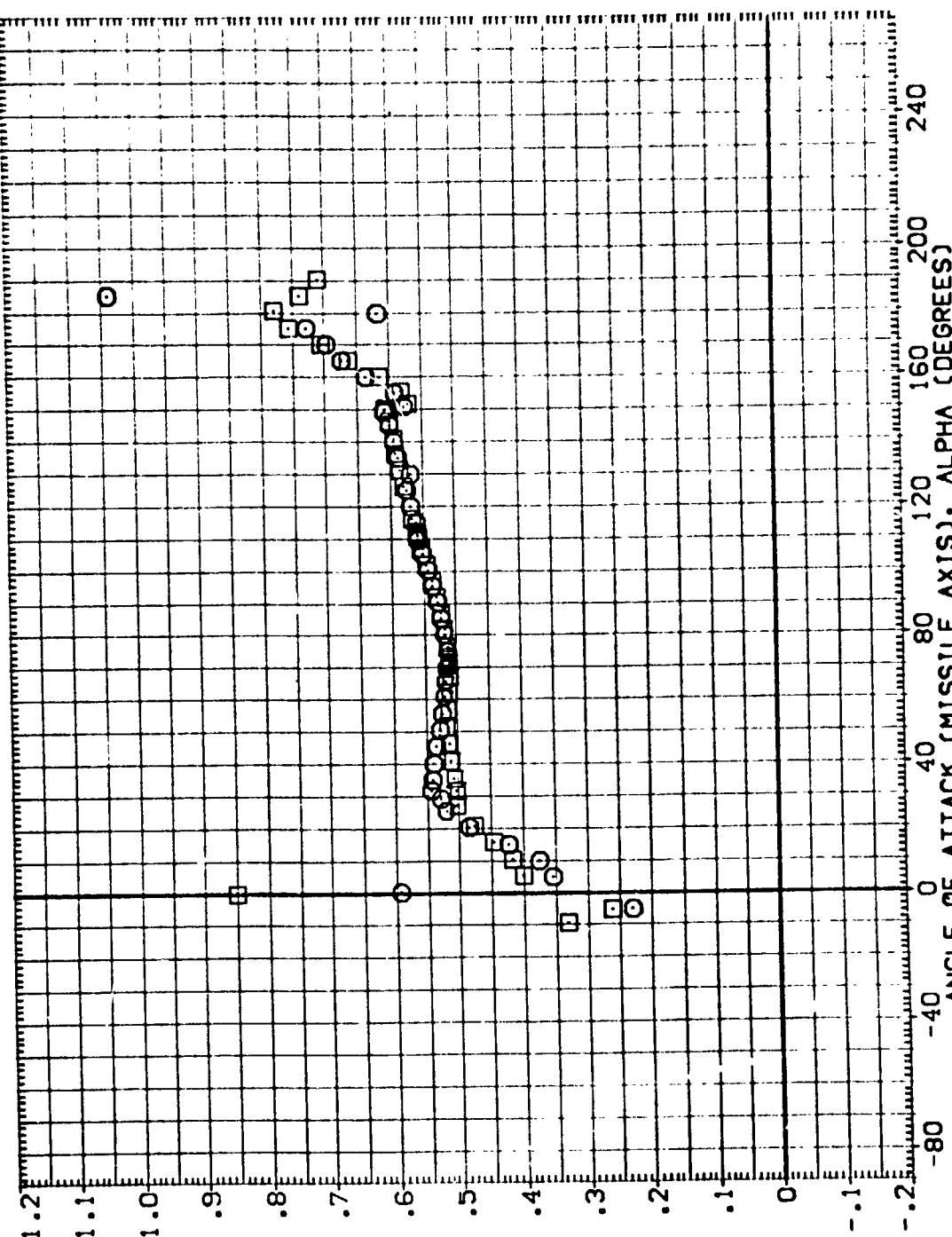
ROLLING MOMENT COEFFICIENT (MISSILE AXIS), C

FIG. 12 MACH NUMBER AND REYNOLDS NUMBER COMPARISON
 $(\Delta \rho \Phi) = 180.00$

DATA SET
(VEMO)
DATE SET
(CE)

FIGURE DESCRIPTION
ARC 3.5-196 TAG ET (TANK WITH PROTRUSIONS)
ARC 3.5-196 TAG ET (TANK WITH PROTRUSIONS)

	MACH	FLVL	REFERENCE INFORMATION
SREF	594.1360	IN.	
LREF	320.	IN.	
BREF	330.	IN.	
XMRP	1406.	IN.XT	
YMRP	.	IN.YT	
ZMRP	.	IN.ZT	
SCALE	.	.	



CENTER OF PRESSURE LOCATION, XCP/L

FIG. 12 MACH NUMBER AND REYNOLDS NUMBER COMPARISON
($\Delta\Phi$) = 180.00

APPENDIX
TABULATION SOURCE DATA

**Plotted data tabulations are available from
Data Management Services on request.**